



S-K 1300 Technical Report Summary

Sleeper Gold Mine, Humboldt County, Nevada

Paramount Gold Nevada Corp.

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1.0 Executive Summary

1.1 Summary

SLR International Corporation (SLR) was retained by Paramount Gold Nevada Corp. (PGN, Paramount Gold, or the Company) to prepare an independent Technical Report Summary (TRS) on the Sleeper Gold Mine (Sleeper or the Project), located in Humboldt County, Nevada, USA. The purpose of this TRS is to provide an Initial Assessment to support Mineral Resource disclosure. This TRS conforms to the United States Securities and Exchange Commission's (SEC) *Modernized Property Disclosure Requirements for Mining Registrants* as described in Subpart 229.1300 of Regulation S-K, Disclosure by Registrants Engaged in Mining Operations (S-K 1300) and Item 601(b)(96) Technical Report Summary.

Paramount Gold is a U.S.-domiciled precious metals exploration and development company engaged in the acquisition, exploration, and development of gold and silver projects in the United States. The company's principal assets include the Sleeper Gold Mine in Nevada and the Grassy Mountain Gold Project in Oregon, as well as additional exploration properties in the western United States. Paramount Gold is publicly listed on the NYSE exchange under the ticker symbol PZG and maintains its corporate offices in Winnemucca, Nevada.

Paramount Gold holds a 100% interest in the Sleeper Gold Mine, which includes the historical Sleeper open-pit gold mine and a large surrounding claim block totaling 2,474 unpatented mining claims covering approximately 44,917 acres (approximately 18,178 hectares) in Humboldt County, Nevada. The Sleeper mine was operated by AMAX Gold Inc. (AMAX) from 1986 through 1996, producing approximately 1.66 million ounces (Moz) of gold and 2.3 Moz of silver from open-pit mining and heap leaching and milling operations.

The Project is currently at the Initial Assessment (IA) stage, and as such, the level of engineering, geological definition, and metallurgical characterization remains preliminary. The Mineral Resources for the Project comprise in situ oxide and mixed material, in situ sulfide material, and material from existing waste rock dumps, heap leach pads (HLPs), and tailing storage facilities (TSFs). The development concept considered in the cash flow analysis presented in this TRS contemplates the restart of mining and processing operations with a focus on those Mineral Resources amenable to heap leaching, i.e., existing waste rock dumps and in situ oxide and mixed mineralized material. Additional work is required to develop the cash flow analysis for the sulfide Mineral Resources, including the heap leach and tailings material.

The existing waste rock dumps were generated during prior mining operations conducted under substantially lower gold prices, which led to the application of higher cut-off grades (COGs) at the time of mining. Consequently, material that was classified as waste under historical economic conditions contains grades that are potentially economic under current or reasonably foreseeable gold price assumptions and processing technologies. This reclassification to Mineral Resources forms a key component of the Project's economic rationale.

To support this evaluation, the waste rock dumps have been subject to initial drilling, sampling, and assaying programs, supplemented by preliminary metallurgical test work. These programs have been designed to characterize the grade distribution, material variability, and metallurgical response of the dump material, including leachability and recovery potential. While these datasets provide an important foundation for the current assessment, they remain limited in scope and density relative to that required for higher-confidence classifications, and additional work will be required to support future Mineral Resource estimation, metallurgical modeling, and process design.



In parallel, the Project concept includes recovery of in situ oxide and mixed mineralized material remaining in the vicinity of the historical pit. These materials are considered amenable to conventional surface mining methods and heap leach processing, consistent with prior operations at Sleeper, although additional drilling, metallurgical testing, and engineering studies will be required to confirm recoveries, processing parameters, and economic viability.

Overall, the Project represents a brownfields redevelopment opportunity, leveraging existing site disturbance, historical data, and previously mined material inventories; however, given the early stage of evaluation, all assumptions related to mineralization, processing performance, and economic outcomes should be considered preliminary and subject to refinement through subsequent phases of study. The development concept assumes a nominal processing rate of approximately 30,000 tonnes per day (tpd), utilizing conventional open pit mining, crushing and agglomeration, cyanide heap leaching, and Merrill-Crowe zinc precipitation to recover gold and silver.

The Base Case economic analysis presented in this TRS evaluates the potential economic viability of processing Measured, Indicated, and Inferred Mineral Resources. The Base Case mining inventory comprises the following:

- Approximately 47 million tonnes (Mt) of waste rock dump material, classified as Inferred Mineral Resources, grading approximately 0.28 g/t gold (Au)
- In situ oxide and mixed mineralized material including approximately 2 Mt Measured Resources grading 0.29 g/t Au, 78 Mt Indicated Resources grading 0.26 g/t Au, and 49 Mt Inferred Resources grading 0.24 g/t Au.

Overall, the Base Case production schedule includes approximately 55% of Inferred Resources as part of the economic analysis. An Alternative Case was considered that included only in situ Measured and Indicated Resources in the economic analysis.

1.1.1 Conclusions

1.1.1.1 Geology and Mineral Resources

- The geological interpretation and deposit model are appropriate, internally consistent, and aligned with a low-sulfidation epithermal system, with mineralization strongly controlled by fault architecture and lithological contrasts.
- Mineralization exhibits high spatial variability, with discontinuous high-grade veins embedded within a laterally and vertically continuous low-grade stockwork domain, which comprises most of the tonnage.
- The Mineral Resource estimate has been prepared in accordance with S-K 1300 and CIM (2019) Best Practice Guidelines, supported by appropriate domain modeling, compositing, grade capping, interpolation, and validation workflows.
- The estimate is constrained within optimized open-pit shells demonstrating Reasonable Prospects for Economic Extraction (RPEE,) based on reasonable mining, processing, and economic assumptions, including a long-term gold price of US\$3,100/oz.
- The drilling database is large and generally adequate (approximately 4,300+ drill holes); however, gaps in historical metadata, incomplete records, and exclusion of unverifiable data introduce uncertainty, which is appropriately reflected in classification.



- Historical drilling is predominantly vertical RC, which adequately defines bulk-tonnage mineralization but limits confidence in true geometry and continuity of steeply dipping high-grade structures.
- The QA/QC and sampling protocols, while variable in early historical programs, are considered sufficient overall due to:
 - o Exclusion of unreliable or unsupported data from the Mineral Resource Estimate (MRE)
 - o Validation of assay datasets through statistical analysis, capping, compositing, and multi-method estimation checks
 - o Use of industry-standard QA/QC review and data screening prior to estimation. Accordingly, the QP considers the analytical dataset valid and appropriate to support the MRE, with remaining uncertainties reflected in classification.
- The oxidation model has been reviewed and corrected for inconsistencies and is considered appropriate for current estimation; however, localized coding issues indicate moderate residual uncertainty where metallurgical assumptions are sensitive.
- Exploration datasets (geophysical, geochemical, geological) are well integrated and effective for targeting, defining structural corridors, and mineralized trends extending beyond historically mined areas.
- Mineralization remains open along strike, at depth, and beneath cover, with identified targets considered conceptual but supported by integrated datasets.
- Compared to the 2023 estimate, the 2026 MRE shows a material increase in tonnage and contained metal, driven by:
 - o Inclusion and delineation of surface materials (existing waste rock dumps, heap leach pads, and tailings storage facility);
 - o Expanded pit shells under higher gold price assumptions (US\$3,100/oz versus approximately US\$1,800/oz); and
 - o Updated geological interpretation and database validation.
- This increase in tonnage is accompanied by a moderate reduction in average grade, consistent with inclusion of marginal material and not indicative of estimation bias.

1.1.1.2 Mining and Mineral Reserves

- There is no current geotechnical information for the pit slopes. Current pit slope assumptions may be optimized once geotechnical information has been collected and incorporated into the pit design.
- The current Base Case life of mine (LOM) plan includes a significant proportion of Inferred Mineral Resources (approximately 55%). The next stage of the Project will require converting Inferred Resources to Indicated Resources to reduce the project risk.
- Pit slope design assumes dry (i.e., dewatered) walls. Pit dewatering needs to start early enough for the open-pit mining operation to begin.
- There is potential to extend the mine life with the addition of a sulfide pit. To include the sulfide pit in the LOM plan, additional metallurgical test work and block modeling will be required.



1.1.1.3 Mineral Processing

- Metallurgical test work supports heap leaching with Merrill-Crowe recovery for oxide, mixed, and selected waste-rock materials, and flotation with off-site toll treatment or concentrate sale for sulfide, existing heap leach pad (HLP), and existing tailings material.
- The Base Case economic analysis is restricted to the heap-leach scenario, which is supported by the most complete, representative, and internally consistent metallurgical dataset.
- The proposed Base Case processing facility is a 30,000 tpd conventional crush–agglomerate–heap-leach operation employing Merrill-Crowe recovery. Design parameters include crushing to approximately P₈₀ 19 mm and agglomeration using cement and/or lime.
- Facilities oxide material demonstrates the strongest metallurgical response to heap leaching, with additional oxide, mixed, and selected waste-dump composites also supporting inclusion in the heap-leach feed blend.
- Gold and silver recovery assumptions for the heap-leach case are derived primarily from column leach testing, with conservative assumptions applied where only bottle-roll or limited test data exist.
- Sulfide, HLP, and tailings materials represent future processing opportunities via flotation. Recoveries have been reduced by 12% to account for toll-milling deductions and downstream treatment charges.
- No silver recovery is currently attributed to the flotation scenario; silver is treated as upside potential pending further metallurgical test work and commercial assessment.
- The heap leach flowsheet is a commercially proven, low-risk processing route appropriate for IA-level planning.
- Preliminary test work of the flotation option as a processing method for the sulfide material and existing HLP and TSF material is sufficient for the declaration of Mineral Resources; however, additional variability testing, concentrate characterization, and commercial evaluation are required to advance this option.

1.1.1.4 Infrastructure

- Access to the mine site is reliable via frequently traveled and maintained public infrastructure from Winnemucca, Nevada.
- Access and haul roads constructed on site will be designed and constructed in a manner sufficient to facilitate required on-site vehicular movement
- The proposed heap leach pad has been sited based on terrain, environmental, and operational bases and has been adequately sized to accommodate 175 Mt of agglomerated mineralized material.
- The pregnant solution and barren solution ponds have been located in proximity to the leach pad to take advantage to native slopes and have been sized to accommodate operational solution flow rates.
- The storm event pond has been located adjacent to the process ponds and has been sized to accommodate the 100-year 24-hour storm volume.



- Rapid infiltration basins have been designed to accommodate infiltration from pit dewatering efforts at an average rate of 4,542 m³/hr (20,000 US gallons per minute [gpm]).
- No accommodation camp has been included in the proposed infrastructure as the town of Winnemucca is within commuting distance and hosts a knowledgeable mining industry labor force.

1.1.1.5 Environment

- There are no known significant environmental issues at the site, and the former mine is in an advanced state of closure with post-closure monitoring and minor operational and maintenance activities being conducted.
- The regulatory environment is well developed, and the environmental permitting path forward for the mine plan presented in this TRS is generally well understood.

1.1.1.6 Capital and Operating Costs

- Preliminary capital and operating cost estimates have been prepared for the proposed mining operation based on a conceptual processing rate of approximately 30,000 tpd.
- For the Base Case, initial capital costs required to restart mining operations are estimated to be approximately US\$201 million, with sustaining capital estimated at approximately US\$342 million over the life of mine.
- Life-of-mine operating costs for the Base Case are estimated to average approximately US\$13.03 per tonne processed, resulting in an estimated all-in sustaining cost of approximately US\$2,407 per ounce of gold produced.

1.1.1.7 Risks

- The economic analysis presented in the Base Case as part of this TRS includes a material proportion of Inferred Mineral Resources within the mine plan and associated cash flow. The Inferred Mineral Resources are included at the beginning of the life-of-mine plan by mining existing dumps in the economic analysis, which introduces significant uncertainty.

1.1.2 Recommendations

The SLR QPs offer the following recommendations by discipline:

1.1.2.1 Geology and Mineral Resources

- 1 Conduct the following drilling and exploration programs:
 - a) Infill drilling to support conversion of Inferred to Indicated Mineral Resources (in situ and surface materials) by conducting systematic infill drilling within pit-constrained in situ domains and within surface material domains (dumps, heap leach pads, and TSF) to increase data density and improve confidence in grade continuity, tonnage, and material variability, consistent with S-K 1300 classification criteria.
 - b) Targeted infill drilling within established mineralization domains to increase drill density within defined grade domains to better constrain grade variability and continuity, particularly in areas where current spacing limits classification.



- c) Additional drilling and geological logging to improve confidence in oxide, mixed, and sulfide boundaries, which directly influence metallurgical assumptions applied in the MRE.
- 2 Geology and Mineral Resource Estimate
- a) Maintain domain-controlled drilling and sampling protocols to ensure all new data collection aligns with the current geological, mineralization, and estimation domain framework to support direct integration into future MRE updates.
 - b) Incorporate new data into updated geological interpretations and block models to support iterative improvement of the Mineral Resource estimate in accordance with S-K 1300 reporting requirements.
 - c) Acquire additional bulk density measurements across in situ and surface material domains where current density assignments are based on limited data, to improve tonnage estimates.
 - d) Focus drilling within the existing Mineral Resource footprint by prioritizing data acquisition in areas where incremental drilling is most likely to materially improve classification, rather than expanding the resource footprint at this stage.
- 3 Quality Assurance and Quality Control
- a) Implement consistent QA/QC protocols for future work. Apply standardized QA/QC procedures (sampling, insertion rates, documentation) to ensure all new data meets S-K 1300 and CIM (2019) requirements and supports classification upgrades.
 - b) Recommend investigation of incomplete database information and update the database through investigation of historic files

To advance the Project, the QP recommends that Paramount Gold undertake a two-phase exploration and data validation program totaling \$8.52 million, as summarized in Table 1-1.

The goal is to support upgrading Inferred Mineral Resources to the Indicated category, validate key project assumptions regarding density and metallurgy, and continue delineation in underexplored areas.

This budget reflects a disciplined yet robust investment to de-risk the MRE, validate key technical assumptions (density, metallurgical recovery), and support a potential future Preliminary Feasibility Study (PFS). The recommended work is expected to materially enhance the geological understanding and economic viability of the Sleeper Project.

The two phases of the work program are independent of each other.

Table 1-1: Proposed Sleeper 2026-2027 Exploration Budget

Activity	Details	Estimated Cost (US\$ 000)
Phase 1 – Surface and In Situ Resource Definition, QA/QC Implementation, and Metallurgical Studies		
ESG Permitting	Exploration and Environmental Permits for Phase 1 drilling	25
Sonic Drilling	Up to 30 holes (4000 ft) of sonic drilling at \$90/ft focused on obtaining metallurgical samples from Waste dumps, TSF and HL pads	360
RC Drilling	Up to 500 holes (50,000 ft) of RC drilling in Waste dumps, HL pads at \$50/ft	2,500



Activity	Details	Estimated Cost (US\$ 000)
Core drilling	Confirmation core drilling of up to 10,000 ft at \$120/ft (HQ/NQ core)	1,200
Bulk Density Sampling	Collection and testing of up to 200 core and/or pit samples across all domains	12
Geochemical Assays	Assaying of approximately 15,000 samples incl. duplicates, standards, and blanks	750
QA/QC Program Implementation	Establish certified sample control and auditing protocols	100
Metallurgical Testing	Leach testing of mineralized core for recovery studies	750
Technical Staff & Supervision	Field geologist, QA/QC lead, database tech	300
Total Phase 1		5,997
Phase 2 – Project Development Scoping		
ESG Permitting	Exploration and Environmental Permits for Phase 2 Geotech	25
Ground Support Geotechnical Testing	Geotech and analysis studies for Ground Support	250
Heap Leach Pad Geotechnical Testing and Design	Geotech and design engineering studies for Heap Leach Pad	600
Mining and Process Design & Engineering Analysis	Process design and engineering cost analysis and modeling	400
Environmental Baseline Studies	Hydrogeology, cultural, flora/fauna baseline for mine permitting	800
Stakeholder Engagement & Permitting Prep	Initial outreach, permitting roadmap	100
Technical Oversight & Contingency (10%)	Includes legal, overhead, permitting scope prep	218
Reporting and Independent Review	S-K 1300 PFS update and QP sign-off	350
Total Phase 2		2,723
Grand Total		8,740

1.1.2.2 Mining and Mineral Reserves

- 1 Collect geotechnical information and develop geotechnical studies to support the pit design slopes for the next stage of the project.
- 2 Ensure the open-pit mining sequence is closely coordinated with the open-pit dewatering plan.
- 3 Continue the analysis of the sulfide pit as an opportunity after the oxide pit mining.



1.1.2.3 Mineral Processing

1. Complete additional variability column leach testing on oxide, mixed, and waste rock dump domains to confirm recovery, leach kinetics, and reagent consumption across the planned heap leach feed range.
2. Confirm provisional recovery assumptions for Sleeper oxide, Sleeper mixed, and West Wood mixed material with representative column leach test work.
3. Refine crush-size and agglomeration test work to confirm the selected coarse-crush heap leach design basis and optimize cement and lime addition by material type.
4. Expand reagent-consumption testing to better define sodium cyanide, lime, and cement demand for oxide, mixed, and waste rock dump materials, particularly where existing results indicate variable or elevated consumable requirements.
5. Complete additional column leach testing on selected waste rock dump materials to refine recovery assumptions by dump area and improve confidence in domain-based economic modeling.
6. Complete additional deleterious-element and precipitate-quality testing for Hg, As, Sb, and sulfur to confirm mercury management requirements and refine refinery and operating cost assumptions.
7. Complete flotation variability, optimization, and locked-cycle test work on representative sulfide, HLP and tailings composites to confirm recovery, consumable requirements, concentrate quality, and the suitability of an off-site toll-treatment or concentrate-sale route.

1.1.2.4 Infrastructure

- 1 Evaluate site-wide water balance and discharge requirements.
- 2 Perform a hydrogeological evaluation to support PFS level engineering of the rapid infiltration basin.
- 3 Confirm power requirements and supply availability.
- 4 Develop site-specific design criteria for the HLP and perform field investigations and laboratory testing to support advancing the HLP design.
- 5 Develop a PFS level HLP design that incorporates site specific data into the engineering calculations and analysis for such items as grading plan, slope stability analysis, water balance, settlement, and closure.

1.1.2.5 Environment

1. Complete updated baseline studies in accordance with National Environmental Policy Act of 1969 (NEPA) and applicable guidelines.
2. Engage early with local stakeholders and tribes and develop a stakeholder outreach plan.
3. Develop a permitting strategy and timeline.



1.1.2.6 Capital and Operating Costs

- 1 Move the dewatering from an “Allowance” to a full ‘Engineered System’, e.g., calibrated groundwater model; staged dewatering sequencing; pumping lift curves by pit phase; transient inflow modeling; wellfield spacing and drawdown analysis; contingency pumping scenarios; and power demand modeling for peak pumping periods.
- 2 Re-evaluate the crushing/agglomeration trade-off, e.g., variability column testing; permeability testing; compaction testing; fines migration testing; cement consumption optimization; lift-height testing; and irrigation optimization.
- 3 Tighten the heap leach pad phasing strategy, e.g., minimizing initial lined acreage; maximizing early vertical expansion; deferring later phases; reducing early pond construction; and sequencing underdrain installation.
- 4 Lock down power infrastructure requirements early, e.g., actual condition of transmission line; substation rebuild requirements; transformer replacement needs; utility interconnect requirements; and backup generation philosophy.
- 5 Validate the contractor mining strategy, i.e., obtain budgetary contractor bids; benchmark Nevada owner-mining versus contractor-mining; validate bank cubic meter (bcm) assumptions; stress-test diesel escalation; and stress-test productivity losses from wet conditions.
- 6 Refine the estimate by:
 - a) Improving mine haulage and re-handle modeling.
 - b) Tightening reagent consumption assumptions.
 - c) Adding more detailed closure escalation and water management costs.

1.2 Economic Analysis

The economic analysis presented in this IA considers the processing of the in situ oxide and mixed Mineral Resources and the Mineral Resources in the existing waste rock dumps only.

The economic analyses contained in this TRS are preliminary in nature and are based, in part, on Inferred Mineral Resources that are considered too speculative geologically to have modifying factors applied to them that would enable them to be categorized as Mineral Reserves. It is important to note that, unlike Mineral Reserves, Mineral Resources do not have demonstrated economic viability, and there is no certainty that the economic projections presented in this IA will be realized.

Taxes and revenues are assumed. Discounted cash flow analyses are based on assumed production rates and revenues from available Mineral Resources.

SLR notes that the economic analysis presented in this section is based on revenue from gold and silver only. After-tax cash flow projections have been generated from the Base Case and the Alternative Case LOM production schedules and capital and operating cost estimates, as summarized in the sub-sections that follow.

1.2.1 Base Case

The Project’s Base Case is based on a production plan with a mine life of 17 years and includes a mineralized material inventory of approximately:



- Approximately 47 million tonnes (Mt) of waste rock dump material, classified as Inferred Mineral Resources, grading approximately 0.28 g/t gold (Au)
- In situ oxide and mixed Mineral Resources including approximately 2 Mt Measured Resources grading 0.29 g/t Au, 78 Mt Indicated Resources grading 0.26 g/t Au, and 49 Mt Inferred Resources grading 0.24 g/t Au.

The Base Case mineralized material inventory includes approximately 95.6 Mt of Inferred Mineral Resources containing 788 koz of gold and 6,484 koz of silver, representing approximately:

- 55% of the total Base Case tonnage.
- 54% of the total Base Case gold ounces.
- 41% of the total Base Case silver ounces.

The remaining material in the mined inventory is from Measured and Indicated Mineral Resources. A summary of the Base Case criteria is provided below.

1.2.1.1 Economic Criteria

1.2.1.1.1 Revenue

- Mine life: 17 years.
- LOM production and processing plans as summarized in Table 13-9 and Table 13-8, respectively.
- 30,000 tpd mineralized material stacked (approximately 10.8 Mt per year), average stacked grade of 0.26 g/t Au and silver grade of 2.79 g/t Ag (ROM, crushed, and stockpile mine plan).
- Mine life averages 65,000 ounces per year of gold recovered and 205,000 ounces per year of silver recovered from the mine plan, with LOM stacked process gold recovery averaging 75.8% and silver recovery averaging 22.1%.
- Total 1.11 Moz of gold recovered, and 3.5 Moz of silver recovered over the LOM operation.
- The summary of the physicals in the financial model is listed in Table 1-2. It has been estimated that 420 koz of gold and 2,952 koz of silver are in waste rock dumps and are accounted for in the financial model over the first five years of Leach Pad operations.
- Gold and silver payable at the refinery are assumed at 99.95% Au payable and 97.0% Ag payable
- Gold and silver prices are based on analyst consensus price forecasts from the end of March 2026. For the economic analysis it was assumed:
 - o Y1: US\$4,000/oz Au and US\$59.00/oz Ag
 - o Y2 to Y17: US\$3,600/oz Au and US\$48.00/oz Ag
 - o Resulting in LOM net realized prices of:US\$3,618/oz Au and US\$48.70/oz Ag
- Net Smelter Return (NSR) includes doré refining, transport, and insurance costs.
- NSR royalty assumed at 3%. The property is subject to different royalties between 0.5% and 3%, and for modeling purposes was assumed at an overall 3%



- Revenue is recognized at the time of gold and silver production.
- Non-cash inventory adjustments are not included in the SLR cash flow model.
- LOM net revenue is US\$4,014 million (after royalty, transportation, and refining charges)

Table 1-2: Sleeper Base Case Production Physicals Summary

Physicals	Value
Total Mineralized Material Stacked (kt)	175,445
Max Process Rate (tpd)	30,000
Au Head Grade (g/t)	0.26
Ag Head Grade (g/t)	2.79
Contained Au (koz)	1,459
Contained Ag (koz)	15,721
Average Recovery, Au	75.8%
Average Recovery, Ag	22.1%
Recovered Au (koz)	1,106
Recovered Ag (koz)	3,481
Payable Au (koz)	1,101
Payable Ag (koz)	3,376
Avg Annual Au - LOM (koz / yr)	65
Avg Annual Ag Sales - LOM (koz / yr)	199

1.2.1.1.2 Costs

- Pre-production period assumes 24 months (Year -1 to Year -2).
- Initial (Growth) and development capital costs total US\$201 million
- Mine life sustaining capital totals US\$343 million
- Final reclamation costs from after year 17 total US\$52.4 million.
- Mine life capital totals US\$596 million.
- Average LOM operating cost is US\$13.03 per tonne stacked.
 - o Open pit operating costs of US\$2.53 per tonne mined (US\$6.37 per tonne stacked). Includes out-of-scope mining operations.
 - o Dewatering operating costs of US\$0.59 per tonne stacked.
 - o Processing operating costs of US\$5.55 per tonne stacked.
 - o Site services & general and administrative (G&A) costs of US\$5.6 million per year for years of full production (LOM average of US\$0.52 per tonne stacked).
- Life of Mine production plan as summarized in Table 13-9.

1.2.1.1.3 Taxation and Royalties

The federal and state income taxes are summarized in Table 1-3.



Table 1-3: Federal and State Tax Summary

Tax Type	Rate
Federal Corporate Income Tax	21.0%
Nevada Corporate Income Tax	5.0% of federal taxable income
Royalties and Severance Fees	Based on ore extracted (state-regulated).

A total of five NSR royalties apply to future mineral production from portions of the Project. These royalties are summarized in Table 1-4.

Table 1-4: Royalties Summary

Royalty Holder	Royalty Terms
Snyder Syndicate	1% NSR on the 1,044 Sleeper Gold Mine claims (All claims, EXCEPT for ALL MIMI, ALL SP, AL SS, AND ALL BLUE.)
Franco-Nevada U.S. Corporation	2% NSR on minerals produced from all 2,474 claims
Evolving Gold / Quinton Hennigh	2% NSR royalty on all SS and all SP claims.
Dry Lake Placer Association	3% NSR on Dry Lake Placer claims
ICN Resources Ltd.	0.5% NSR on all SS and all SP claims; 1.5% NSR on all Blue claims

For the economic analysis and financial modeling purposes, an overall 3% NSR royalty rate was assumed over the LOM.

1.2.1.2 Cash Flow Analysis

SLR has prepared its own unlevered after-tax LOM cash flow model based on the information contained in this TRS to confirm the physical and economic parameters of the Project.

The Project's Base Case economics have been evaluated using the discounted cash flow method, considering annual processed tonnages and the associated gold and silver grades. The process gold and silver recoveries, gold and silver price forecasts, operating costs, refining and transportation charges, royalties, and initial and sustaining capital expenditures were also considered.

The Project, as currently designed, has variations in the mining and processing amounts over its planned 17-year life. These variations are shown in Figure 1-1, Figure 1-2, and Figure 1-3.



Figure 1-1: Mine Production Profile by Material Movement – Base Case

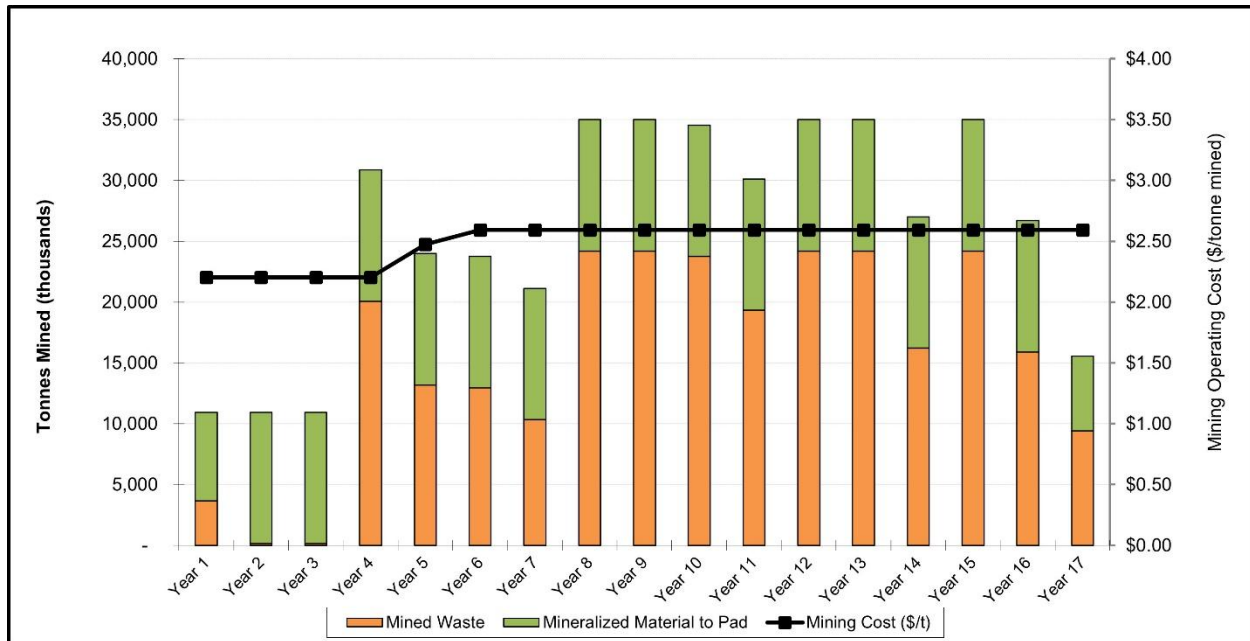


Figure 1-2: Process Production Profile and Head Grade – Base Case

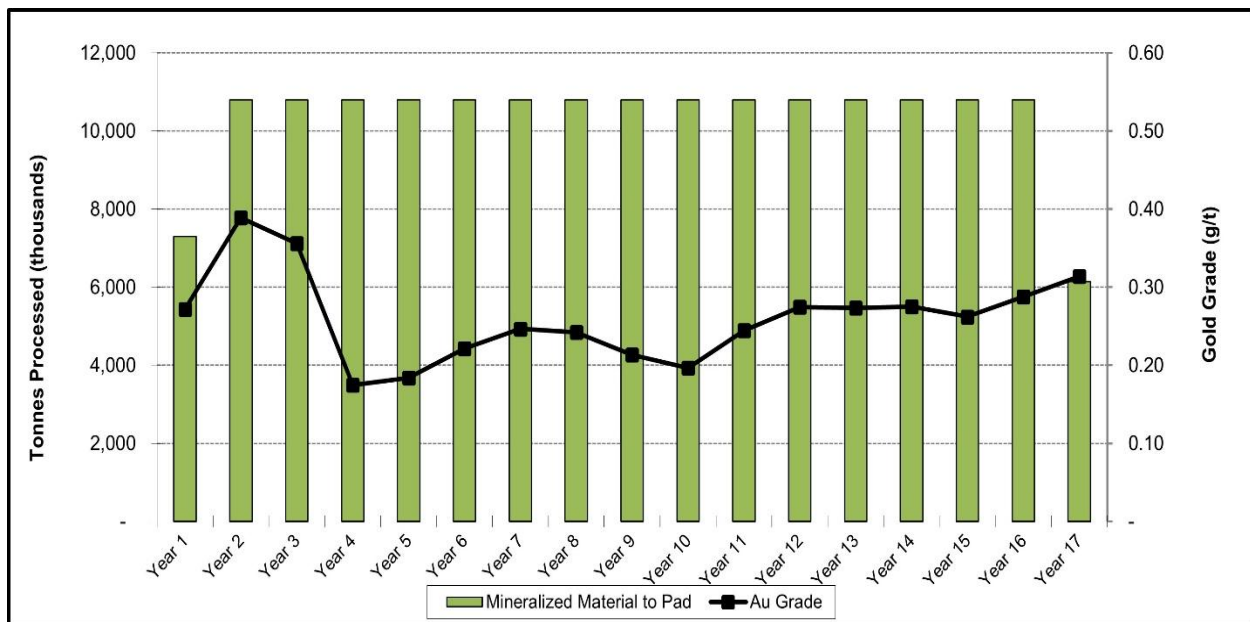
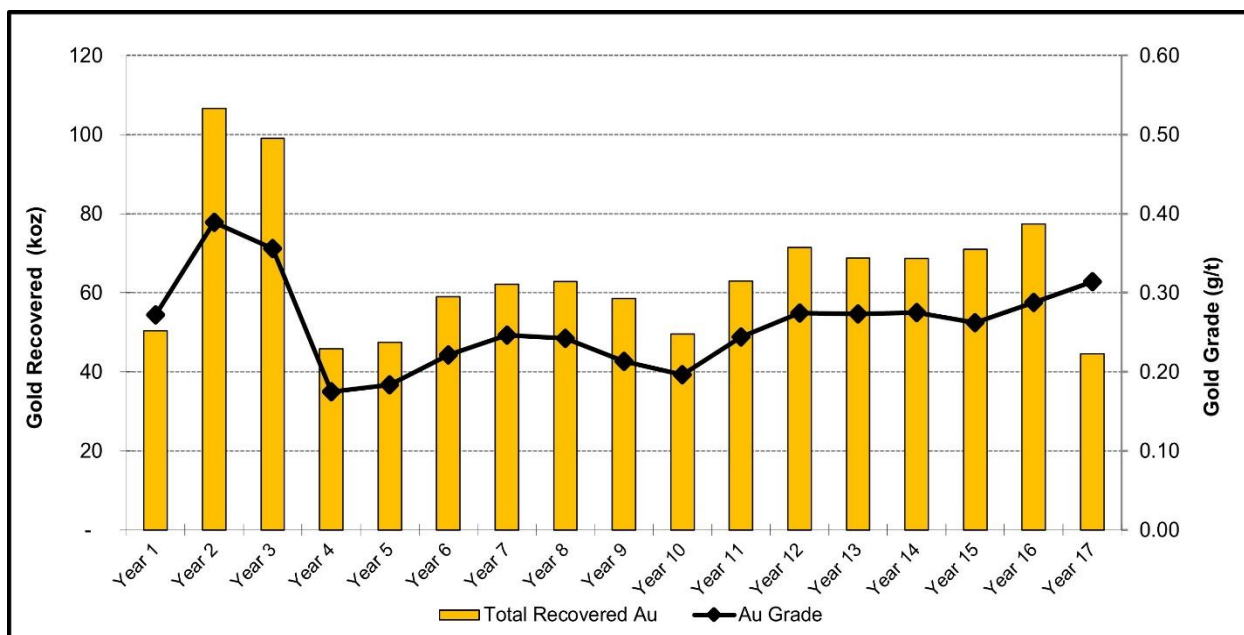


Figure 1-3: Annual Processing Gold Production and Head Grade Profile – Base Case



The economic analysis demonstrates that the Project’s Mineral Resources have reasonable prospects for economic extraction at the LOM net average realized prices of US\$3,618/oz Au and US\$48.70/oz Ag, and with long-term prices of US\$3,600/oz Au and US\$48.00/oz Ag, and that further advancement of Project studies is warranted.

A base discount rate of 8% has been applied in this TRS for the Project. This rate is considered reasonable for evaluating a precious metals project at a preliminary level of project definition, such as Sleeper. Discounted present values of annual cash flows are summed to arrive at the Mine’s Base Case NPV.

Considering the Project’s Base Case on a stand-alone basis, the Project’s pre-tax NPV at an 8% discount rate is approximately US\$505 million, and the pre-tax internal rate of return (IRR) is approximately 51.3%. The Project’s after-tax NPV at an 8% discount is approximately US\$402 million, the after-tax IRR is approximately 44.5%, and the payback period is approximately 1.4 years from the start of production.

The LOM undiscounted pre-tax cash flow totals approximately US\$1,132 million, and the LOM undiscounted after-tax cash flow totals approximately US\$918 million.

SLR has also run a stand-alone economic analysis for the Project using flat resource metal prices of US\$3,100/oz Au and US\$34/oz Ag, and the analysis demonstrates that the Project’s Mineral Resources also have reasonable prospects for economic extraction at these prices.

The Project’s after-tax free cash flow profile and gold payable metal per year are presented in Figure 1-4.



Figure 1-4: Base Case Project After-Tax Metrics Summary

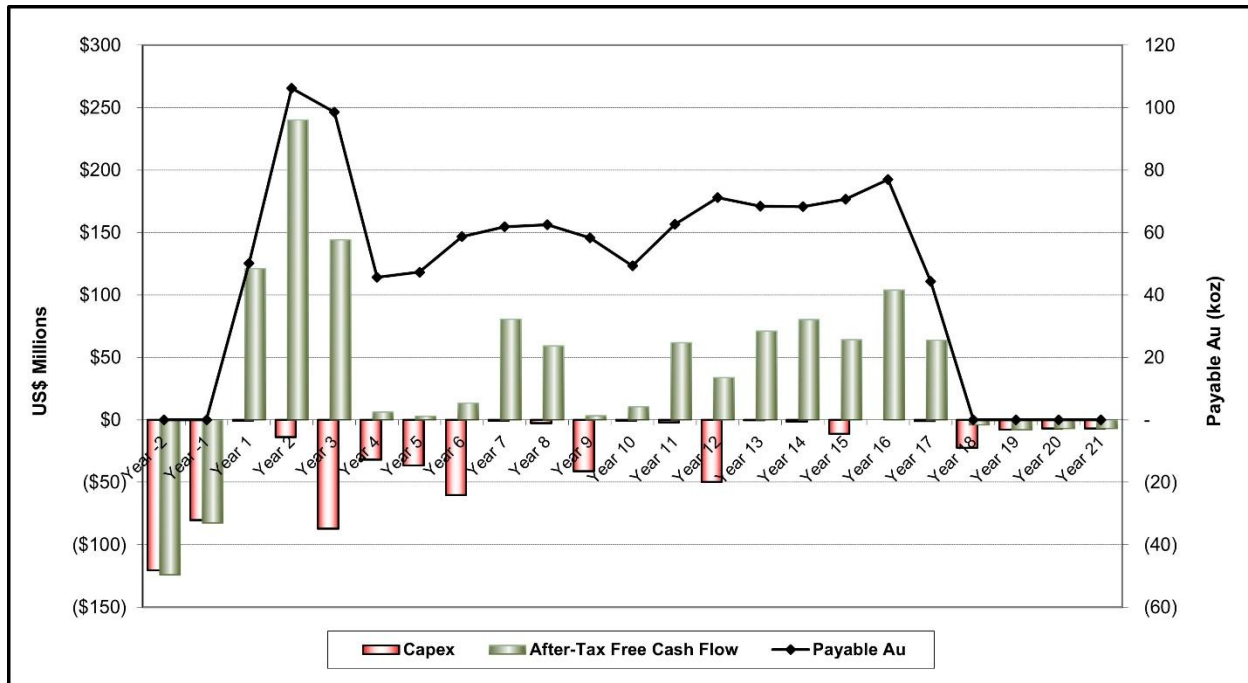


Table 1-5 shows the LOM total metrics for the Sleeper mine as currently designed. Due to the length of the mine life, the full annual cash flow model is presented in Appendix 2.

Table 1-5: Total Life of Mine Metrics – Base Case

Item	Units	Base Case Values
Realized Market Prices		
Au Price	US\$/oz	\$3,618
Ag Price	US\$/oz	\$48.70
Payable Gold	koz	1,101
Payable Silver	koz	3,376
Total Gross Revenue	US\$ million	4,147
Mining Cost	US\$ million	(1,117)
Dewatering Costs	US\$ million	(104)
Process Cost	US\$ million	(974)
G & A Cost	US\$ million	(92)
Refining/Freight	US\$ million	(8)
Royalties	US\$ million	(124)
Total Operating Costs	US\$ million	(2,418)
Operating Margin (EBITDA)	US\$ million	1,728
Federal Income Tax	US\$ million	(134)



Item	Units	Base Case Values
State Tax - Nevada Mining Tax	US\$ million	(80)
Working Capital	US\$ million	0
Operating Cash Flow	US\$ million	1,514
Development (Initial) Capital	US\$ million	(201)
Sustaining Capital	US\$ million	(343)
Closure/Reclamation Capital	US\$ million	(52)
Total Capital	US\$ million	(596)
Pre-tax Free Cash Flow	US\$ million	1,132
Pre-tax NPV @ 5%	US\$ million	670
Pre-tax NPV @ 8%	US\$ million	505
Pre-Tax IRR	%	51.3%
Pre-Tax Payback	years	1.3
After-tax Free Cash Flow	US\$ million	918
After-tax NPV @ 5%	US\$ million	539
After-tax NPV @ 8%	US\$ million	402
After-Tax IRR	%	44.5%
After-Tax Payback	years	1.4

Note: Numbers may not add due to rounding.

The Project's World Gold Council Adjusted Operating Cost (AOC) net of Ag by-product credits is US\$2,048/oz Au payable. The mine life sustaining capital costs are US\$359/oz Au payable, for an All-in Sustaining Cost (AISC) net of Ag by-products credits of US\$2,407/oz Au payable.

The average annual gold sales during operations are approximately 64,746 payable ounces. Table 1-6 shows the AISC build-up.

Table 1-6: Base Case All-in Sustaining Costs Composition

Item	Total LOM (\$ million)	Unit Cost (\$/oz Au)
Mining	1,117	1,015
Dewatering	104	94
Process	974	885
Site G&A	92	83
Subtotal Site Costs	2,286	2,077
Refining/Freight	8	8
Mining Royalties	124	113



Item	Total LOM (\$ million)	Unit Cost (\$/oz Au)
Total Cash Costs before by-product credits	2,418	2,197
Ag By-Product Credit	(164)	(149)
Total Cash Costs net of by-product credits	2,254	2,048
Sustaining Capital Cost	343	311
Closure/Reclamation Costs	52	48
Total Sustaining Costs	395	359
Total All-in Sustaining Costs	2,649	2,407

Note: Numbers may not add due to rounding.

The AISC calculated in the cash flow analysis reflects the benefit of low-cost ounces already stacked on the heap leach pads, compared to AISC estimated in a steady-state model that assumes current input costs. Much of Sleeper’s near-term production comes from material mined and placed in prior years, when gold prices, fuel, and consumable costs were lower. These ounces require minimal additional spending to recover, resulting in lower realized cash costs. As these legacy ounces are depleted and replaced with newly mined material, unit costs are expected to gradually normalize toward long-term levels.

1.2.1.3 Sensitivity Analysis

The Project’s Base Case risks can be identified in both economic and non-economic terms. Key economic risks were examined by running cash flow sensitivities:

- Metal prices
- Head grade
- Metallurgical Recovery
- Operating costs
- Pre-production and sustaining capital costs

Where possible, the after-tax NPV 8% sensitivities relative to the Base Case have been calculated for -20% to +20% variations in head grade and recovery, and -20% to +30% in metal prices. Operating and capital cost sensitivities have been calculated at -15% to +35% variations. The sensitivities are shown in Table 1-7 and Figure 1-5.

Table 1-7: Base Case After-Tax Sensitivity Analyses

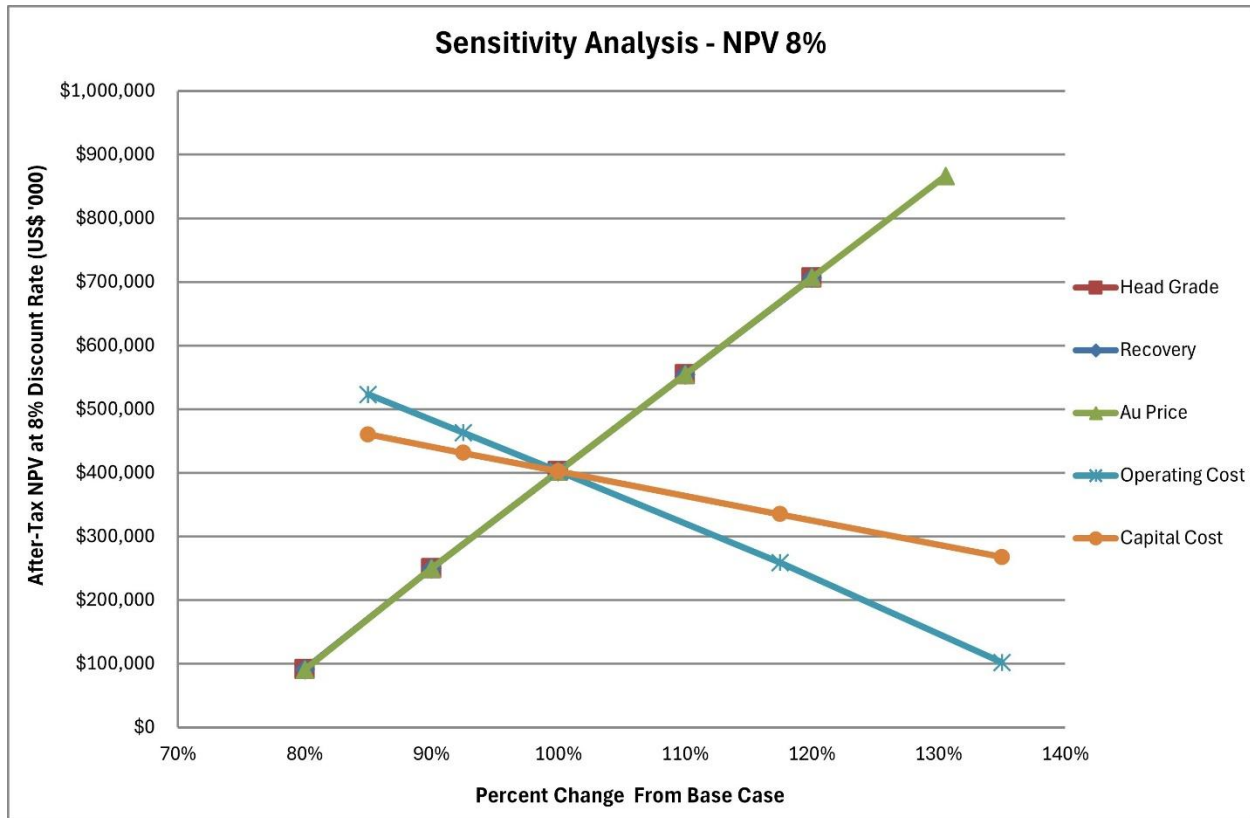
Variance	Head Grade (g/t Au)	NPV at 8% (US\$ 000)
80%	0.21	91,329
90%	0.23	249,814
100%	0.26	402,353
110%	0.28	554,310
120%	0.31	706,171



Variance	Recovery (% Au)	NPV at 8% (US\$ 000)
80%	60.7%	91,329
90%	68.2%	249,814
100%	75.8%	402,353
110%	83.4%	554,310
120%	91.0%	706,171
Variance	Metal Prices (US\$/oz Au)	NPV at 8% (US\$ 000)
80%	\$2,880	90,637
90%	\$3,240	249,505
100%	\$3,600	402,353
110%	\$3,960	554,614
131%	\$4,700	866,553
Variance	Operating Costs (US\$/t)	NPV at 8% (US\$ 000)
85%	\$11.07	523,205
93%	\$12.05	462,780
100%	\$13.03	402,353
118%	\$15.31	259,020
135%	\$17.59	102,091
Variance	Capital Costs (US\$ 000)	NPV at 8% (US\$ 000)
85%	\$506,652	460,155
93%	\$551,357	431,254
100%	\$596,062	402,353
118%	\$700,372	334,916
135%	\$804,683	267,480



Figure 1-5: Base Case After-Tax Sensitivity Analysis



1.2.2 Alternative Case - Measured and Indicated Only

1.2.2.1 Economic Criteria

The Alternative Case assumes a production schedule based exclusively on Measured and Indicated Mineral Resources, resulting in a mineralized material inventory of 62.4 Mt and a projected mine life of seven years. A summary of the Measured and Indicated Only Case criteria is provided below.

1.2.2.1.1 Revenue

- Mine life: 7 years.
- 30,000 tpd mineralized material stacked (approximately 10.8 Mt per year), average stacked grade of 0.27 g/t Au and silver grade of 3.83 g/t Ag (ROM, crushed, and stockpile mine plan).
- Mine life averages 58,500 ounces per year of gold recovered and 200,000 ounces per year of silver recovered from the mine plan, with LOM stacked process gold recovery averaging 74.3% and silver recovery averaging 18.1%.
- Total 410 koz of gold recovered, and 1,396 koz of silver recovered over the LOM operation.
- Gold and silver payable at the refinery are assumed at 99.95% Au payable and 97% Ag payable



- Gold and silver prices are based on analyst consensus price forecasts from the end of March 2026. For the economic analysis was assumed:
 - o Y1: US\$4,000/oz Au and US\$59.00/oz Ag
 - o Y2 to Y7: US\$3,600/oz Au and US\$48.00/oz Ag
 - o Resulting in LOM net realized prices of:US\$3,622/oz Au and US\$48.00/oz Ag
- Net Smelter Return (NSR) includes doré refining, transport, and insurance costs.
- NSR royalty assumed at 3%. The property is subject to different royalties between 0.5% and 3%, and for modeling purposes was assumed at an overall 3%
- Revenue is recognized at the time of gold and silver production.
- Non-cash inventory adjustments are not included in the SLR cash flow model.
- LOM net revenue is US\$1,493 million (after royalty, and transportation, and refining charges).

Table 1-8: Sleeper Alternative Case Production Physicals Summary

Physicals	Value
Total Mineralized Material Stacked (kt)	62,447
Max Process Rate (tpd)	30,000
Au Head Grade (g/t)	0.27
Ag Head Grade (g/t)	3.83
Contained Au (koz)	552
Contained Ag (koz)	7,697
Average Recovery, Au	74.3%
Average Recovery, Ag	18.1%
Recovered Au (koz)	410
Recovered Ag (koz)	1,396
Payable Au (koz)	408
Payable Ag (koz)	1,354
Avg Annual Au Sales - LOM (koz / yr) – full production	64
Avg Annual Ag Sales - LOM (koz / yr) – Full production	218

1.2.2.1.2 Costs

- Pre-production period: assumes at 24 months (Year -1 to Year -2).
- Initial (Growth) and development capital costs total US\$335 million.¹
- Mine life sustaining capital totals US\$120 million

¹ Note that, in the Alternative Case, only in situ Measured and Indicated Mineral Resources are included in the mining inventory. The existing waste dumps are not included in the LOM plan for the Alternative Case because they are currently classified as Inferred Mineral Resources. As dewatering of the in situ Mineral Resources must start before mining, the rapid infiltration basins cost and the dewatering costs are Initial Capital Costs for the Alternative Case rather than Sustaining Capital as in the Base Case.



- Final reclamation costs from after year 7 total US\$18.7 million.
- Mine life capital totals US\$473 million.
- Average LOM operating cost is US\$11.87 per tonne stacked.
 - Open pit operating costs of US\$2.59 per tonne mined (US\$5.03 per tonne stacked). Includes out-of-scope mining operations.
 - Dewatering operating costs of US\$0.73 per tonne stacked.
 - Processing operating costs of US\$5.55 per tonne stacked.
 - Site services & general and administrative (G&A) costs of US\$5.6 million per year for years of full production (LOM average of US\$0.56 per tonne stacked).

1.2.2.1.3 Taxation and Royalties

The federal and state income taxes are summarized in Table 1-9.

Table 1-9: Federal and State Tax Summary

Tax Type	Rate
Federal Corporate Income Tax	21.0%
Nevada Corporate Income Tax	5.0% of federal taxable income
Royalties and Severance Fees	Based on ore extracted (state-regulated).

A total of five NSR royalties apply to future mineral production from portions of the Project. These royalties are summarized in Table 1-10.

Table 1-10: Royalties Summary

Royalty Holder	Royalty Terms
Snyder Syndicate	1% NSR on the 1,044 Sleeper Gold Mine claims (All claims, EXCEPT for ALL MIMI, ALL SP, AL SS, AND ALL BLUE.)
Franco-Nevada U.S. Corporation	2% NSR on minerals produced from all 2,474 claims
Evolving Gold / Quinton Hennigh	2% NSR royalty on all SS and all SP claims.
Dry Lake Placer Association	3% NSR on Dry Lake Placer claims
ICN Resources Ltd.	0.5% NSR on all SS and all SP claims; 1.5% NSR on all Blue claims

For the economic analysis and financial modeling purposes, an overall 3% NSR royalty rate was assumed over the LOM.

1.2.2.2 Cash Flow Analysis

SLR has prepared its own unlevered after-tax LOM cash flow model based on the information contained in this TRS to confirm the physical and economic parameters of the Project.

The Project's Alternative Case economics have been evaluated using the discounted cash flow method, considering annual processed tonnages and the associated gold and silver grades. The process gold and silver recoveries, gold and silver price forecasts, operating costs, refining



and transportation charges, royalties, and initial and sustaining capital expenditures were also considered.

The Project, as currently designed, has variations in the mining and processing amounts over its planned 7-year life. These variations are shown in Figure 1-6, Figure 1-7, and Figure 1-8.

Figure 1-6: Mine Production Profile by Material Movement – Alternative Case

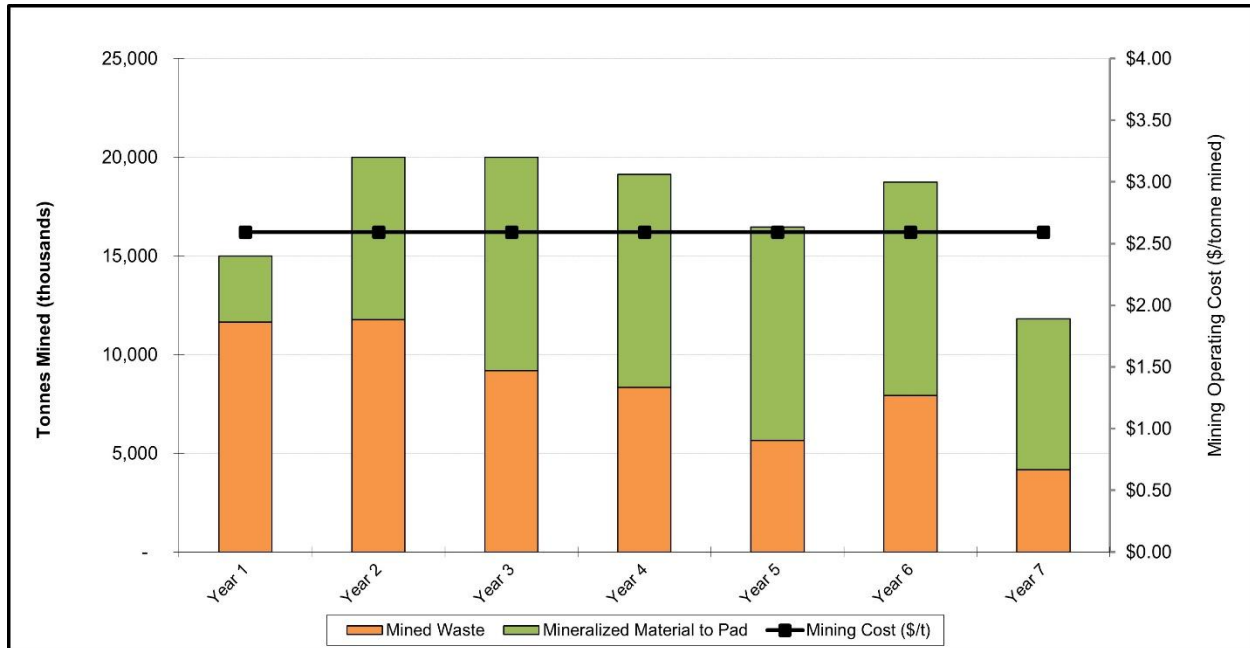


Figure 1-7: Process Production Profile and Head Grade – Alternative Case

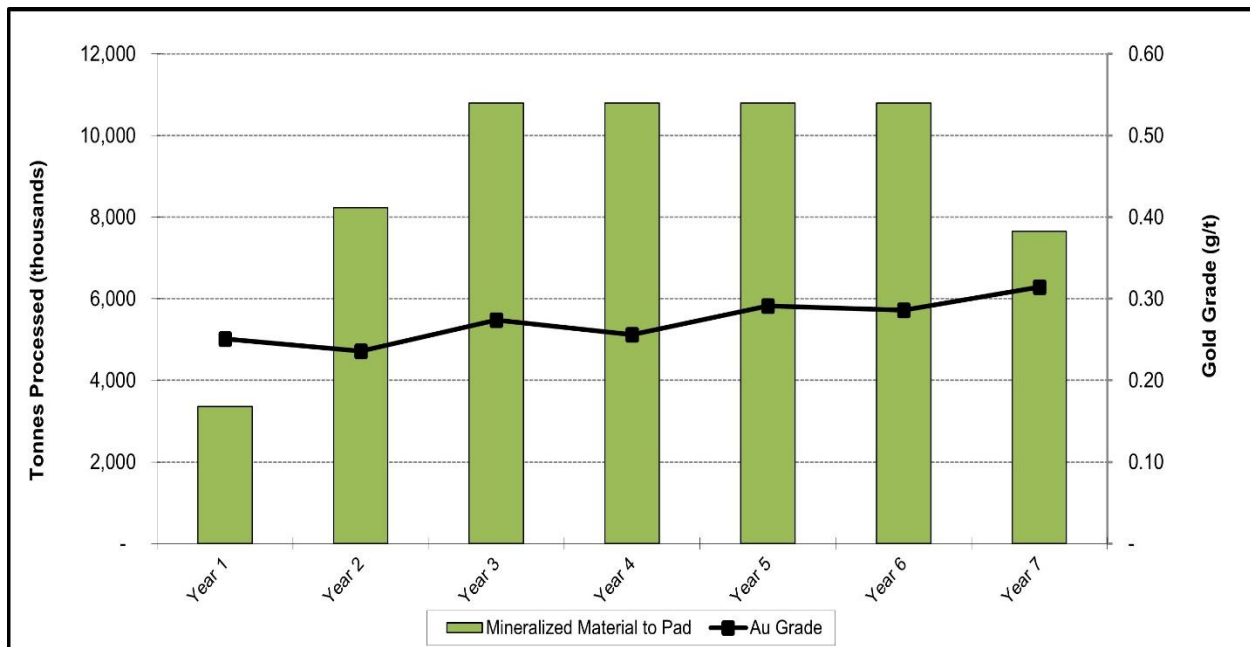
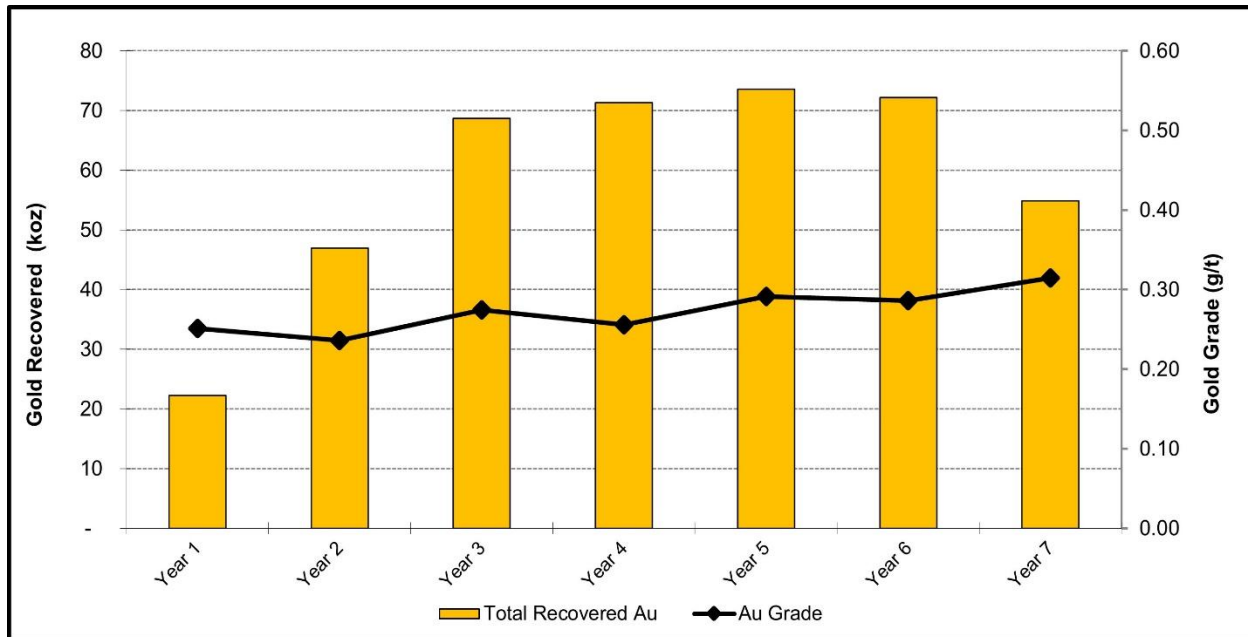


Figure 1-8: Annual Processing Gold Production and Head Grade Profile



The economic analysis demonstrates that the Project’s Mineral Resources have reasonable prospects for economic extraction, at the LOM net average realized prices of US\$3,622/oz Au and US\$48.40/oz Ag, with long-term prices of US\$3,600/oz Au and US\$48.00/oz Ag, and that further advancement of Project studies is warranted.

A base discount rate of 8% has been applied in this TRS for the Project. This rate is considered reasonable for evaluating a precious metals project at a preliminary level of project definition, such as Sleeper. Discounted present values of annual cash flows are summed to arrive at the Mine’s Base Case NPV.

Considering the Project’s Alternative Case on a stand-alone basis, the Project’s pre-tax NPV at an 8% discount rate is approximately US\$59 million, and the pre-tax internal rate of return (IRR) is approximately 11.5%. The Project’s after-tax NPV at an 8% discount is approximately US\$31 million, the after-tax IRR is approximately 9.9%, and the payback period is approximately 4.9 years from the start of production.

The LOM undiscounted pre-tax cash flow totals approximately US\$279 million, and the LOM undiscounted after-tax cash flow totals approximately US\$232 million.

The Project’s after-tax free cash flow profile and gold payable metal per year are presented in Figure 1-9.



Figure 1-9: Alternative Case Project After-Tax Metrics Summary

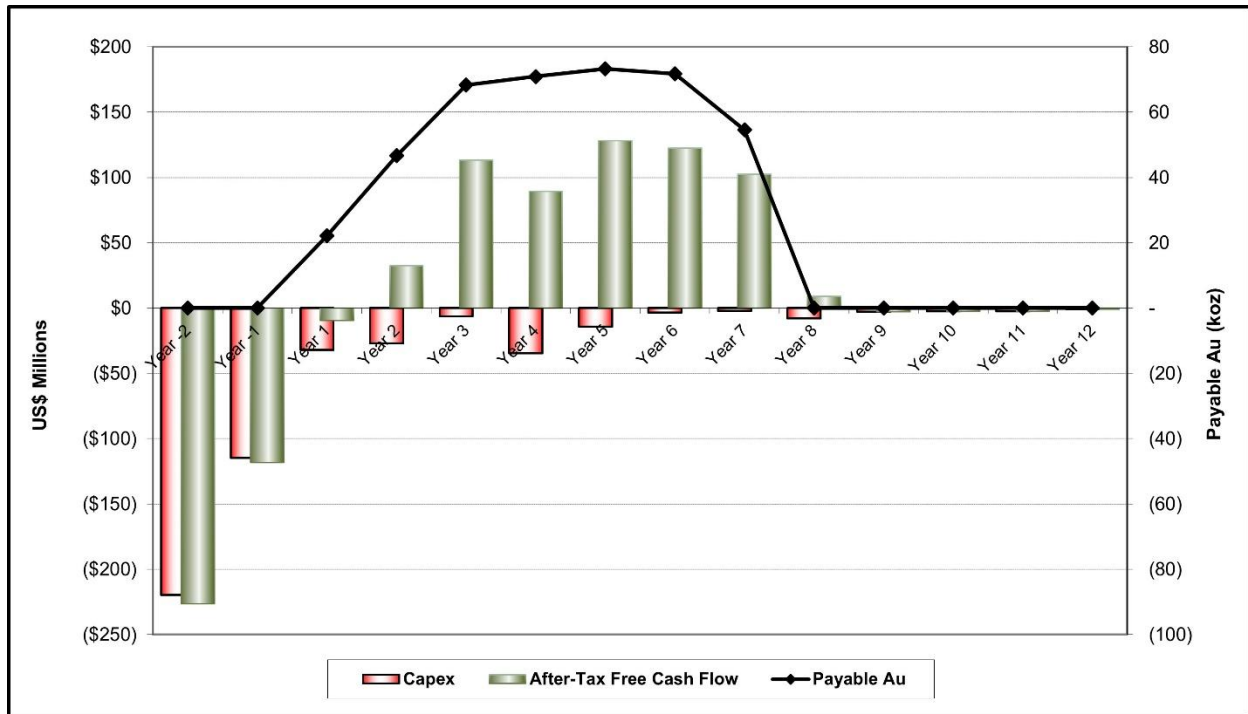


Table 1-11 shows the LOM total metrics for the Project’s Alternative Case. The full annual cash flow model is presented in Appendix 2.

Table 1-11: Total Life of Mine Metrics – Alternative Case (Measured and Indicated Only)

Item	Units	Base Case Values
Realized Market Prices		
Au Price	US\$/oz	\$3,622
Ag Price	US\$/oz	\$48.40
Payable Gold	koz	408
Payable Silver	koz	1,354
Total Gross Revenue	US\$ million	1,542
Mining Cost	US\$ million	(314)
Dewatering Costs	US\$ million	(45)
Process Cost	US\$ million	(347)
G & A Cost	US\$ million	(35)
Refining/Freight	US\$ million	(3)
Royalties	US\$ million	(46)
Total Operating Costs	US\$ million	(790)
Operating Margin (EBITDA)	US\$ million	752
Federal Income Tax	US\$ million	(12)



Item	Units	Base Case Values
State Tax - Nevada Mining Tax	US\$ million	(34)
Working Capital	US\$ million	0
Operating Cash Flow	US\$ million	705
Development (Initial) Capital	US\$ million	(335)
Sustaining Capital	US\$ million	(120)
Closure/Reclamation Capital	US\$ million	(19)
Total Capital	US\$ million	(473)
Pre-tax Free Cash Flow	US\$ million	279
Pre-tax NPV @ 5%	US\$ million	124
Pre-tax NPV @ 8%	US\$ million	59
Pre-Tax IRR	%	11.5%
Pre-Tax Payback	years	4.7
After-tax Free Cash Flow	US\$ million	232
After-tax NPV @ 5%	US\$ million	91
After-tax NPV @ 8%	US\$ million	31
After-Tax IRR	%	9.9%
After-Tax Payback	years	4.9
Note:	Numbers may not add due to rounding.	

The Project's World Gold Council Adjusted Operating Cost (AOC) net of Ag by-product credits is US\$1,778/oz Au payable. The mine life sustaining capital costs are US\$339/oz Au payable, for an All-in Sustaining Cost (AISC) net of Ag by-products credits of US\$2,117/oz Au payable.

The average annual gold sales during operations are approximately 64,267 payable ounces. Table 1-12 shows the AISC build-up.

Table 1-12: Alternative Case All-in Sustaining Costs Composition

Item	Total LOM (\$ million)	Unit Cost (\$/oz Au)
Mining	314	770
Dewatering	45	111
Process	347	850
Site G&A	35	86
Subtotal Site Costs	741	1,817
Refining/Freight	3	8



Item	Total LOM (\$ million)	Unit Cost (\$/oz Au)
Mining Royalties	46	113
Total Cash Costs before by-product credits	790	1,938
Ag By-Product Credit	(65)	(161)
Total Cash Costs net of by-product credits	725	1,778
Sustaining Capital Cost	120	293
Closure/Reclamation Costs	19	46
Total Sustaining Costs	138	339
Total All-in Sustaining Costs	863	2,117

Note: Numbers may not add due to rounding.

1.2.2.3 Sensitivity Analysis

The project's Alternative Case risks can be identified in both economic and non-economic terms. Key economic risks were examined by running cash flow sensitivities:

- Metal prices
- Head grade
- Metallurgical Recovery
- Operating costs
- Pre-production and sustaining capital costs

Where possible, the after-tax NPV 8% sensitivities relative to the Alternative Case have been calculated for -20% to +20% variations in head grade and recovery, and -20% to +30% in metal prices. Operating and capital cost sensitivities have been calculated at -15% to +35% variations. The sensitivities are shown in Table 1-13 and Figure 19-10.

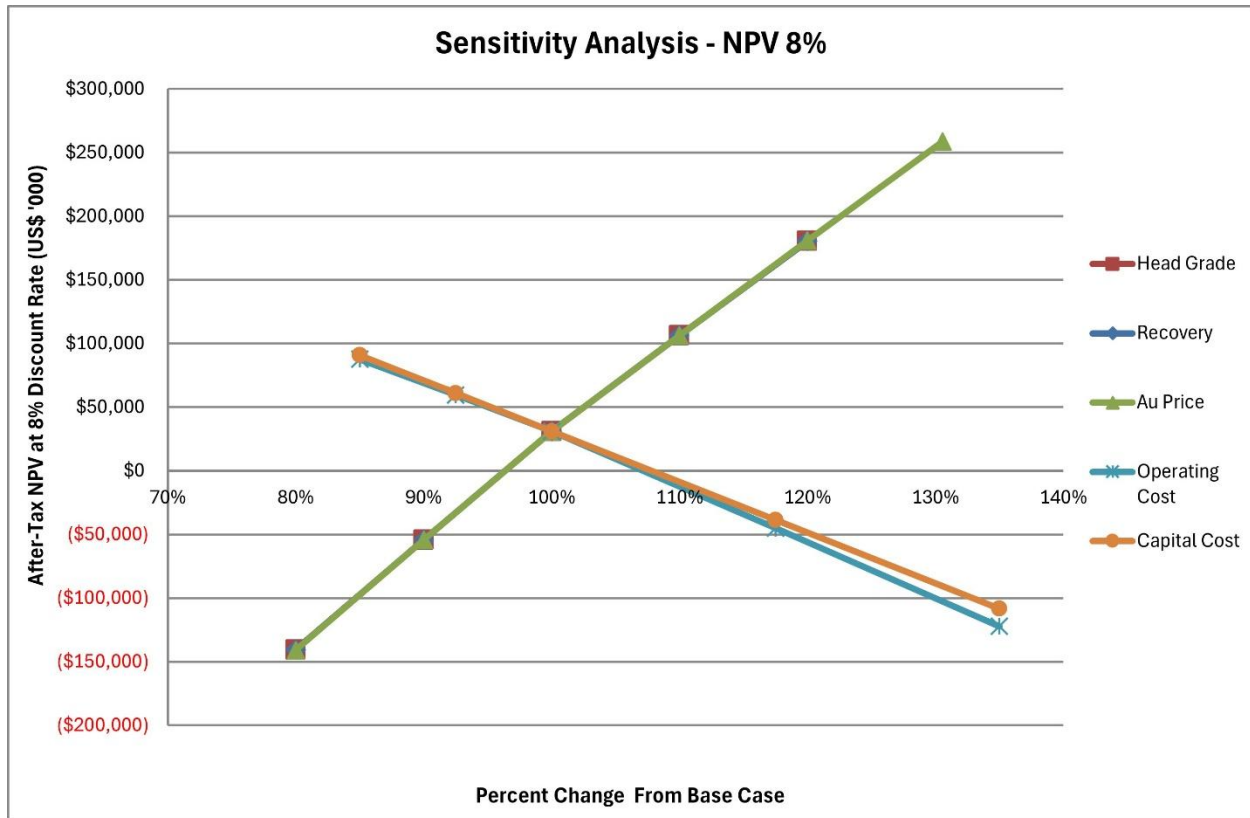


Table 1-13: Alternative Case After-Tax Sensitivity Analyses

Variance	Head Grade (g/t Au)	NPV at 8% (US\$000)
80%	0.22	(140,512)
90%	0.25	(54,187)
100%	0.27	31,106
110%	0.30	106,275
120%	0.33	180,559
Variance	Recovery (% Au)	NPV at 8% (US\$000)
80%	59.4%	(140,512)
90%	66.9%	(54,187)
100%	74.3%	31,106
110%	81.7%	106,275
120%	89.2%	180,559
Variance	Metal Prices (US\$/oz Au)	NPV at 8% (US\$000)
80%	\$2,880	(140,868)
90%	\$3,240	(54,363)
100%	\$3,600	31,106
110%	\$3,960	106,424
131%	\$4,700	258,552
Variance	Operating Costs (US\$/t)	NPV at 8% (US\$000)
85%	\$10.09	87,662
93%	\$10.98	59,481
100%	\$11.87	31,106
118%	\$13.94	(44,879)
135%	\$16.02	(122,212)
Variance	Capital Costs (US\$000)	NPV at 8% (US\$000)
85%	\$401,924	90,847
93%	\$437,387	60,977
100%	\$472,851	31,106
118%	\$555,600	(38,591)
135%	\$638,349	(108,288)



Figure 1-10: Alternative Case After-Tax Sensitivity Analysis



1.3 Technical Summary

1.3.1 Property Description

The Sleeper Gold Mine is in Humboldt County in north-central Nevada, approximately 42 km (26 mi) northwest of the city of Winnemucca, Nevada. The Project is situated within Desert Valley along the western flank of the Slumbering Hills within the Basin and Range physiographic province. The property includes the historical Sleeper open pit, associated waste rock storage facilities, former process plant areas, and surrounding exploration targets.

The Project is being evaluated as a restart operation focused on processing of existing waste rock dumps and mining of in situ oxide and mixed mineralized material within and adjacent to the historical pit. These materials are considered suitable for heap leach processing with Merrill-Crowe recovery.

1.3.2 Land Tenure

The Sleeper property consists of a block of unpatented lode mining claims, together with associated surface rights covering portions of Townships 36 through 40 North and Ranges 34 and 35 East, Mount Diablo Base and Meridian, Humboldt County, Nevada.

The property comprises approximately 2,474 unpatented mining claims, approximately 18,178 hectares (44,917 acres). The claims are held by Paramount Gold Nevada Corp (Paramount Gold), through its wholly owned subsidiaries of Sleeper Mining Company LLC and South



Sleeper Mining Company LLC. All claims are in good standing with the U.S. Bureau of Land Management and Humboldt County as of the date of this report.

1.3.3 History

The Sleeper deposit was discovered in the early 1980s and subsequently developed by AMAX Gold Inc. Mining operations commenced in 1986 and continued through 1996.

During this period, the Sleeper mine produced approximately 1.66 million ounces of gold and approximately 2.3 million ounces of silver from the open pit mining operations. Ore was processed through both conventional milling and heap leach processing circuits. Following the closure of mining operations in 1996, the site underwent reclamation activities; however, substantial volumes of mineralized material remain within existing waste rock dumps and oxide mineralized zones adjacent to the pit.

Subsequent exploration and technical studies conducted by Paramount Gold and previous operators have identified the potential to reprocess historical surface materials and recover additional gold from remaining oxide and mixed mineralization.

1.3.4 Geological Setting, Mineralization, and Deposit

The Sleeper deposit is a low-sulfidation epithermal gold-silver system hosted within Miocene volcanic rocks typical of the northern Nevada volcanic field. Mineralization occurs within a sequence of rhyolitic flows, volcanic breccias, and ash-flow tuffs that have been affected by hydrothermal alteration and silicification.

Gold mineralization occurs as disseminated and fracture-controlled mineralization associated with hydrothermal brecciation, silicification, and quartz-adularia veining. Near-surface oxidation of sulfide minerals has produced oxide and mixed mineralization amenable to cyanide heap-leach processing.

1.3.5 Exploration

Exploration activities at the Sleeper property have included geological mapping, geochemical sampling, geophysical surveys, and diamond and reverse circulation drilling. Since mine closure, exploration has focused on delineating oxide and mixed mineralization and on evaluating the gold content of existing waste rock dump, heap leach pads, and tailings. Drilling has identified gold mineralization in oxide and mixed zones, and sampling of existing waste rock dumps indicates that portions of this material contain measurable gold.

1.3.6 Mineral Resource Estimates

The Mineral Resource estimate for the Sleeper Gold Mine (Table 1-14) was developed using a three-dimensional block modeling approach incorporating validated drilling data, geological and oxidation domain modeling, compositing, grade capping, and domain-controlled interpolation. The estimate has been independently reviewed by the SLR QP and is compliant with SEC Regulation S-K 1300 and prepared in accordance with CIM (2019) Best Practice Guidelines. Mineral Resources include both in situ mineralization constrained within an optimized open-pit shell demonstrating RRPEE and surface materials, including waste rock dumps, heap leach pads, and tailings storage facilities. The estimate is based on appropriate mining, processing, metallurgical, and economic assumptions and supersedes prior disclosures for the Project.

Measured Mineral Resources total 5.5 Mt at 0.492 g/t Au and 3.487 g/t Ag, containing 0.09 Moz Au and 0.62 Moz Ag. Indicated Mineral Resources total 179.2 Mt at 0.330 g/t Au and



3.842 g/t Ag, containing 1.90 Moz Au and 22.1 Moz Ag. Measured and Indicated Mineral Resources combined total 184.7 Mt at 0.335 g/t Au and 3.832 g/t Ag, containing 1.99 Moz Au and 22.8 Moz Ag, with average metallurgical recoveries of approximately 70.0% for Au and 7.5% for Ag.

Inferred Mineral Resources total 238.0 Mt at 0.301 g/t Au and 3.403 g/t Ag, containing 2.30 Moz Au and 26.0 Moz Ag, including 89.7 Mt of surface materials (waste rock dumps, heap leach pads, and tailings storage facilities) at 0.327 g/t Au and 4.738 g/t Ag.



Table 1-14: Summary of Mineral Resources Estimate – April 29, 2026

Category	Tonnage (000 t)	Grade (g/t Au)	Grade (g/t Ag)	Contained Metal (000 oz Au)	Contained Metal (000 oz Ag)	Metallurgical Au Recovery (%)	Metallurgical Ag Recovery (%)
Measured Oxide/Mixed Pit (non-sulfide)	2,004	0.293	3.019	19	195	75.2%	17.1%
Measured Oxide/Mixed Pit (sulfide)	178	0.316	4.307	2	25	70.6%	0.0%
Measured Sulfide Pit	3,347	0.621	3.724	67	401	66.5%	0.0%
Total Measured In Situ	5,528	0.492	3.487	88	620	69.8%	6.2%
Indicated Oxide/Mixed Pit (non-sulfide)	77,899	0.261	3.613	653	9,049	74.2%	17.3%
Indicated Oxide/Mixed Pit (sulfide)	15,941	0.328	4.934	168	2,529	68.7%	0.0%
Indicated Sulfide Pit	85,336	0.393	3.848	1,078	10,558	66.5%	0.0%
Total Indicated In Situ	179,176	0.330	3.842	1,900	22,135	70.1%	7.5%
Total Measured + Indicated In Situ	184,704	0.335	3.832	1,987	22,755	70.0%	7.5%
Inferred Dumps	46,893	0.279	1.941	420	2,927	77.1%	44.6%
Inferred Heap Leach	31,600	0.301	8.363	306	8,497	40.0%	0.0%
Inferred TSF	11,165	0.599	6.221	215	2,233	50.1%	0.0%
Total Inferred Surface	89,658	0.327	4.738	942	13,657	60.6%	23.3%
Inferred Oxide/Mixed Pit (non-sulfide)	48,656	0.235	2.384	367	3,729	76.6%	14.4%
Inferred Oxide/Mixed Pit (sulfide)	4,960	0.286	3.543	46	565	68.9%	0.0%
Inferred Sulfide Pit	94,761	0.311	2.657	948	8,095	66.5%	0.0%
Total Inferred In Situ	148,377	0.285	2.597	1,361	12,390	69.9%	4.7%
Total Inferred Surface + In Situ	238,035	0.301	3.403	2,303	26,047	97.9%	8.8%



Notes:

1. The definitions for Mineral Resources in S-K 1300 were followed for Mineral Resources
2. The Mineral Resource estimate is reported on a 100% ownership basis.
3. The point of reference for the Mineral Resource is before the crusher (in situ).
4. Open Pit Mineral Resources are reported at a cut-off grade ranging from 0.074 g/t to 0.217 g/t Au, depending on area and constrained by a preliminary optimized pit shell with a pit slope angle of 45° for rock and 22° for alluvium and a bench height of 10 m.
5. The optimized pit shell and cut-off grades were generated by assuming metallurgical gold recovery ranging from 63.7% to 85.0% and silver recoveries ranging from 0.0% to 54.6%, standard treatment and refining charges, mining costs of US\$2.40/t moved for open pit, processing costs of \$5.51/t oxide/mixed and \$10.44 sulfide processed, and general and administrative costs of \$0.46/t processed
6. Minimal mining width was 60 m for oxide/mixed material and 20 m for sulfide material
7. Mineral Resources are estimated using a long-term gold price of US\$3,100 per ounce
8. Bulk density ranges from 1.5 t/m³ in the tailings storage area to 2.7 t/m³ for in situ material
9. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.
10. Numbers may not add due to rounding.



1.3.7 Mineral Reserve Estimates

There are no defined Mineral Reserves for the Sleeper Gold Mine as of the date of this TRS.

1.3.8 Mining Methods

Mining operations are planned as a conventional open pit operation using drill, blast, load, and haul methods on benches. Mining will be performed by a third-party mining contractor. The mining fleet is expected to consist of diesel-powered hydraulic excavators and/or front-end loaders, supported by haul trucks typical of modern open pit mining operations in Nevada. Mining activities will include both the rehandling of existing waste rock dump material and the extraction of in situ oxide and mixed mineralized material considered amenable to heap leaching and Merrill-Crowe recovery.

The Initial Assessment (IA) economic analysis considers only leachable mineralized material, including oxide and mixed material within the pit limits and existing waste rock dump material. Existing waste rock dump material is currently estimated at approximately 47 Mt grading approximately 0.28 g/t gold, while in situ oxide and mixed mineralized material totals approximately 129 Mt grading approximately 0.25 g/t gold. Sulfide mineralization, as well as material contained within the tailings storage facility (TSF) and heap leach pad (HLP), demonstrates RPEE; however, additional metallurgical testing, engineering studies, environmental review, and economic evaluation are required before these materials can be considered for inclusion in the IA economic analysis.

The Base Case mine plan considers Measured, Indicated, and Inferred Mineral Resources. Inferred Mineral Resources account for approximately 55% of the total mining inventory and are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorized as Mineral Reserves. There is no certainty that the results of the Base Case economic analysis will be realized.

An Alternative Case was also evaluated comprising Measured and Indicated Mineral Resources only, excluding all Inferred Mineral Resources from the mine plan and economic analysis.

1.3.9 Processing and Recovery Methods

Processing of mined material is planned using conventional crushing, agglomeration, and cyanide heap leach processing, followed by Merrill-Crowe zinc precipitation for recovery of gold and silver.

The conceptual processing rate for the operation is approximately 30,000 tpd. Heap leach processing will involve stacking crushed material on lined leach pads and applying cyanide solution to dissolve precious metals.

To date, metallurgical test work at Sleeper has included historical bottle roll and column leach testing on oxide, mixed, waste rock dump, and selected sulfide materials; flotation testing on sulfide and existing tailings composites; and later bio-oxidation, pressure oxidation, mineralogical, and comminution testing on selected refractory or sulfide-bearing materials. Overall, the work supports heap leach evaluation for oxide, mixed, and waste materials, and flotation-based evaluation for tailings, HLP, and sulfide materials.

For the oxide, mixed, and waste rock dump material groups included in the heap leach case, applied recoveries range from 65.0% Au to 83.9% Au and 8.1% Ag to 54.6% Ag. For the existing HLP and tailings, and sulfide material groups evaluated under the flotation and toll-milling case, applied gold recoveries range from 50.0% Au to 71.2% Au. No silver recovery is



applied to the flotation case at this stage, and silver remains upside potential pending additional metallurgical and commercial evaluation.

For oxide, mixed, and waste rock dump material within the Measured and Indicated Resource categories, estimated recoveries of approximately 70% Au and 7.5% Ag were applied.

1.3.10 Infrastructure

Existing infrastructure at the Sleeper property includes exploration offices, equipment maintenance shops, water management ponds, monitoring wells, and a network of access roads constructed during historical mining operations.

Electrical power is available via an existing 120-kV transmission line serving the region. Water supply for operations will be sourced from groundwater within the Desert Valley hydrographic basin under existing water rights.

1.3.11 Market Studies

Gold and silver produced from the proposed operation would be recovered as doré bars through the Merrill-Crowe process and transported to third-party refineries for final metal recovery.

Gold and silver are internationally traded commodities with established global markets. Market studies are therefore not considered necessary for the Project's evaluation.

1.3.12 Environmental Studies, Permitting and Plans, Negotiations, or Agreements with Local Individuals or Groups

Historical mining operations at Sleeper were conducted under permits issued by federal and state regulatory agencies, including the U.S. Bureau of Land Management and the Nevada Division of Environmental Protection.

Future development of the Project will require updated environmental studies, permitting, and regulatory approvals associated with the restart of mining operations. These will include updates to existing permits and approvals for mine operations, water management, and heap leach processing facilities.

The project area is in a sparsely populated region with limited nearby residential development. Consultation with regulatory agencies and local stakeholders will continue throughout the permitting process.

1.3.13 Capital and Operating Cost Estimates

The capital and operating cost estimates for the IA were developed by SLR using a combination of first-principles estimating, benchmarking against comparable operations, and available contractor quotations, with all costs expressed in Q2 2026 US dollars and based on metric tonnes. Consistent with AACE International Class 5 scoping-level estimates, the cost estimates reflect a preliminary level of engineering definition with an expected accuracy range of approximately $\pm 50\%$. The capital costs include a 25% contingency.

For the Base Case, total LOM capital costs are estimated at approximately \$596 million, including \$201 million in initial growth and development capital, \$343 million in sustaining capital, and approximately \$52 million allocated for reclamation and closure activities. Initial capital requirements are reduced through the use of contract mining and phased heap leach pad development. Sustaining capital is dominated by pit dewatering expenditures totaling approximately \$139 million over the LOM. Additional sustaining expenditures are associated



with staged heap leach pad expansions occurring in years 6, 9, and 12, as well as ongoing infrastructure and indirect costs.

Average LOM operating costs are estimated at approximately \$13.03/t processed, including mining, dewatering, processing, and general and administrative costs. Open pit mining costs are estimated at \$2.40/t mined, with total mining costs averaging \$6.37/t processed after accounting for waste movement, rehandling requirements, and out-of-scope contractor allowances. Processing costs are estimated at \$5.55/t processed and reflect a relatively simple crushing, heap leach, and Merrill-Crowe flowsheet.

Primary consumable costs include power at approximately \$0.085/kWh based on NV Energy Northern Nevada industrial tariffs, off-highway diesel at approximately \$3.50 per US gallon, propane at approximately \$2.25 per US gallon, sodium cyanide at approximately \$2,650 per tonne delivered, and quicklime at approximately \$375 per tonne.

The proposed operation is expected to employ approximately 210 to 220 personnel during steady-state operations using a conventional four-crew, 12-hour shift rotation to support continuous 24-hour-per-day mining and processing activities. Staffing requirements are moderated by the use of large 150 t class haul trucks, contractor mining, and a relatively simple processing flowsheet; however, additional personnel are required to support significant pit dewatering activities. Approximately 75% of the workforce is expected to reside in Humboldt County, Nevada, with the balance drawn from surrounding regions on a drive-in/drive-out basis without the use of an on-site accommodation camp.



2.0 Introduction

SLR International Corporation (SLR) was retained by Paramount Gold Nevada Corp. (PGN, Paramount Gold, or the Company) to prepare an independent Technical Report Summary (TRS) on the Sleeper Gold Mine (Sleeper or the Project). The purpose of this TRS is to provide an Initial Assessment to support Mineral Resource disclosure. This TRS conforms to the United States Securities and Exchange Commission's (SEC) *Modernized Property Disclosure Requirements for Mining Registrants* as described in Subpart 229.1300 of Regulation S-K, Disclosure by Registrants Engaged in Mining Operations (S-K 1300) and Item 601(b)(96) Technical Report Summary.

Paramount Gold is a U.S.-domiciled precious metals exploration and development company engaged in the acquisition, exploration, and development of gold and silver projects in the United States. The company's principal assets include the Sleeper Gold Mine in Nevada and the Grassy Mountain Gold Project in Oregon, as well as additional exploration properties in the western United States. Paramount Gold is publicly listed on the NYSE exchange under the ticker symbol PZG and maintains its corporate offices in Winnemucca, Nevada.

Paramount Gold holds a 100% interest in the Sleeper Gold Mine, which includes the historical Sleeper open-pit gold mine and a large surrounding claim block totaling 2,474 unpatented mining claims covering approximately 44,917 acres (approximately 18,178 hectares) in Humboldt County, Nevada. The Sleeper mine was operated by AMAX Gold Inc. (AMAX) from 1986 through 1996, producing approximately 1.66 million ounces (Moz) of gold and 2.3 Moz of silver from open-pit mining and heap leaching and milling operations.

The Project is currently at the Initial Assessment (IA) stage, and as such, the level of engineering, geological definition, and metallurgical characterization remains preliminary. The Mineral Resources for the Project comprise in situ oxide and mixed material, in situ sulfide material, and material from existing waste rock dumps, heap leach pads (HLPs), and tailing storage facilities (TSFs). The development concept considered in the cash flow analysis presented in this TRS contemplates the restart of mining and processing operations with a focus on those Mineral Resources amenable to heap leaching, i.e., existing waste rock dumps and in situ oxide and mixed mineralized material. Additional work is required to develop the cash flow analysis for the sulfide Mineral Resources, including the heap leach and tailings material.

The existing waste rock dumps were generated during prior mining operations conducted under substantially lower gold prices, which led to the application of higher cut-off grades (COGs) at the time of mining. Consequently, material that was classified as waste under historical economic conditions contains grades that are potentially economic under current or reasonably foreseeable gold price assumptions and processing technologies. This reclassification to Mineral Resources forms a key component of the Project's economic rationale.

To support this evaluation, the waste rock dumps have been subject to initial drilling, sampling, and assaying programs, supplemented by preliminary metallurgical test work. These programs have been designed to characterize the grade distribution, material variability, and metallurgical response of the dump material, including leachability and recovery potential. While these datasets provide an important foundation for the current assessment, they remain limited in scope and density relative to that required for higher-confidence classifications, and additional work will be required to support future Mineral Resource estimation, metallurgical modeling, and process design.

In parallel, the Project concept includes recovery of in situ oxide and mixed mineralized material remaining in the vicinity of the historical pit. These materials are considered amenable to



conventional surface mining methods and heap leach processing, consistent with prior operations at Sleeper, although additional drilling, metallurgical testing, and engineering studies will be required to confirm recoveries, processing parameters, and economic viability.

Overall, the Project represents a brownfields redevelopment opportunity, leveraging existing site disturbance, historical data, and previously mined material inventories; however, given the early stage of evaluation, all assumptions related to mineralization, processing performance, and economic outcomes should be considered preliminary and subject to refinement through subsequent phases of study. The development concept assumes a nominal processing rate of approximately 30,000 tonnes per day (tpd), utilizing conventional open pit mining, crushing and agglomeration, cyanide heap leaching, and Merrill-Crowe zinc precipitation to recover gold and silver.

The Base Case economic analysis presented in this TRS evaluates the potential economic viability of processing Measured, Indicated, and Inferred Mineral Resources. The Base Case mining inventory comprises the following:

- Approximately 47 million tonnes (Mt) of waste rock dump material, classified as Inferred Mineral Resources, grading approximately 0.28 g/t gold (Au)
- In situ oxide and mixed mineralized material including approximately 2 Mt Measured Resources grading 0.29 g/t Au, 78 Mt Indicated Resources grading 0.26 g/t Au, and 49 Mt Inferred Resources grading 0.24 g/t Au.

The Base Case production schedule includes approximately 55% of Inferred Resources as part of the economic analysis. An Alternative Case was considered that included only in situ Measured and Indicated Resources in the economic analysis.

Unlike Mineral Reserves, Mineral Resources do not have demonstrated economic viability. The economic analysis contained in this TRS is preliminary in nature and is based, in part, on Inferred Mineral Resources that are considered too speculative geologically to have modifying factors applied to them that would enable them to be categorized as Mineral Reserves. There is no certainty that economic forecasts on which this Initial Assessment is based will be realized.

Terms of Reference and Purpose

This Technical Report Summary has been prepared for Paramount Gold Nevada Corp. in accordance with the requirements of Regulation S-K 1300 for disclosure of Mineral Resources, exploration results, and initial assessments for mining properties.

The purposes of this TRS are listed:

- Summarize the geology, mineralization, exploration history, and technical studies conducted on the Project.
- Present the results of an IA evaluating the potential economic viability of processing existing waste rock dump material and in situ oxide and mixed mineralization.
- Provide disclosure of Mineral Resources, mining methods, processing methods, infrastructure, and economic assumptions consistent with S-K 1300 disclosure standards.

This TRS supersedes all previously filed TRS for the Sleeper Gold Mine and is an update to the most recent TRS titled, "Technical Report Summary for the Sleeper Gold-Silver Project, Humboldt County, Nevada, USA" with an effective date of June 30, 2023, prepared for Paramount Gold Nevada Corp. by RESPEC Company LLC., dated August 31, 2023 (RESPEC 2023).



2.1 Site Visits

The Qualified Persons (QPs) responsible for the preparation of this TRS include professionals from SLR with relevant expertise in geology, mining engineering, metallurgy, and economic evaluation.

Personal inspections of Sleeper were completed by SLR QPs on April 2, 2026, and May 17, 2024. During the April 2, 2026, site visit, the SLR mining and geology QPs reviewed the historical mine site, surface geology, waste rock dump areas, exploration facilities, and infrastructure relevant to the Project evaluation. During the May 17, 2024, site visit, the SLR heap leach QP reviewed the historical mine site, waste rock dump areas, exploration facilities, and infrastructure relevant to the Project evaluation. The Environmental QP has visited the site several times over the past five years, including the most recent visit on January 27, 2026, at which time all permitted facilities were reviewed.

2.2 Sources of Information

During the preparation of this TRS, discussions were held with personnel from PGN:

- Rachel Goldman, CEO, Paramount Gold Nevada Corp.
- Michael McGinnis, CPG, Owner's Representative, Paramount Gold Nevada Corp.
- Carlo Buffone, CFO, Paramount Gold Nevada Corp.

This TRS has been prepared using information and data obtained from multiple sources, including:

- Historical technical reports and feasibility studies for the Sleeper Gold Mine
- Company reports, internal studies, and databases provided by Paramount Gold Nevada Corp.
- Geological, metallurgical, and engineering studies prepared by previous operators and consultants
- Publicly available technical publications and regulatory filings
- Site visits and technical discussions with Paramount Gold personnel

Where appropriate, data sources are referenced within the relevant sections of this report.

The documentation reviewed and other sources of information are listed at the end of this TRS in Section 24.0 References.



2.3 List of Abbreviations

Units of measurement used in this TRS conform to the metric system, unless otherwise noted. All currency in this TRS is US dollars (US\$) unless otherwise noted.

μ	micron	kVA	kilovolt-amperes
μg	microgram	kW	kilowatt
a	annum	kWh	kilowatt-hour
A	ampere	L	litre
bbl	barrels	lb	pound
Btu	British thermal units	L/s	litres per second
°C	degree Celsius	m	metre
C\$	Canadian dollars	M	mega (million); molar
cal	calorie	m ²	square metre
cfm	cubic feet per minute	m ³	cubic metre
cm	centimetre	MASL	metres above sea level
cm ²	square centimetre	m ³ /h	cubic metres per hour
d	day	mi	mile
dia	diameter	min	minute
dmt	dry metric tonne	μm	micrometre
dwt	dead-weight ton	mm	millimetre
°F	degree Fahrenheit	mph	miles per hour
ft	foot	MVA	megavolt-amperes
ft ²	square foot	MW	megawatt
ft ³	cubic foot	MWh	megawatt-hour
ft/s	foot per second	oz	Troy ounce (31.1035g)
g	gram	oz/st, opt	ounce per short ton
G	giga (billion)	ppb	part per billion
gal	US gallon	ppm	part per million
g/L	gram per litre	psia	pound per square inch absolute
gpm	US gallons per minute	psig	pound per square inch gauge
g/t	gram per tonne	RL	relative elevation
gr/ft ³	grain per cubic foot	s	second
gr/m ³	grain per cubic metre	st	short ton
ha	hectare	stpa	short ton per year
hp	horsepower	stpd	short ton per day
hr	hour	t	metric tonne
Hz	hertz	tpa	metric tonne per year
in.	inch	tpd	metric tonne per day
in ²	square inch	US\$	United States dollar
kcal	kilocalorie	V	volt
kg	kilogram	W	watt
km	kilometre	wmt	wet metric tonne
km ²	square kilometre	wt%	weight percent
km/h	kilometre per hour	yd ³	cubic yard
kPa	kilopascal	yr	year



3.0 Property Description

3.1 Location

The Sleeper Gold Mine, a material exploration property of Paramount Gold, is located in Desert Valley at the western base of the Slumbering Hills within the Awakening Mining District, Humboldt County, Nevada, United States. The Company holds the rights to explore, develop, and mine the property through its 100% ownership of unpatented lode mining claims (the Property). The Property lies approximately 42 kilometers (km) (26 miles [mi]) northwest of Winnemucca, Nevada, and is centered at approximately latitude 41°20'03" North and longitude 118°03'10" West. The location of the Property is illustrated in Figure 3-1 and is shown on the Jackson Well 7.5-minute quadrangle published by the United States Geological Survey. The main historical Sleeper mine workings are located near these coordinates.



Figure 3-1: Location Map



Source: SLR 2026.



3.2 Land Tenure

The Property comprises 2,474 unpatented federal lode mining claims covering approximately 18,178 hectares (approximately 44,917 acres) in Humboldt County, Nevada. The claims are administered by the U.S. Bureau of Land Management (BLM) under the provisions of the Mining Law of 1872. Paramount Gold Nevada Corp., through its wholly owned subsidiaries Sleeper Mining LLC and New Sleeper LLC, holds 100% ownership of the claims that make up the Project.

Ownership of unpatented mining claims conveys the right to explore, develop, and mine locatable minerals subject to compliance with federal and state regulations. The surface estate remains under the title of the United States Government and is managed by the BLM. Surface use associated with exploration and mining activities is subject to applicable environmental and land management regulations.

Paramount Gold’s latest Title Report was completed in December 2023, and the land position has not been altered since. The properties subject to this 2023 Title Report Update include all the Claims.

The Property consists of contiguous unpatented lode and placer mining claims covering portions of Sections 35 through 36 in Township 40 North, Range 34 East; Sections 3 through 10, 11, 14 through 23, and 25 through 36 in Township 40 North, Range 35 East; Sections 1 through 2, 11 through 14, 23 through 26, and 35 through 36 in Township 39 North, Range 34 East; Sections 1 through 12, 16 through 22, and 28 through 33 in Township 39 North, Range 35 East; Sections 1, 2, 11, and 12 in Township 38 North, Range 34 East; Sections 9, 16, 19 through 21, 28, and 32 through 34 in Township 38 North, Range 35 East; Sections 24, and 35 through 36 in Township 37 North, Range 34 East; Sections 1 through 5, 8, 9, 15 through 17, and 27 through 28 in Township 37 North, Range 35 East; Sections 2 through 3, in Township 36 North, Range 34 East, Mount Diablo Base and Meridian, Humboldt County, Nevada. Surface rights for the unpatented claims are owned by the United States Government.

3.2.1 Mining Claims

The Project consists of four primary claim groups totaling 2,474 unpatented lode mining claims. These claim groups were assembled through a series of acquisitions and claim-staking programs from 2010 to 2021.

Table 3-1: Sleeper – Summary of Claim Holdings

Claim Group (SUB CLAIM NAMES)	Number of Claims	Approximate Surface Area	
		(Hectares)	(Acres)
Sleeper Gold Mine (AW, CR, DAY, DRYLAKE, ELECTRUM, FREE GOLD, LAM, LLY, MORNING, MORNING STAR, NA, NEW ALMA, NEW EVENING, NEW SNOWSTORM, PDSL P, SK, SLEEPER, SS, VIRGINIA, YORK)	1,044	6,544	16,171
Dunes (Blue No., SP, SS)	394	2,997	7,405
Mimi (MIMI)	884	7,383	18,243
South Sleeper (RO, SH)	152	1,254	3,098
Total	2,474	18,178	44,917



Section 27.0 provides a complete list of individual mining claims that comprise the Property.

Federal and State Mining Law Framework

Federal laws governing mining activities on public lands in the United States are primarily contained in Title 30 of the United States Code (USC), “Mineral Lands and Mining,” and Title 43 of the United States Code, Chapter 35, “Federal Land Policy and Management Act” (FLPMA). Implementing regulations for these statutes are contained in Title 43 of the Code of Federal Regulations (CFR), “Public Lands.”

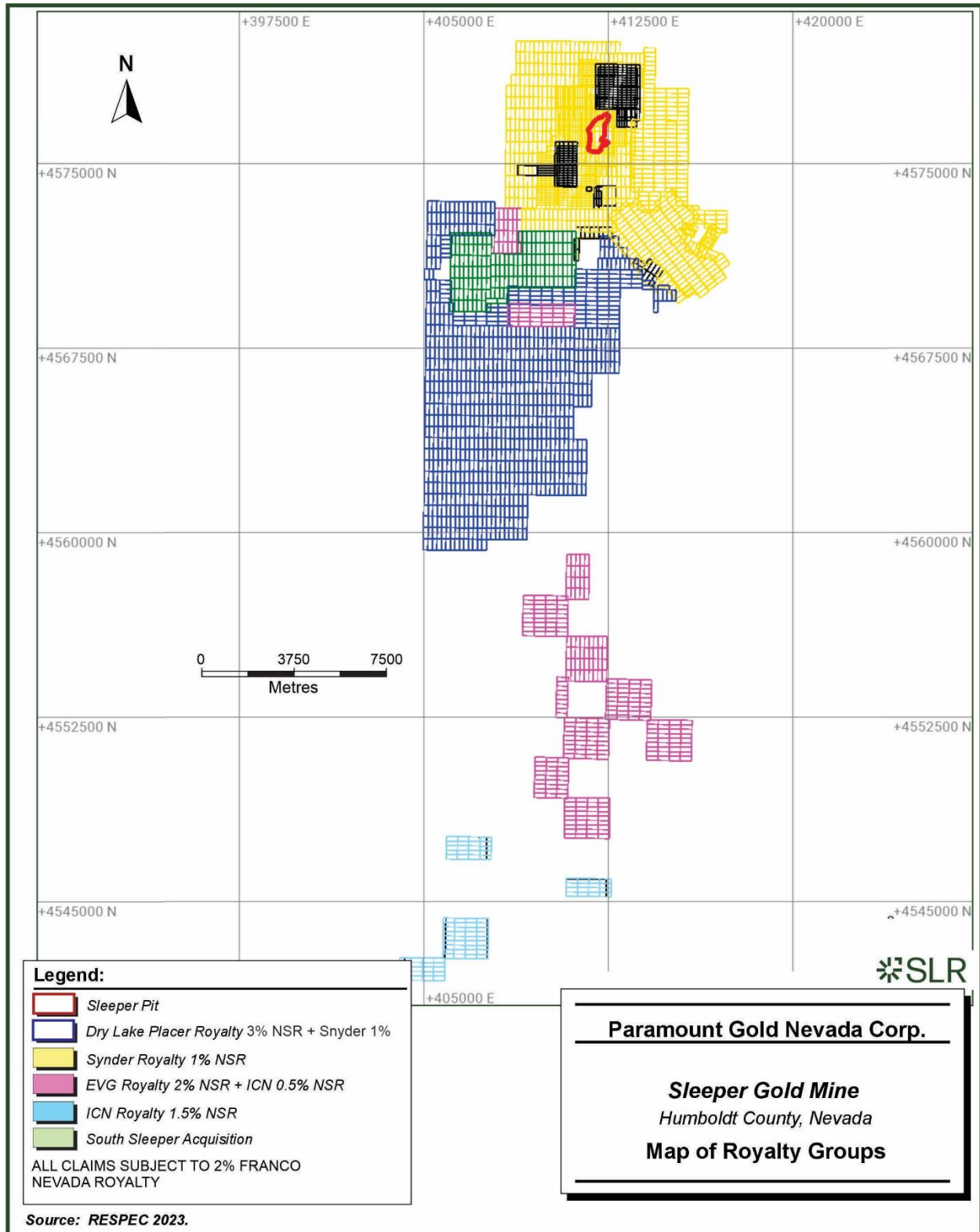
Nevada state laws applicable to mining operations are primarily contained in the Nevada Revised Statutes (NRS), particularly Chapters 512 through 520, and in the Nevada Administrative Code (NAC), primarily Chapter 517.

Federal mining claim law applicable to claims located on federal lands is based on the General Mining Law of 1872, formally titled “*An Act to Promote the Development of Mineral Resources of the United States*”. Federal regulations governing mining claims and surface disturbance are implemented through provisions in 30 USC, 43 USC, and 43 CFR, as well as corresponding Nevada statutes, including NRS 517.

Approximately 85 percent of the land area within the State of Nevada is federally owned. Most of these lands are administered by federal agencies, including the BLM, the United States Forest Service (USFS), the United States Department of Energy (DoE), and the United States Department of Defense. Large areas of land administered by the Bureau of Land Management and the Forest Service remain open to mineral exploration and to the location of mining claims under the General Mining Law.



Figure 3-2: Sleeper Tenement Map



Federal Requirements for Exploration and Mining Activities

Regulations administered by the BLM governing surface disturbance and reclamation are contained in 43 CFR 3809. These regulations require that exploration activities involving disturbance of five acres or less be conducted under a Notice of Intent submitted to the appropriate BLM Field Office (43 CFR 3809.1-1 through 3809.1-4).

A Plan of Operations (POO) must be submitted and approved for mining or processing activities, as well as for exploration activities that will disturb more than five acres. A Plan of Operations is also required for bulk sampling programs where 1,000 short tons or more of presumed ore are proposed to be removed (43 CFR 3802.1 through 3802.6; 43 CFR 3809.1-4 and 3809.1-5).

BLM regulations further require that operators post reclamation bonds sufficient to ensure reclamation of disturbances caused by activities exceeding casual use (43 CFR 3809.500 through 3809.560).

Federal Mining Claim Location and Maintenance Requirements

Federal regulations (43 USC 1744; 43 CFR 3833.1-2) require that the locator of a mining claim, mill site, or tunnel site file a copy of the notice or certificate of location with the appropriate State Office of the Bureau of Land Management. This filing must include a map showing the claim location and must be completed within 90 days after the claim is located. Failure to complete this filing within the required period renders the claim void.

The certificate of location must include:

- The name and current mailing address of the claim owner or owners
- The type of claim
- The legal location of the claim, including township, range, section, and quarter section
- The accompanying map must correspond to the claim location requirements established under Nevada state law.

Federal law (30 USC 28f; 43 CFR 3833.1-5) also requires payment of an annual claim maintenance fee to the Bureau of Land Management. This fee must be paid to the appropriate BLM State Office on or before September 1 of each year. During the initial assessment year (the year in which the claim is located), the maintenance fee must be paid at the time the notice of location is filed with the BLM. Failure to pay the claim maintenance fee results in the claim being declared void.

Nevada State Requirements

Nevada law also requires claim holders to file documentation demonstrating continued intent to hold mining claims. Under NRS 517.230, on or before November 1 of each year, the claimant, or an authorized representative, must record with the County Recorder a Notice of Intent to Hold if annual assessment work is not being performed.

This affidavit must include the following:

- Name and mailing address of the claimant
- Name of the mining claim
- Bureau of Land Management serial number (if assigned)



- Statement affirming the claimant’s intention to maintain the claim

The Notice of Intent to Hold establishes the claimant’s intent to maintain the claim from 12:00 pm on September 1 of the previous year through 11:59 am on September 1 of the current year.

3.3 Encumbrances

Unpatented mining claims require annual maintenance fees paid to the BLM as well as county recording fees. As of the Effective Date of this report, claim maintenance fees have been paid in full through August 31, 2026.

Table 3-2: Property Holding Costs

Cost Category	Annual Cost (US\$)	Notes
Annual Claim Fees	494,800	BLM maintenance fees (\$200/claim)
County Recording Fees	37,110	Humboldt County recording costs (approximately \$15/claim)
Total Annual Holding Cost	531,910	Estimated annual property holding cost

3.4 Royalties

A total of five net smelter return (NSR) royalties apply to future mineral production from portions of the Project. These royalties are summarized in Table 3-3.

Table 3-3: Royalty Agreement Summary

Royalty Holder	Royalty Terms
Montezuma	1% NSR on ALL RO and SH claims (South Sleeper)
Geologix	1% NSR on ALL RO and SH claims (South Sleeper)
Snyder Syndicate	1% NSR on the 1,044 Sleeper Gold Mine claims (All claims, EXCEPT for ALL MIMI, ALL SP, ALL SS, AND ALL BLUE.)
Franco-Nevada U.S. Corporation	2% NSR on minerals produced from all 2,474 claims
Evolving Gold / Quinton Hennigh	2% NSR royalty on all SS and all SP claims.
Dry Lake Placer Association	3% NSR on Dry Lake Placer claims
ICN Resources Ltd.	0.5% NSR on all SS and all SP claims; 1.5% NSR on all Blue claims

3.5 Required Permits and Status

The permits are summarized in Table 3-4 represent the principal BLM and State of Nevada authorizations for exploration, reclamation, historical operations, and ongoing site maintenance at the Property as of the report’s Effective Date. The summary preserves the permit numbers, bond references, and compliance details from the source material and is intended to support a concise yet complete permit section in the technical report.



3.5.1 Key BLM and State Permits in Place

Table 1 summarizes the key BLM and State permits identified as being in place as of the Effective Date of the report. These permits are associated with exploration, mine operations, air quality, reclamation, water management, solid waste, and related site activities.

Table 3-4: Sleeper - Key BLM and State Permits in Place

Permit / Authorization	Permit Number	Regulatory Agency	Notes/Scope
Exploration Reclamation Permit	#0219	Nevada Division of Environmental Protection / Nevada Division of Minerals	Exploration reclamation authorization maintained for exploration disturbance and associated reclamation obligations.
Exploration Plan of Operations	#NVN077104	BLM	Federal exploration plan covering exploration activities and related surface disturbance.
Sleeper Mine	#NVN064100	BLM	Mine-level federal authorization associated with the Sleeper Mine operations area.
Class II Air Quality Operating Permit – Surface Area Disturbance	#AP1041-2831	State of Nevada	Air quality operating permit associated with surface disturbance activities.
Mine Reclamation Permit	#0037	State of Nevada	Legacy permit maintained from prior mining activities for future reactivation flexibility.
Water Pollution Control Permit	#NEV50006	State of Nevada	Water pollution control authorization maintained from prior operations.
Ground Water Appropriation Permits	#53228, #53231, and #53236	State of Nevada	Groundwater rights and appropriation permits applicable to the project area.
Hazardous Materials Permit	#30473; FDID #08250; Facility #1168-2326	State / Local	Hazardous materials registration and related compliance records for the site.
Class III Solid Waste Landfill Waiver	#SWMI-08-10	State of Nevada	Waiver associated with the site landfill / solid waste management function.
Industrial Artificial Pond Permit	#S34480	State of Nevada	Industrial pond authorization maintained from prior operating conditions.
Mine Plan of Operations	#N64100	BLM	Mine plan maintained for historical operations and future updating if production is reinitiated.

In addition to the principal permits listed above, the property maintains numerous other permits associated with previous mining activities. These legacy permits are retained to facilitate future



updates should a decision be made to reinitiate production at the site. Ongoing maintenance of these permits includes monthly, quarterly, and annual monitoring and reporting, as applicable.

3.5.2 Reclamation Bonds

Table 3-5 summarizes the reclamation bonds associated with the principal BLM-authorized activities. The BLM Nevada State Office currently holds both bonds, and the current bond obligation was approved on October 9, 2020. The bond amounts are reviewed every three years.

Table 3-5: Sleeper Reclamation Bonds

Bond Number	Principal	Covered Authorization	Current Obligation (US\$)	Purpose
NVB000444	New Sleeper Gold LLC	NVN077104	345,044	Surface reclamation coverage for the Sleeper Gold Exploration Plan.
NVB000330	Sleeper Mining Company LLC	NVN064100	3,966,373	Surface reclamation coverage for operations conducted under the Sleeper Mine authorization.

3.5.3 Compliance and Permit Status

According to the source material, Paramount Gold is currently in compliance with all issued permits and is in the process of renewing those permits that require renewal. The bonds held by the BLM provide surface reclamation coverage for operations conducted by the relevant principals under NVN064100 and NVN077104, respectively.

The current bond obligation was approved on October 9, 2020, and is reviewed every three years. Permit maintenance activities include monthly, quarterly, and annual monitoring and reporting. Retaining legacy permits from previous mining activities is intended to simplify future permit updates if production is restarted.

3.6 Other Significant Factors and Risks

The SLR QP is not aware of any environmental liabilities on the property. Paramount Gold has, or can obtain, all the required permits to conduct the proposed work on the property. The SLR QP is not aware of any other significant factors and risks that may affect access, title, or the right or ability to perform the proposed work program on the property.



4.0 Accessibility, Climate, Local Resources, Infrastructure, and Physiography

4.1 Accessibility

The Sleeper Gold Mine is in Humboldt County in north-central Nevada, approximately 42 km (26 mi) northwest of Winnemucca, Nevada, which lies along Interstate 80, the principal east–west transportation corridor across northern Nevada connecting Reno, Nevada, and Salt Lake City, Utah. Access to the project area is provided by Nevada State Highway 95, approximately 51 km (32 mi) north of Winnemucca, and Nevada State Highway 140, approximately 23 km (14 mi) west toward the project area. The property is connected to the paved highway network by Sod House Road, a maintained gravel road that provides direct access to the mine site and surrounding exploration areas. Interstate 80 parallels the Union Pacific transcontinental railroad, providing efficient transportation of bulk materials and mining consumables to Winnemucca and the surrounding mining district. The project area can be reached year-round by vehicle under typical weather conditions, given the region's generally dry climate and moderate winter snowfall.

4.2 Climate

The Sleeper Gold Mine is in Desert Valley at the western base of the Slumbering Hills in Humboldt County, Nevada. The project area lies within the Basin and Range physiographic province at an elevation of approximately 1,300 m (about 4,265 ft) above sea level. The regional climate is characteristic of the semi-arid high desert of northern Nevada, with relatively low annual precipitation, large daily temperature variations, and generally clear skies throughout much of the year. Winters are typically cool to cold, with average daytime temperatures in January of approximately 6°C to 8°C and nighttime temperatures commonly declining to approximately -7°C to -9°C, although colder temperatures may occur during periodic Arctic air incursions. Snowfall occurs intermittently during winter storm events; however, snow accumulations at the valley floor are generally modest and short-lived, typically melting within several days.

Average annual precipitation in the Desert Valley area is approximately 130 mm to 150 mm per year (about 5 to 6 inches), with most precipitation occurring during winter and early spring frontal systems. Summers are generally warm to hot during the day, with temperatures often exceeding 30°C, while nighttime temperatures typically cool significantly due to the dry desert air and elevation. Summer precipitation is relatively limited and typically occurs as isolated convective thunderstorms associated with late-season Great Basin monsoonal activity. Overall, the area is characterized by low humidity, high evaporation rates, and sparse high-desert vegetation. Because of the relatively dry climate, moderate winter snowfall, and the absence of prolonged severe weather conditions, the Sleeper property area is considered favorable for year-round exploration, development, and mining operations, with only minor seasonal impacts on access or operational efficiency.

4.3 Local Resources and Infrastructure

The Project lies within a region with a long history of mining activity. The historical Sleeper mine was operated by AMAX from 1986 to 1996 as a large open-pit gold and silver operation. The previous operation required the development of significant mining infrastructure, including haul roads, processing facilities, water supply systems, electrical distribution systems, and support



facilities, demonstrating that the area can support large-scale mining operations. Several facilities remain on-site and are currently utilized to support exploration activities, including office space, equipment maintenance facilities, and storage areas used for drilling and exploration programs.

The nearest regional service center is Winnemucca, Nevada, located approximately 42 km southeast of the property. The city of Winnemucca is the county seat of Humboldt County and has a population of approximately 8,400 people. The city functions as a primary commercial and logistical hub for mining operations throughout north-central Nevada and provides access to equipment suppliers, fuel distribution, heavy equipment maintenance facilities, drilling and blasting contractors, warehousing, lodging, medical services, and other industrial support services commonly required by mining projects.

Transportation and Access

Regional access to the Sleeper property is provided by Interstate 80, which passes through Winnemucca and serves as the principal east–west transportation corridor across northern Nevada. Interstate 80 provides direct connections to major mining centers, including Elko, Nevada and Salt Lake City, Utah, to the east and Reno, Nevada, to the west.

An extensive network of historical mine haul roads, exploration access roads, and drill roads exists throughout the property, resulting from mining activities conducted between 1986 and 1996 and subsequent exploration programs. These roads provide access to the historical open pit, heap-leach pads, waste-rock facilities, and exploration targets throughout the Sleeper district. Depending on the development scenario, portions of this road network may require upgrading or rehabilitation to support future operations.

Electrical Power

Electrical power in northern Nevada is supplied by regional utilities through a network of high-voltage transmission lines serving numerous mining operations. Transmission infrastructure in the broader region commonly includes 69-kV, 120-kV, and 230-kV lines that connect mines and industrial facilities to the regional grid operated by NV Energy. Typical overhead transmission lines in the region consist of aluminum-conductor steel-reinforced (ACSR) cables mounted on steel or wooden monopole structures spaced approximately 90 m to 135 m apart, with structure heights typically ranging from about 17 m to 25 m, depending on terrain and span requirements. Transmission corridors commonly occupy rights-of-way approximately 27 m wide.

Historical mining operations at Sleeper required electrical power for mining equipment, ore processing facilities, pumping systems, and general site infrastructure. Historically, electrical power to the project area was supplied by an existing 120-kV transmission line approaching the property from the north, operated by Harney Electric Cooperative. Future operations could utilize regional transmission connections, combined with on-site substations and electrical distribution systems similar to those used at other open-pit mining operations in northern Nevada.

Airports and Air Transportation

The closest airport to the project area is Winnemucca Municipal Airport, approximately 10 km southwest of Winnemucca. The airport has a primary asphalt runway approximately 2,134 m (7,000 ft) in length and supports general aviation and charter aircraft used by mining companies operating in the region. The nearest airports offering scheduled commercial airline service are Reno–Tahoe International Airport, approximately 260 km southwest of the project area, and Elko Regional Airport, approximately 200 km east of the project area.



Workforce and Mining Services

Northern Nevada is one of the most active gold-mining regions in the world and hosts numerous large mining operations. As a result, the region supports a well-established mining workforce, including equipment operators, geologists, engineers, mechanics, electricians, and other skilled trades. Many workers employed at regional mines reside in Winnemucca or nearby communities. The presence of multiple operating mines has also resulted in the establishment of numerous mining contractors and equipment suppliers capable of supporting exploration programs, construction activities, and large-scale mining operations.

Services available in Winnemucca and the surrounding region include heavy equipment repair facilities, fuel distribution, drilling and blasting contractors, industrial construction contractors, mining equipment suppliers, and transportation and logistics companies. These services support both existing mining operations and exploration activities throughout Humboldt County and the broader northern Nevada mining district.

Sources of Water

Water for the previous operations was obtained from groundwater sources within the Desert Valley basin, supplemented by pit dewatering systems during mining operations. Paramount Gold currently holds water rights associated with the Project.

General Infrastructure

Much of the previous mining infrastructure has been reclaimed following the mine's closure in 1996; however, several facilities remain available to support exploration and future development. The property's subdued topography provides suitable areas for the construction of mine infrastructure, including processing facilities, heap leach pads, waste rock storage areas, and associated operational infrastructure.

Existing infrastructure at the Sleeper site is listed below:

- Exploration and administrative office building
- Heavy equipment maintenance shop (four-bay truck shop)
- Dewatering well service shop
- Truck maintenance facilities
- Diesel storage and fuel tanks
- Electrical transmission and distribution lines
- Groundwater monitoring wells
- Water management ponds
- Administrative and storage buildings
- On-site landfill area
- Existing mine haul roads and exploration access roads

4.4 Physiography

The Project is in north-central Nevada within the Basin and Range physiographic province, a region characterized by alternating north-south trending mountain ranges and broad alluvial valleys formed by extensional tectonics. The Sleeper property lies primarily within Desert Valley



and along the western flank of the Slumbering Hills, a low mountain range that forms the eastern boundary of the valley. Elevations in the immediate project area average approximately 1,300 m above sea level (masl) (about 4,265 feet above mean sea level [fasl]) on the valley floor, increasing eastward into the Slumbering Hills where elevations exceed approximately 1,700 masl. The terrain surrounding the historical Sleeper open pit consists of gently sloping alluvial fans, pediments, and low bedrock ridges, which transition into steeper volcanic uplands within the Slumbering Hills. Relief within the immediate mine area is generally moderate, with local elevation differences of several hundred meters between the valley floor and adjacent uplands.

Desert Valley is a broad internally drained basin typical of northern Nevada, formed by fault-bounded mountain ranges and filled with unconsolidated alluvial and lacustrine sediments derived from surrounding highlands. Surface drainage in the project area is limited and largely ephemeral, consisting of intermittent washes and small drainage channels that flow only during seasonal precipitation or localized storm events. These ephemeral drainages typically flow westward across the valley floor and dissipate into alluvial sediments, forming no perennial streams. Vegetation in the area is characteristic of Great Basin high-desert shrubland, dominated by sagebrush, rabbitbrush, and scattered grasses adapted to semi-arid conditions. The relatively subdued topography of the valley floor, combined with sparse vegetation and arid conditions, provides favorable terrain for the development of large open-pit mining operations, heap leach facilities, and associated infrastructure. Overall, the physiography of the Sleeper property is typical of the northern Nevada Basin and Range region and presents few significant natural constraints to exploration, development, or mining activities.



5.0 History

5.1 Early Mining – Awakening District (Pre-1982)

The Sleeper Gold Mine is in the Awakening Mining District. Gold mineralization in the district was recognized well before the discovery of the Sleeper deposit. Early mining activity in the district dates to the early 1900s, with production associated primarily with gold-bearing quartz veins hosted in metasedimentary rocks.

Significant production began in the 1930s from the Jumbo and Alma mines in the Slumbering Hills, approximately 6 km southeast of the eventual Sleeper pit. Narrow quartz–adularia veins were mined by underground and small open pit methods. Historical compilations report that the Awakening District produced approximately 26,262 ounces of gold between 1932 and 1958. Numerous historical shafts, adits, and prospect pits occur within a few kilometers of the Sleeper deposit, indicating widespread early exploration activity.

5.2 Ownership

5.2.1 AMAX Gold Inc. Discovery and Mining (1982–1996)

The modern history of the Sleeper deposit began in 1982 when John Wood, an exploration geologist with AMAX, recognized iron-oxide staining in an outcrop during aerial reconnaissance. AMAX conducted geological mapping, geochemical sampling, and drilling programs between 1982 and 1984.

A breakthrough occurred in late 1984 when a step-out drill hole intersected approximately 102 m of silicified breccia averaging approximately 27.87 g/t gold and 61.7 g/t silver. The discovery hole confirmed the presence of a high-grade epithermal gold system and led to rapid project advancement. AMAX formally announced the Sleeper gold discovery in February 1985. Regulatory approvals for the mine's construction were granted later in 1985. Mining began in January 1986, and mill commissioning commenced the following month. The first gold bar was poured on March 26, 1986, only slightly more than a year after the discovery announcement.

The operation processed oxide mineralization using both milling and heap-leaching circuits. Initial mine plans projected modest production, but actual production greatly exceeded expectations due to exceptionally high grades encountered early in the Sleeper vein system. Gold production during 1986 reached approximately 126,000 ounces, with operating costs reported at less than US\$60 per ounce.

Production increased to approximately 159,000 oz in 1987 and approximately 230,000 oz in 1988. The mine was widely recognized as one of the lowest-cost gold producers in the world during the late 1980s. AMAX later added heap-leach facilities to process lower-grade oxide material.

In 1994, AMAX merged with Cyprus Minerals to form Cyprus Amax Minerals Company. Mining at Sleeper continued until 1996, when operations were suspended. Total historical production from the Sleeper mine is approximately 1.66 Moz Au and 2.3 Moz Ag. Approximately 1,219,880 Moz Au were recovered from milling operations and approximately 438,609 Moz Au from heap-leach processing.



Following closure, groundwater began filling the open pit, forming a pit lake. AMAX accelerated the filling of the open pit to prevent the formation of acidic water. Processing facilities and crushing equipment have since been removed, and the former mill area has been reclaimed.

5.2.2 X-Cal Resources Ltd. and Joint Venture Exploration (1993–2010)

X-Cal Resources Ltd (X-Cal) began assembling a land package in the district in 1993 when it acquired property around the Alma Mine through an agreement with Leland York. Surface mapping and sampling identified several areas of anomalous gold mineralization. Additional claims were acquired in 1994 and 1995, extending X-Cal's holdings to the boundary of the AMAX Sleeper property.

In April 1996, X-Cal and AMAX entered into a joint venture agreement to explore the Sleeper property and the surrounding land package. In 1997, X-Cal entered into an option agreement with Placer Dome Inc. (Placer Dome). During a 40-day review period, Placer Dome conducted data compilation, completed an aeromagnetic survey, and drilled 47 holes totaling approximately 13,323 m (43,710 ft) of reverse circulation (RC) drilling and of diamond core drilling. The option ultimately expired after revised terms could not be negotiated.

Kinross Gold Corp. (Kinross) acquired AMAX's interest in the Sleeper project. Between 1998 and 2003, X-Cal negotiated several agreements with Kinross regarding ownership of the property.

On January 9, 2004, X-Cal and New Sleeper Gold Corp. (New Sleeper Gold) formed a 50/50 joint venture and acquired Kinross's 50% interest in the Sleeper property. New Sleeper Gold assumed management of the Project and funded extensive exploration programs between 2004 and 2005. These programs included approximately 29,780 m (97,704 ft) of drilling, consisting of sonic, reverse-circulation, and diamond-core drilling, as well as trenching, induced polarization and magnetotelluric geophysical surveys, gravity surveys, soil-gas surveys, geological mapping, and geochemical sampling.

In May 2006, X-Cal acquired New Sleeper Gold's 50% interest in the joint venture, consolidating 100% ownership of the Sleeper project.

5.2.3 Paramount Gold Nevada Corp. (2010–Present)

In August 2010, Paramount Gold and Silver Corp. acquired all outstanding shares of X-Cal Resources Ltd. through a plan of arrangement. Following the acquisition, Paramount Gold Corp. began renewed exploration drilling at Sleeper in October 2010.

In 2011, Paramount Gold Corp. acquired the Dunes Project claims located south of the Sleeper deposit from ICN Resources Ltd. (ICN). In 2012, additional claims known as the Mimi Project were staked adjacent to the historical Sleeper mine.

In connection with the acquisition of Paramount Gold and Silver Corp. by Coeur Mining, Inc., the Nevada assets were spun out into a separate publicly traded company, Paramount Gold Nevada Corp., in 2015. Paramount Gold Nevada Corp. now controls the Project through its subsidiaries, Sleeper Mining LLC and New Sleeper LLC.

Additional claims known as the South Sleeper (RO and SH groups) were acquired in 2021, expanding the overall property. The Sleeper Gold Mine currently comprises a large district-scale land position comprising 2,474 unpatented federal mining claims administered by the BLM. The Project is an advanced exploration and redevelopment project centered on the historical open pit mine and numerous surrounding exploration targets within the Awakening Mining District.



5.3 Exploration and Development History

5.3.1 Historical Drilling (1983–2010)

Drilling at the Project has been conducted intermittently since the early 1980s by multiple operators and forms the primary basis for the current geological, structural, and grade interpretation of the deposit. Initial drilling programs undertaken by AMAX between 1983 and 1995 established the core of the drilling database. Subsequent exploration and evaluation programs were completed by Placer Dome, X-Cal, New Sleeper Gold, and others through approximately 2010.

The historical drilling database is extensive and represents the majority of drilling completed at the Project. Reverse circulation (RC) drilling predominates, accounting for approximately 95% of all drill holes and meters drilled, with most holes oriented vertically, reflecting the exploration and production objectives of early-stage development. Later programs incorporated angled diamond core drilling to better define structural controls, vein orientations, and the geometry of higher-grade mineralization. These core programs significantly improved geological control, particularly in areas characterized by steeply dipping vein systems and structurally controlled mineralization. Integration of RC and core datasets has enabled the development of a refined geological and structural model, including the recognition of multiple vein sets, hydrothermal breccias, and stratigraphically controlled mineralized domains. However, portions of the historical database are incomplete, with missing hole metadata, survey information, and total depths for certain programs. These limitations have been considered by the QP in evaluating data reliability and Mineral Resource classification.

Modern exploration commenced with AMAX in April 1982, following reconnaissance identification of iron staining. Surface mapping, geochemical sampling, and drilling culminated in a late-1984 step-out hole intercepting 102 m averaging 27.87 g/t Au (0.81 oz/st Au) and 61.7 g/t silver, including a high-grade quartz-electrum vein with visible gold. Discovery was announced in February 1985, construction was approved in August 1985, and mining began in January 1986. The mill was commissioned in February 1986, and first gold was poured on March 26, 1986. Between 1986 and 1996, production totaled approximately 1.66 Moz of gold and 2.3 Moz of silver. During the 1983–1995 period, AMAX completed 3,668 drill holes totaling 509,043 m and conducted an IP/resistivity survey in 1987. Mining concluded in 1996.

In 1989, NGM reportedly drilled nine holes totaling 438 m; however, SLR is unaware of NGM's full name or of any relationship, if any, between NGM and AMAX. No information is available regarding NGM's drilling contractors, drill rig types, sample collection procedures, or collar and down-hole survey methods.

From 1996 to 1997, under the X-Cal/AMAX joint venture, work focused on data compilation, mapping, surface geochemistry, and geophysics. Between 1993 and 1997, X-Cal collected 7,599 soil samples and 2,480 rock samples and completed 140 RC holes totaling 27,700 m. QA/QC procedures established during this period formed the basis for protocols adopted in later programs.

In 1997, Placer Dome optioned the property, conducted a comprehensive database review, and completed a high-resolution airborne magnetic survey (50 m line spacing with 2 m readings). Placer Dome drilled 47 holes totaling 13,323 m, including RC and RC/core combination holes. During this period, Mineral Resources Development Inc. (MRDI) evaluated tailings and heap-leach pads using six auger holes in tailings (7.6 m to 10.7 m depth), two RC holes, and three auger holes in leach pads.



Between 1998 and 2003, X-Cal focused on consolidating and evaluating tailings and heap-leach materials. This work included ten auger holes drilled into tailings in 1999, 83 sonic holes completed in 2002 (9.1 m to 10.7 m depth with 1.52 m sampling intervals), and a gravity survey conducted in 2003 on 500 m line spacing with 200 m stations. Sampling and analytical procedures were generally consistent with industry standards, although documentation from early programs is incomplete.

In January 2004, New Sleeper Gold acquired Kinross' 50% interest and entered into a joint venture with X-Cal. Between 2004 and 2005, exploration and development activities included 29,780 m of drilling (comprising 17,028.9 m core, 11,373.6 m RC, and 688.8 m sonic drilling), trenching, IP, magnetotelluric (MT), gravity surveys, soil-gas surveys (Hg and O₂/CO₂), surface mapping, geochemical sampling, and aerial photography. During this period, mill and crusher facilities were removed and reclaimed. Joint funding commenced in August 2005, and X-Cal acquired full ownership in May 2006.

From 2004 to 2007, integrated interpretation of magnetic, gravity, IP, and MT datasets refined the understanding of structural controls on mineralization. Magnetic inversion modeling in 2005 identified mineralization within a magnetic low bounded by magnetic highs, while gravity surveys completed between 2003 and 2005 delineated density contrasts and major structural trends. Soil-gas and geochemical anomalies further highlighted concealed structures. QA/QC procedures applied during this period were consistent with industry practice.

Between 2003 and 2007, X-Cal drilled an additional 47,347 m, including 30 core holes (9,027 m), 133 RC holes (35,546 m), eight RC/core combination holes (2,776 m), and one hole of unknown type. Drilling, sampling, and QA/QC procedures implemented in 2006 and refined in 2007 became standard for subsequent programs. Work during this period also included structural interpretation, target generation, blasthole modeling, and continued evaluation of tailings and heap-leach materials. Subsequent exploration drilling included 69 drill holes totaling 18,041 m by New Sleeper Gold between 2004 and 2005, followed by an additional 34 holes (6,636 m) completed by Evolving Gold in 2008, and by Montezuma Mines, 11 holes (1,940 m) between 2011 and 2012. Evolving Gold also conducted gravity, IP/resistivity, and ground magnetic surveys between 2007 and 2008, while Montezuma completed ground magnetics (2009–2010) and gravity/IP surveys (2011–2012). Some drill hole locations from these programs were not incorporated into the historical drilling database due to unresolved drill hole location surveys. In 2021, Paramount Gold conducted an exploration RC drilling program focused on the Range Front target area southeast of the pit in the hills east of the South Dump. Drilling of 6 RC holes totaling 2,644 m was completed.

5.3.2 Historical Geophysical and Surface Exploration Programs

5.3.2.1 Airborne Geophysical Surveys (1980s–1997)

Airborne geophysical surveys were conducted during several phases of exploration from the 1980s through the late 1990s, culminating in a detailed aeromagnetic survey completed in 1997. This survey utilized closely spaced east–west and north–south flight lines, approximately 50 m apart, with high-frequency data acquisition along the lines. The airborne magnetic data were used to identify lithologic variations and structural features, including volcanic units, intrusive bodies, and fault zones. Magnetic highs were interpreted to be associated with volcanic, hypabyssal, and metasedimentary rock units, providing important context for geological interpretation and exploration targeting. These airborne datasets provided regional-scale coverage of the property and were instrumental in defining large-scale structural trends and lithologic domains that guided subsequent ground-based exploration and drilling programs.



5.3.2.2 Ground Geophysical Surveys (1980s–2012)

Ground-based geophysical surveys were conducted from the early 1980s through 2012 and included magnetic, gravity, IP, resistivity, and MT methods. Ground magnetic surveys were used to refine interpretations derived from airborne data and to provide higher-resolution mapping of local structures and lithologic contacts. Gravity surveys conducted throughout this period, including early programs and later expansions, were used to define basin geometry, bedrock topography, and density contrasts associated with lithologic and alteration variations. These data were particularly important in identifying structural features beneath post-mineral cover and in constraining the geometry of the basin hosting the Sleeper deposit. Electrical geophysical methods, including induced polarization and resistivity surveys conducted during multiple phases of exploration, including the 2004–2005 joint venture period, were used to detect chargeability anomalies and resistivity contrasts associated with sulfide mineralization, silicification, and hydrothermal alteration. MT surveys conducted during this period provided insight into deeper conductivity structures and regional controls on hydrothermal fluid pathways.

5.3.2.3 Surface Geochemical Programs (1980s–2012)

Surface geochemical sampling programs were conducted from the early 1980s through 2012 and included extensive soil and rock-chip sampling campaigns across the property. Soil geochemical programs, comprising more than 11,000 samples collected over multiple phases, were designed to identify anomalous concentrations of gold and pathfinder elements, particularly in areas of shallow alluvial cover.

Rock-chip sampling programs were used to verify mineralization exposed at surface and to characterize lithologic units and alteration zones. The integration of geochemical data with geological mapping and geophysical interpretations enabled the delineation of coherent mineralized trends and target areas for follow-up drilling.

5.3.2.4 Soil Gas and Specialized Geochemical Surveys (2004–2005)

During the 2004–2005 joint venture exploration programs, specialized soil gas surveys were conducted, including mercury vapor and O₂/CO₂ measurements. These techniques were applied to detect subtle geochemical signatures associated with concealed mineralization and hydrothermal activity, particularly in areas where conventional soil geochemistry was less effective due to cover conditions. These data were integrated with other exploration datasets to refine target generation.

5.3.3 Geological Mapping and Trenching (1980s–2005)

Geological mapping programs were conducted throughout the property's exploration history, beginning in the early 1980s and continuing through later campaigns, including the 2004–2005 joint venture period. These programs focused on defining lithologic units, alteration assemblages, and structural features across the property.

Trenching programs, particularly those conducted during the 2004–2005 period, were used to expose bedrock beneath shallow cover and to allow direct observation and sampling of mineralized zones. These activities supported refinement of the geological model and validation of geochemical and geophysical anomalies.

The integration of these historical geophysical and surface exploration programs resulted in the identification of multiple mineralized trends and structurally controlled zones across the property. Several of these trends, including those associated with volcanic contacts and major



structural corridors, have not been extensively drill tested and remain prospective for additional mineralization

5.4 Past Production

Table 5-1 combines gold production from both the mill and heap-leach circuits operated by AMAX Gold Inc. at the Sleeper Mine. Silver production was primarily recovered from mill operations. Totals correspond with reported cumulative production of approximately 1.66 Moz of gold and approximately 2.3 Moz of silver.

Table 5-1: Sleeper Gold Mine – Total Annual Production (1986–1996)

Year	Mill Gold (000 oz)	Heap Gold (000 oz)	Total Gold (000 oz)	Mill Silver (000 oz)	Heap Silver (000 oz)	Total Silver (000 oz)
1986	132.6	4.9	137.6	93.1	11.4	104.5
1987	152.8	16.8	169.6	131.3	38.8	170.1
1988	170.6	56.7	227.3	173.4	74.3	247.7
1989	196.3	57.9	254.3	245.0	97.2	342.2
1990	191.1	53.6	244.7	269.7	120.8	390.5
1991	121.1	62.6	183.7	183.2	108.0	291.2
1992	78.3	61.7	140.0	130.0	122.0	252.0
1993	51.3	48.9	100.2	157.7	98.5	256.2
1994	70.9	36.2	107.1	59.6	83.8	143.3
1995	54.7	27.3	82.1	47.7	51.0	98.7
1996	-	12.0	12.0	-	9.9	9.9
Totals	1,219.9	438.6	1,658.5	1,490.8	815.6	2,306.4
Avg. Metallurgical Recovery (%)	89.6	42.9	-	43.4	39.5	-



6.0 Geological Setting, Mineralization, and Deposit

The information presented herein has been reviewed, edited, and, where appropriate, directly derived from RESPEC (2023) and Wilson and SRK (2012). The geological framework, mineralization models, and deposit interpretations have been evaluated by SLR for completeness, internal consistency, and technical reasonableness.

6.1 Regional Geology

The Project is located within the northern Basin and Range Province of Nevada, a region characterized by extensional tectonics, high-angle normal faulting, and widespread Cenozoic magmatism. The regional geologic framework comprises the following (Figure 6-1 and Figure 6-2):

- Mesozoic metasedimentary basement rocks of the Auld Lang Syne Group
- Cretaceous granitic intrusive rocks
- Overlying Tertiary volcanic sequences, including bimodal basaltic and rhyolitic units
- Basin-fill sediments associated with post-mineral extensional deformation

The Project is situated along the western flank of the Slumbering Hills within the western portion of the Northern Nevada Rift (NNR), a northwest-trending mid-Miocene geologic province extending from southeastern Oregon to southeastern Nevada. As described in RESPEC (2023) and Wilson and SRK (2012), the NNR is characterized by bimodal basalt–rhyolite volcanism, extensional tectonics, and a documented spatial association with low-sulfidation epithermal gold-silver mineralization (John 2001).

Available geological information indicates that the NNR developed during a period of regional extension beginning in the mid-Miocene (approximately 17 Ma), expressed by high-angle normal faulting and associated volcanic activity. These structural and magmatic features are widely recognized as key controls on epithermal mineral systems in northern Nevada. The association between mineralization and this tectono-magmatic framework at the Project is based on regional analogs and published studies and should be considered interpretive.

Pre-Tertiary rocks in the Slumbering Hills consist of metasedimentary rocks of the Auld Lang Syne Group and Cretaceous granitic intrusions, consistent with descriptions in both source reports. The metasedimentary sequence has been interpreted as part of an early Mesozoic back-arc basin assemblage that was subsequently deformed and metamorphosed to greenschist facies during late Jurassic contraction associated with the Luning–Fencemaker thrust system.

Tertiary volcanic and volcanoclastic rocks unconformably overlie the pre-Tertiary basement and locally intrude it. As described in the Wilson and SRK report (2012), many of these volcanic units are interpreted to represent outflow facies of the McDermitt volcanic field and related caldera complexes to the north. Volcanic rocks hosting mineralization at Sleeper are interpreted to have been derived from a local volcanic center; however, the extent, timing, and configuration of this source remain open to interpretation.

Quaternary pediment gravels and aeolian deposits occur west of the Slumbering Hills and locally cover portions of the Project area, limiting bedrock exposure and influencing surface geological mapping and exploration methods.



The regional structural framework is dominated by northwest- to north-northeast–trending high-angle normal faults, which control basin development and are interpreted to have provided conduits for hydrothermal fluid flow. Basin and Range extension is also expressed by tilting of structural blocks. District-scale interpretations in the Wilson and SRK report (2012) suggest a northeast-trending arch or anticline within the northern Slumbering Hills, characterized by opposing limb dips; however, this feature is inferred from regional mapping and remains conceptual.

The association between extensional faulting, bimodal volcanism, and epithermal mineralization is supported by regional studies and both technical reports; however, the specific structural and lithologic controls on mineralization at the Property remain interpretive and subject to refinement with additional geological and drilling data.



Figure 6-1: Regional Geology

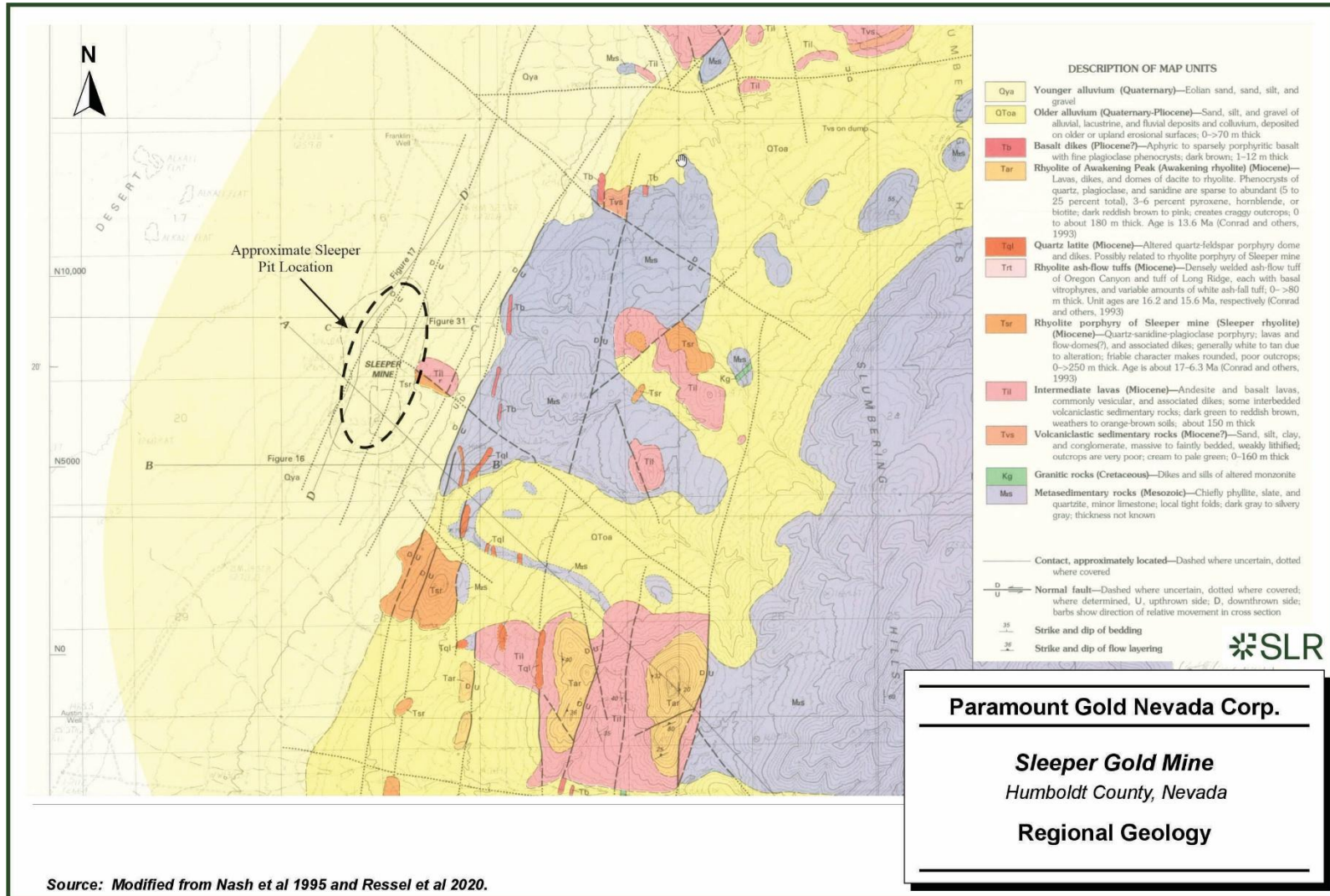
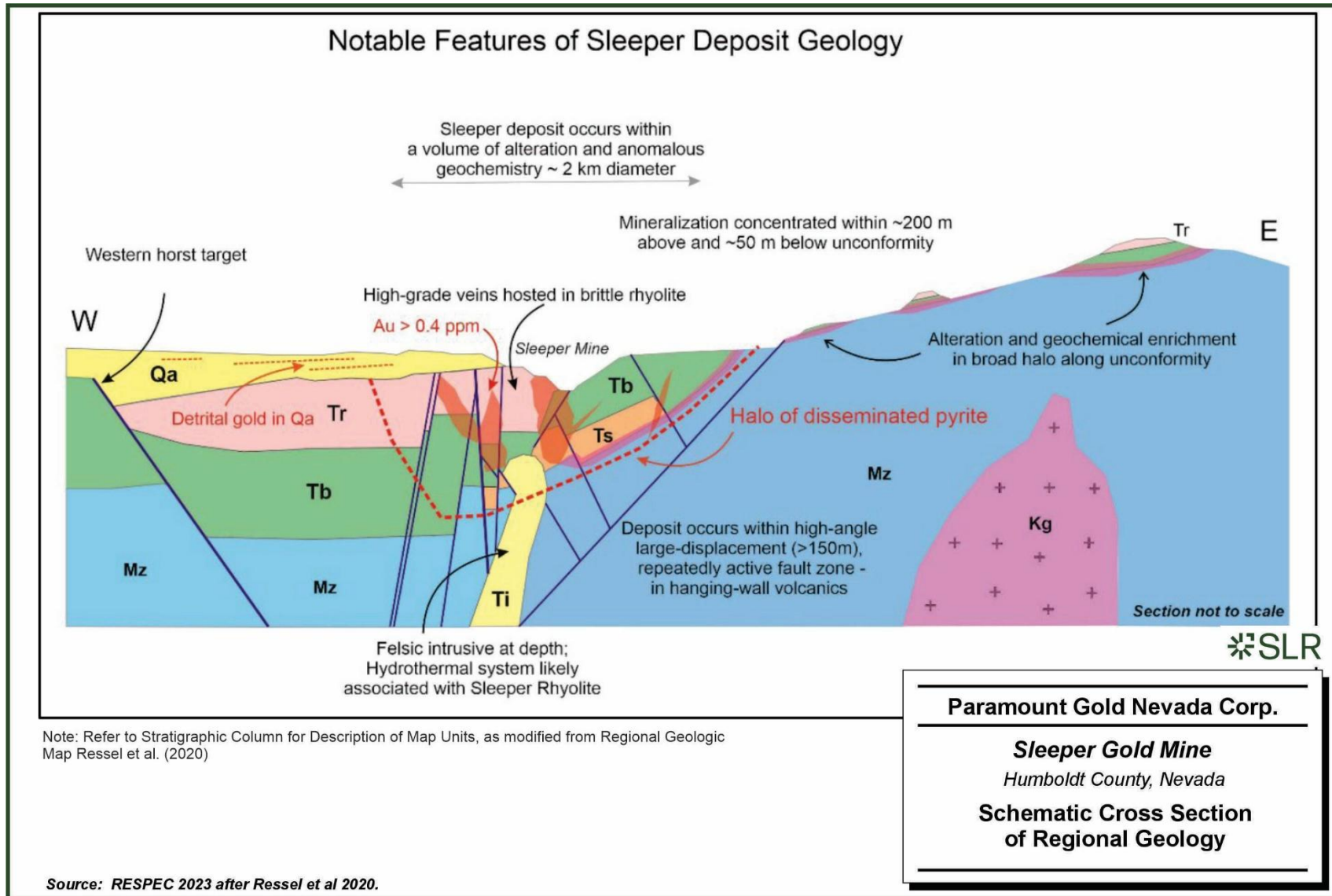


Figure 6-2: Cross Section of Regional Geology



6.2 Local Geology

At the local scale, the Sleeper Gold-Silver Project is situated along the western flank of the Slumbering Hills within Desert Valley, where the geological framework has been significantly modified by Basin and Range extensional tectonics. The present-day configuration reflects substantial displacement along north- to northeast-trending normal faults, which have down-dropped the volcanic and basin-fill sequences by approximately 900 m to 1,000 m (3,000 ft to 3,300 ft) relative to the exposed basement rocks in the adjacent uplifts. In addition to these dominant structures, northwest-striking faults are present and are interpreted as reactivated regional structural trends, contributing to a complex structural architecture that exerts primary control over lithological distribution and mineralization.

The stratigraphic framework at the property comprises Mesozoic basement rocks overlain by a sequence of Tertiary volcanic and volcanoclastic units. The basement consists of the Auld Lang Syne Group, composed of slate, phyllite, quartzite, and calcareous metasedimentary rocks that have undergone deformation and low-grade metamorphism to greenschist facies, and which are locally intruded by Cretaceous granodioritic to monzonitic bodies. These rocks form the structural footwall to the principal mineralized system. Overlying the basement is a succession of Miocene volcanic rocks, which serve as the primary host sequence for mineralization.

The volcanic stratigraphy begins with a basal sequence of intermediate-composition volcanoclastic rocks and minor flow units, which are overlain by dacitic to basaltic lava flows and associated flow breccias. This sequence is succeeded by felsic pyroclastic units, including pumiceous lapilli tuffs, and culminates in the emplacement of the Sleeper rhyolite. The Sleeper rhyolite, consisting of flows, domes, dikes, and sills characterized by quartz-eye textures and sanidine phenocrysts, represents the principal host to gold-silver mineralization and is interpreted to have played a critical role in the development of the hydrothermal system. Post-mineral volcanic units, including peralkaline ash-flow tuffs, overlie the mineralized sequence and are interpreted to post-date mineralization.

Structurally, the deposit is dominated by a west-dipping, range-bounding normal fault that juxtaposes the Mesozoic basement rocks in the footwall against the Miocene volcanic sequence in the hanging wall. This structure is interpreted to have served as the principal conduit for hydrothermal fluids and represents the first-order control on mineralization. Secondary structures within the hanging wall, including splays, vein arrays, and fault intersections, create localized zones of enhanced permeability and are closely associated with the distribution of mineralized veins, breccias, and stockwork zones. The resulting structural framework is hierarchical, with primary faults controlling the overall geometry of the system and secondary structures governing local mineralization patterns and grade distribution.

At the property scale, the Sleeper deposit is defined by a well-developed mineralized system comprising a central zone of historically mined high-grade quartz–adularia veins surrounded by halos of stockwork and breccia-hosted mineralization, which transition outward into peripheral zones of lower-grade mineralization (Figure 6-3, Figure 6-4, and Figure 6-5).

The deposit extends approximately 1,500 m to 1,700 m along strike, is on the order of 600 m in width, and has a vertical extent exceeding 600 m from near-surface to depth. This geometry reflects the combined influence of structural controls and lithological competency contrasts, which together governed the development of permeability and fluid flow within the hydrothermal system.

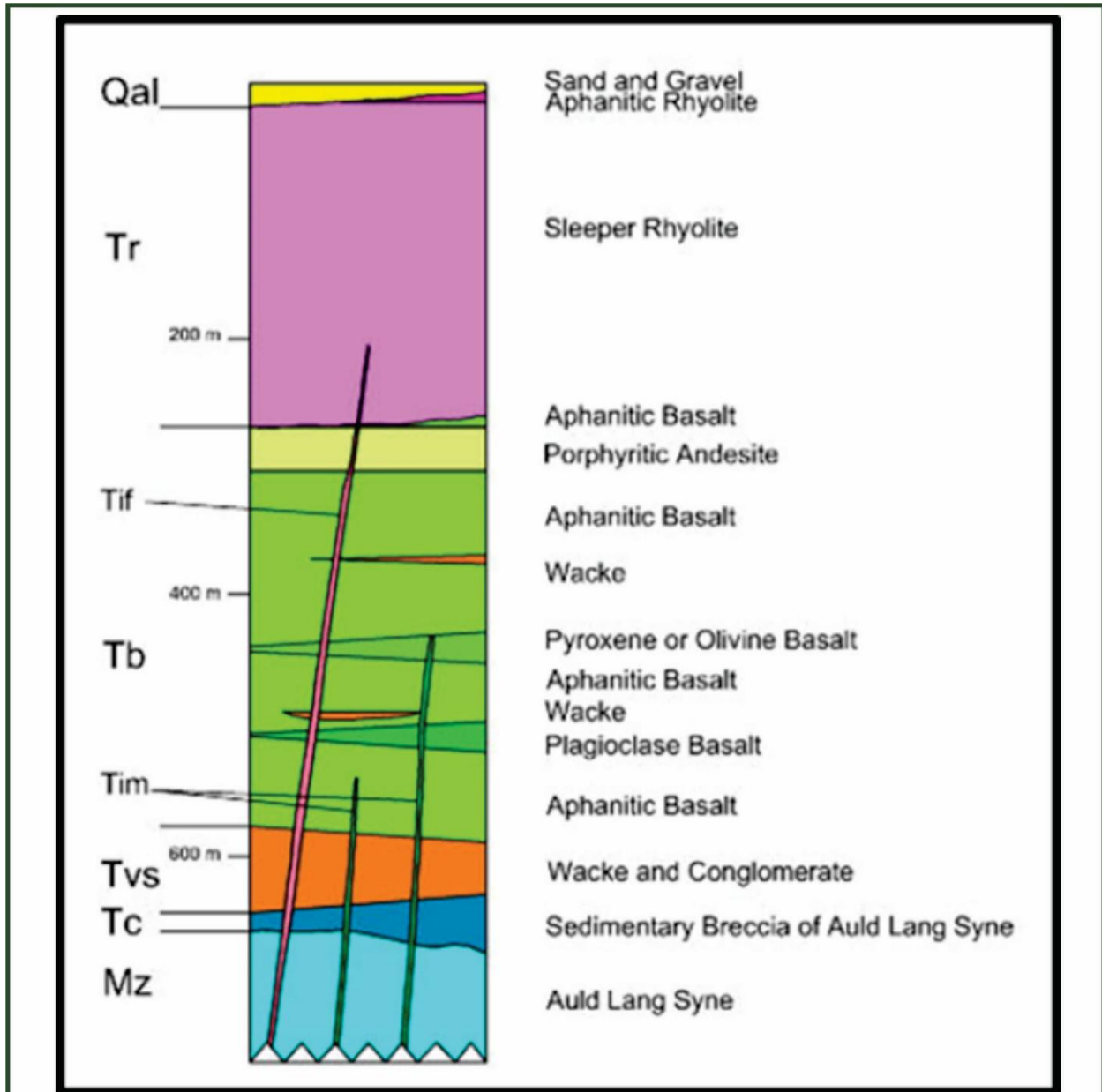


Following historical mining, the geological setting is characterized by extensive envelopes of low-grade stockwork mineralization that surround and underlie the previously mined high-grade vein systems. Remnant mid- to high-grade zones persist beneath and adjacent to mined areas, representing down-dip and along-strike extensions of the primary vein systems as well as mineralization associated with secondary structural zones. Additional mineralization is recognized at targets such as West Wood, where hydrothermal breccia-hosted mineralization is associated with structural complexity and possible intrusive influences, indicating that the mineralizing system remains open and locally underexplored.

The Qualified Person notes that geological continuity is generally well defined within the broader low-grade stockwork domains, which form laterally and vertically continuous mineralized envelopes suitable for bulk-tonnage evaluation. In contrast, high-grade vein-hosted mineralization is discontinuous and strongly controlled by structural features, resulting in significant spatial variability. This variability is an inherent characteristic of the deposit and represents an important consideration in geological modeling and Mineral Resource estimation. The overall geological interpretation is considered robust and appropriate for the current level of study and is consistent with CIM (2014) Definition Standards, CIM (2019) Best Practice Guidelines, and SEC Regulation S-K 1300 reporting requirements.



Figure 6-3: Stratigraphic Column



Note: Description of Map Units Modified from Regional Geologic Map (Ressel et al. 2020)



Paramount Gold Nevada Corp.

Sleeper Gold Mine
 Humboldt County, Nevada
Stratigraphic Column

Source: RESPEC 2023 after Wilson et al 2015.



Figure 6-4: Local Geology

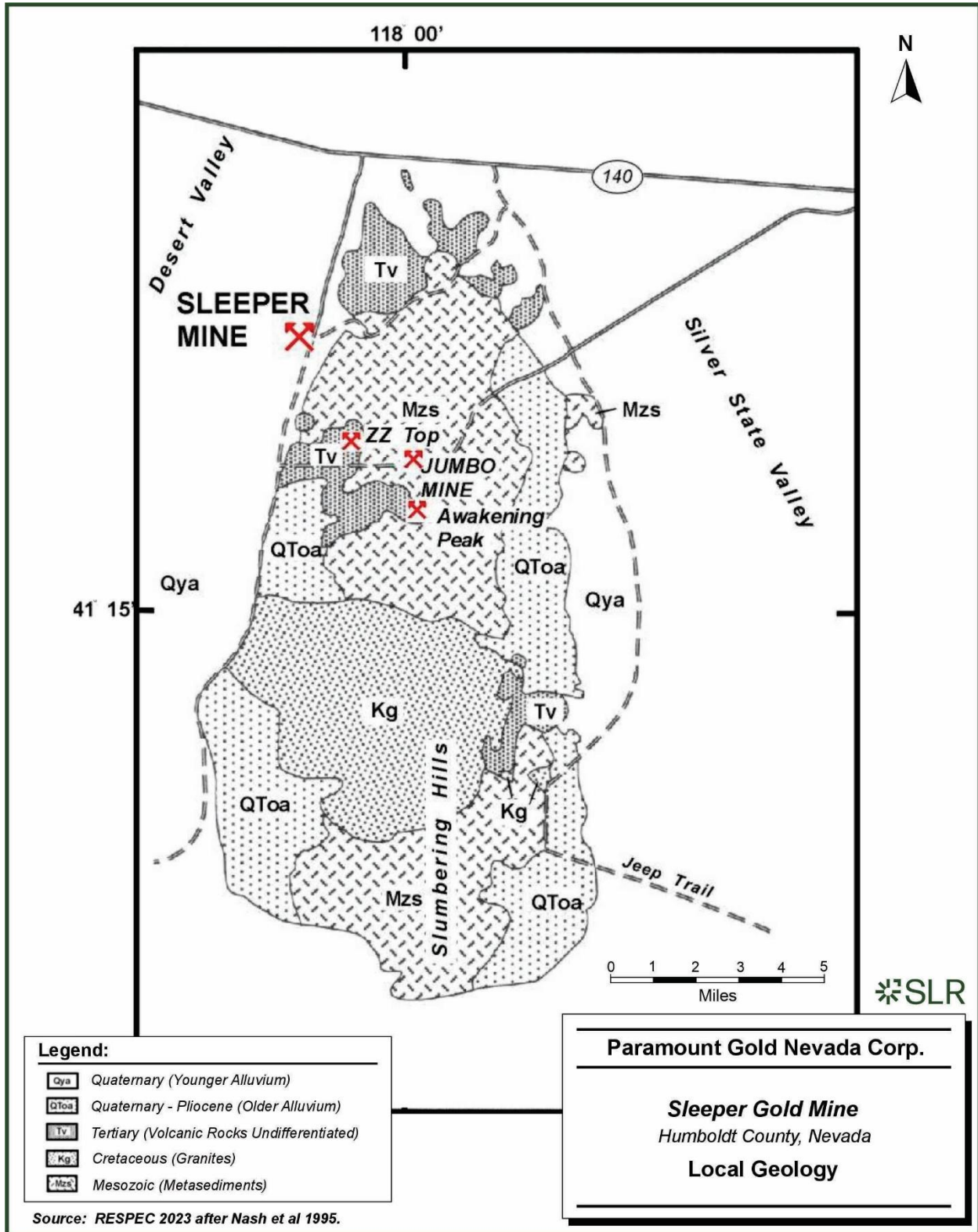
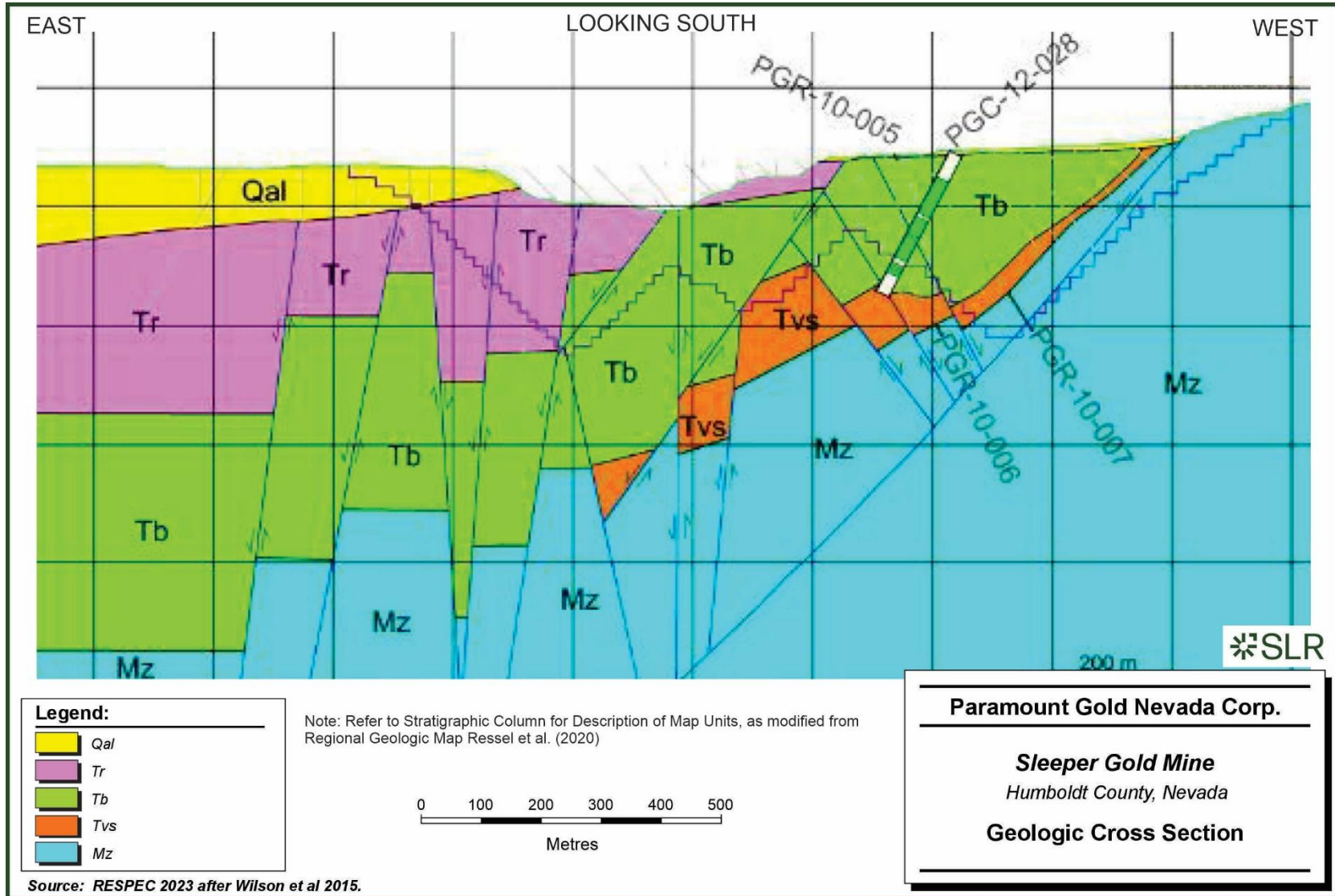


Figure 6-5: Cross Section of Local Geology

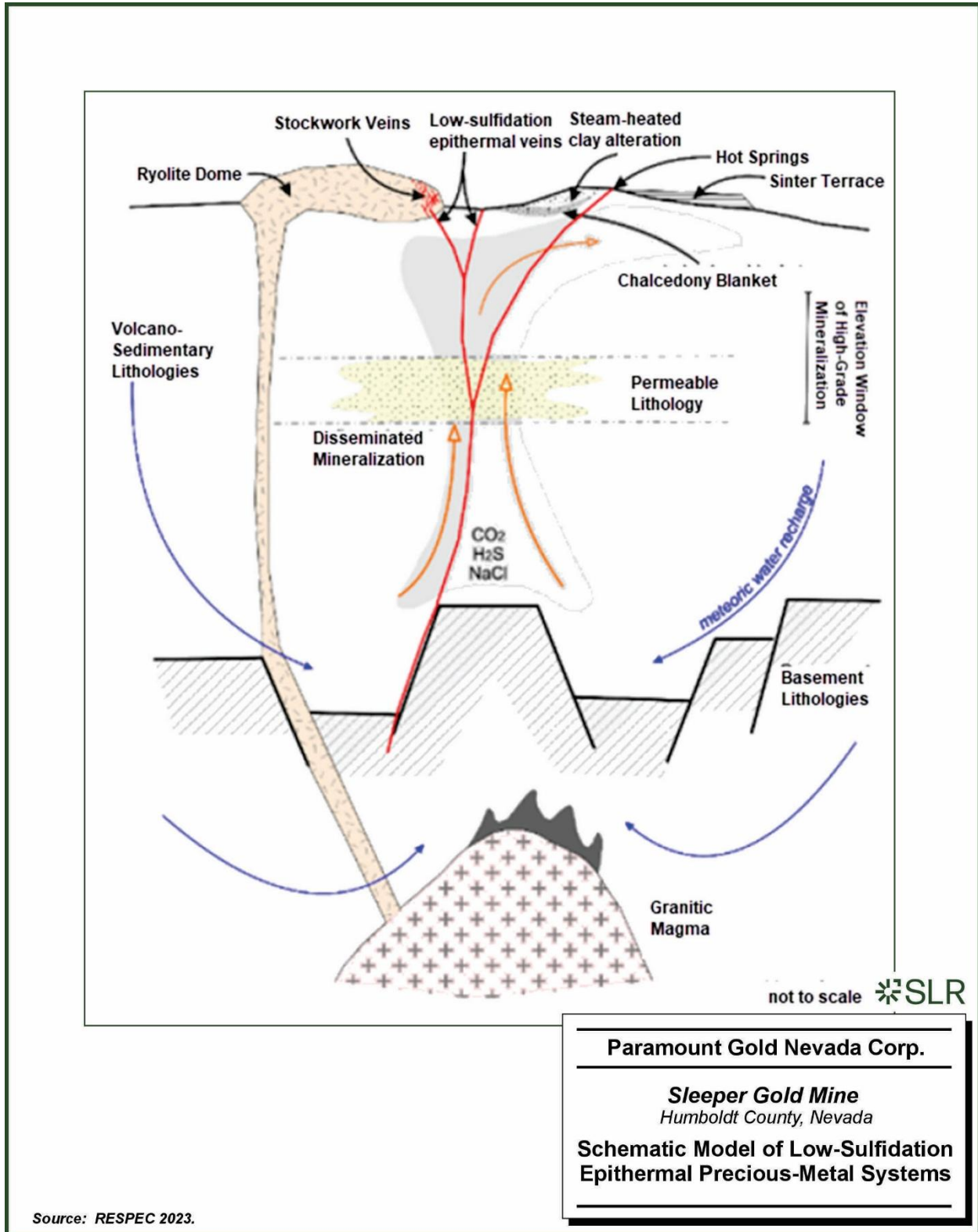


6.3 Mineralization

Mineralization at the Sleeper Gold-Silver Project is characteristic of a low-sulfidation epithermal system (Figure 6-6) developed within a Miocene volcanic center and spatially associated with a major west-dipping, range-bounding normal fault. Gold and silver mineralization occurs predominantly within the hanging-wall volcanic sequence, particularly within the Sleeper rhyolite and underlying basaltic units, and reflects a structurally controlled hydrothermal system with multiple phases of fluid flow and mineral deposition.



Figure 6-6: Schematic Model of Low-Sulfidation Epithermal System



Source: RESPEC 2023.



Mineralization at Sleeper comprises four principal styles that collectively define the deposit architecture: (i) quartz–adularia vein systems, which host the highest grades and represent the primary fluid conduits; (ii) hydrothermal breccias, which occur in structurally prepared zones and locally host moderate- to high-grade mineralization; (iii) stockwork veinlets and disseminated mineralization, which form a broad, lower-grade halo surrounding higher-grade structures; and (iv) alluvial or placer mineralization, derived from erosion of primary mineralized zones and preserved in post-mineral sedimentary units. These styles reflect a continuum of hydrothermal processes ranging from focused fluid flow in discrete structures to more diffuse fluid dispersion into the surrounding host rocks.

Gold and silver mineralization is spatially and genetically linked to the structural framework of the deposit. The principal control is the regional-scale normal fault system, which provided the primary conduit for hydrothermal fluids and established the hanging-wall domain in which mineralization is concentrated. Secondary controls include hanging-wall splays, vein arrays, and structural intersections, which created localized zones of enhanced permeability. These structural features governed the distribution of mineralization and are directly associated with the development of high-grade veins, breccia bodies, and vein swarms. The interaction between structure and lithology, particularly within competent rhyolitic units, played a critical role in focusing fluid flow and controlling mineral deposition.

The mineralization exhibits a clear relationship between style and grade distribution. High-grade mineralization is localized within quartz–adularia vein systems that may extend along strike over significant distances but are typically limited in width and continuity. Bonanza veins were as much as 4 to 5 m wide. Although disrupted by post-ore faulting, the reconstructed strike length of bonanza veins were quite consistent along strike for distances of more than 200 m. These veins can locally exceed 100 g/t Au, particularly within bonanza-grade shoots, although such grades are spatially restricted. Mid-grade mineralization is typically associated with hydrothermal breccias and structurally controlled vein swarms, where grades generally range from approximately 3 g/t Au to 34 g/t Au. These zones represent transitional domains between high-grade vein systems and the broader mineralized envelope. Low-grade mineralization occurs as pervasive stockwork veinlets and disseminations, generally grading less than 3 g/t Au, but forming the bulk of the tonnage within the current Mineral Resource.

Mineralogically, the system is dominated by quartz–adularia gangue assemblages with associated electrum, pyrite, and marcasite, consistent with deposition from near-neutral pH hydrothermal fluids under low-sulfidation epithermal conditions. Alteration is characterized by strong silicification associated with veins and breccias, adularia alteration indicative of boiling conditions, and weaker argillic to sericitic halos in surrounding wall rocks. Distal propylitic alteration is locally developed and reflects background fluid–rock interaction outside the main mineralized zones.

The geometry and continuity of mineralization reflect the underlying structural controls. Mineralized zones extend over a strike length of approximately 1.5 km to 2.0 km, widths of several hundred meters to over 1 km, and vertical extents exceeding 600 m. However, continuity varies significantly by mineralization style, with high-grade veins exhibiting limited lateral and vertical continuity relative to the more continuous, lower grade stockwork domains. This results in a deposit characterized by a highly heterogeneous grade distribution, with localized high-grade zones embedded within a large, lower-grade mineralized envelope.

Following historical mining, the remaining mineralization is dominated by lower-grade stockwork material, down-dip extensions of previously mined high-grade veins, and secondary structural zones hosting moderate-grade mineralization. Discrete zones such as the West Wood area



demonstrate the continued presence of structurally controlled, higher-grade mineralization associated with hydrothermal breccias and intrusive-related features.

6.4 Deposit Types

The Project is classified as a low-sulfidation epithermal gold-silver deposit developed within a middle Miocene volcanic center in an extensional tectonic environment. This classification is supported by the observed geological, mineralogical, structural, and alteration characteristics, including quartz–adularia vein systems, hydrothermal breccias, stockwork mineralization, and associated alteration assemblages typical of epithermal systems formed at shallow crustal levels.

Low-sulfidation epithermal deposits are formed from near-neutral pH hydrothermal fluids, typically derived from magmatic sources and circulating through structurally prepared volcanic sequences. At Sleeper, mineralization is spatially associated with a major west-dipping, range-bounding normal fault and related structural splays, which provided the principal conduits for hydrothermal fluid flow. The deposit is hosted predominantly within Miocene basaltic and rhyolitic volcanic rocks, with the Sleeper rhyolite representing the primary host lithology. The structural and lithological framework is consistent with the development of an epithermal system in an extensional volcanic setting, where repeated fault movement and magmatism facilitated fluid migration and metal deposition.

The mineralization at Sleeper exhibits the key features of low-sulfidation epithermal systems, including banded quartz–adularia veins, chalcedonic silica, and hydrothermal breccias, with associated gold occurring primarily as electrum. Sulfide mineralization is generally limited to pyrite and marcasite, reflecting relatively low sulfur fugacity conditions compared to high-sulfidation systems. The alteration assemblage is dominated by silicification and adularia, with subordinate argillic to sericitic halos and distal propylitic alteration, consistent with deposition from low-temperature hydrothermal fluids under boiling and fluid-mixing conditions.

The deposit displays a well-developed vertical and lateral zonation typical of epithermal systems. High-grade mineralization occurs in structurally controlled quartz–adularia veins and associated breccias within the central portion of the system, representing zones of focused fluid flow and boiling. These zones transition outward and downward into intermediate grade breccias and vein swarms, and ultimately into broad envelopes of low-grade stockwork and disseminated mineralization. This zonation reflects decreasing fluid flux and permeability away from the principal structural conduits and is consistent with established genetic models for low-sulfidation epithermal deposits.

The overall geometry and scale of the Sleeper system are also consistent with this deposit type, with mineralization extending over approximately 1.5 km to 2.0 km along strike, several hundred meters in width, and more than 600 m vertically. The system comprises a combination of discrete high-grade vein structures and a large, lower-grade mineralized envelope, reflecting both focused and diffuse hydrothermal processes. The presence of alluvial or placer mineralization derived from erosion of primary mineralized zones further supports the interpretation of a shallow-level epithermal system that has undergone post-mineral erosion and sediment redistribution.



7.0 Exploration

Exploration at the Project comprises an extensive, multi-decade dataset integrating drilling, geochemical sampling, geological mapping, and a wide range of geophysical surveys completed by multiple operators from the early 1980s through 2013. The deposit was discovered beneath shallow alluvial cover through drilling, and subsequent programs have included more than 4,400 drill holes, extensive soil and rock geochemical datasets, and numerous geophysical surveys, including gravity, airborne and ground magnetics, induced polarization (IP), resistivity, magnetotelluric (MT), and seismic methods

7.1 Exploration

7.1.1 Paramount Gold Geophysical Surveys (2010–2013)

7.1.1.1 Overview (2010–2013)

Following the acquisition of the Project in 2010, Paramount Gold undertook a series of targeted geophysical surveys between 2010 and 2013 to enhance the understanding of the structural and lithologic framework controlling mineralization. These surveys were designed to complement and refine the extensive historical geophysical database and were interpreted by a qualified geophysical consultant in the context of both newly acquired and legacy datasets. The primary objective of this work was to delineate structural corridors, identify lithologic contrasts, and define alteration patterns associated with the hydrothermal system.

7.1.1.2 Gravity Survey (2012)

In 2012, Paramount Gold completed a detailed ground gravity survey over the southern portion of the property. The survey was conducted between late March and mid-April 2012 and comprised approximately 1,019 gravity stations collected on variable grid spacing, including 100 m and 200 m grids, supplemented by wider-spaced reconnaissance stations.

Gravity measurements were acquired using LaCoste & Romberg Model-G gravity meters, with station locations surveyed using Trimble Real-Time Kinematic (RTK) and Fast-Static GPS methods to ensure accurate positioning and elevation control. The dataset was processed to Complete Bouguer Anomaly using a range of assumed densities, with a representative density of approximately 2.35 g/cm³ applied based on prior work in the area. Terrain corrections were applied over multiple radii extending to regional scales, and the processed data were gridded and filtered to generate regional, residual, and horizontal gradient products suitable for structural interpretation.

Interpretation of the gravity data identified three north–south–trending structural corridors extending more than 30 km southward from the Sleeper deposit. These features define a series of basin and horst geometries and are interpreted to represent fundamental controls on the distribution of mineralization and the architecture of the hydrothermal system.

7.1.1.3 Induced Polarization and Electrical Surveys (2012–2013)

Induced polarization (IP) and associated resistivity surveys were conducted during the 2012–2013 period to further investigate subsurface chargeability and resistivity contrasts. These surveys were designed to identify zones of sulfide mineralization, silicification, and hydrothermal alteration that may not be evident from surface observations or magnetic data.



The IP data were integrated with gravity and magnetic datasets to refine interpretations of subsurface structures and alteration zones. Chargeability anomalies identified through these surveys were interpreted as zones of disseminated sulfides and hydrothermal activity, providing additional drilling targets and contributing to the overall understanding of mineralization controls.

7.1.1.4 Data Integration and Interpretation (2010–2013)

All geophysical datasets acquired by Paramount Gold between 2010 and 2013 were integrated with historical geophysical, geological, and drilling data to produce a coherent interpretation of the property-scale structural framework. The combined dataset allowed for improved delineation of major structural trends, basin geometry, and potential mineralized corridors extending beyond the limits of historical mining.

This integrated interpretation confirmed that the Sleeper deposit is situated within a structurally complex setting characterized by major north–south structural corridors and associated secondary structures that control the localization of high-grade vein systems and broader zones of disseminated mineralization. The results of the Paramount Gold geophysical programs have therefore provided a critical foundation for ongoing exploration targeting, particularly in areas beneath post-mineral cover and along underexplored structural trends.

7.1.2 Exploration Targeting – QP Comment

Exploration targeting at Sleeper is based on integrating geological, geochemical, and geophysical datasets, with particular emphasis on structural controls and the distribution of hydrothermal alteration. High-grade mineralization is interpreted to be localized along steeply dipping structural zones and associated vein systems, while broader zones of lower-grade mineralization occur within stratigraphically controlled envelopes surrounding these structures.

Geophysical data, particularly gravity and IP surveys, have played a critical role in identifying structural corridors, basin architecture, and potential alteration zones beneath the cover. These features provide key vectors for exploration, particularly in areas beyond the limits of historical mining and drilling. Targets include down-dip and along-strike extensions of known vein systems, structurally controlled high-grade zones, and underexplored areas beneath post-mineral cover, including West Wood within the broader mineralized halo.

The QP emphasizes that these exploration targets are conceptual and based on geological interpretation supported by available data. There has been insufficient exploration to define Mineral Resources in these areas, and it is uncertain whether further exploration will result in the delineation of additional Mineral Resources.

7.2 Drilling

Drilling at the Project has been conducted by numerous operators over several decades and has served as the primary source of geological and grade information supporting the current understanding of the deposit. As of the effective date of this Technical Report, Paramount Gold and the Project's predecessor owners have completed approximately 4,400 drill holes totaling about 638,000 m of drilling completed between 1983 and 2021 by multiple operators (Table 7-1 and Figure 7-1). Drilling methods are dominated by Reverse Circulation (RC), with limited core and sonic drilling incorporated in later programs. Some historical drilling records lack complete information, including hole type and total depth for certain programs, and these data gaps introduce uncertainty that has been considered in the evaluation of the dataset and Mineral Resource classification.



Table 7-1: Drill Hole Database

Year	Operator / Property	Program / Area	Drill Type	Number of Drill Holes	Total Depth Drilled (m)
1983–2010	Unknown	Exploration	RC	20	780
1983–1995	AMAX	Exploration / Production	RC	3,668	509,043
1989	NGM	Exploration	RC	9	438
1997	Placer Dome	Exploration	RC	47	13,323
1996–1997	X-Cal	Exploration	RC	140	27,700
1998–2003	X-Cal*	Exploration	RC	83	N/A
2003–2007	X-Cal	Exploration	RC	169	47,169
2004–2005	New Sleeper Gold	Exploration	RC	69	18,363
2007–2008	Evolving Gold*	Exploration	RC	34	6,636
2009–2012	Montezuma Mines*	Exploration	RC	11	1,940
2010–2021	Paramount Gold	Exploration	RC	155	29,752
		Waste Rock Dump	RC	65	2,397
			SONIC	9	261
		Heap Leach Pad	CORE	40	978
		TSF	SONIC	83	825
Total				4,596	659,605

Note: * reported historical drilling not contained in Mineral Resource Database

Reconciliation of historically reported drilling totals with the drill hole database provided to SLR indicates that, while the datasets are broadly consistent in overall scale and principal contributors, differences exist due to incomplete, missing, or unverified data within the database available for review and use in the Mineral Resource Estimate (MRE).

AMAX drilling (3,668 holes; approximately 509,000 m), which comprises most of the dataset, is fully reconciled between sources and serves as the primary basis for the database. NGM (9 holes; 438 m) and Placer Dome (47 holes; 13,323 m) drilling was also consistent across datasets and was considered complete.

Discrepancies were identified between historical drilling records and the drill hole database provided to SLR for the X-Cal, Paramount Gold, and related programs. Historical records indicate that X-Cal completed 394 drill holes, including 83 holes drilled between 1998 and 2003 for which total depths are not reported. The database provided to SLR includes 309 X-Cal holes totaling 74,869 m. Consequently, a portion of the X-Cal drilling—primarily from the 1998–2003 program—was excluded from the Mineral Resource Estimate (MRE) due to insufficient or unverifiable supporting information.

Historical documentation also indicates that Evolving Gold drilled 34 holes totaling 6,636 m between 2007 and 2008, and Montezuma Mines drilled 11 holes totaling 1,940 m between 2009 and 2012. These drill holes were not included in the database provided to SLR and were therefore excluded from the MRE.



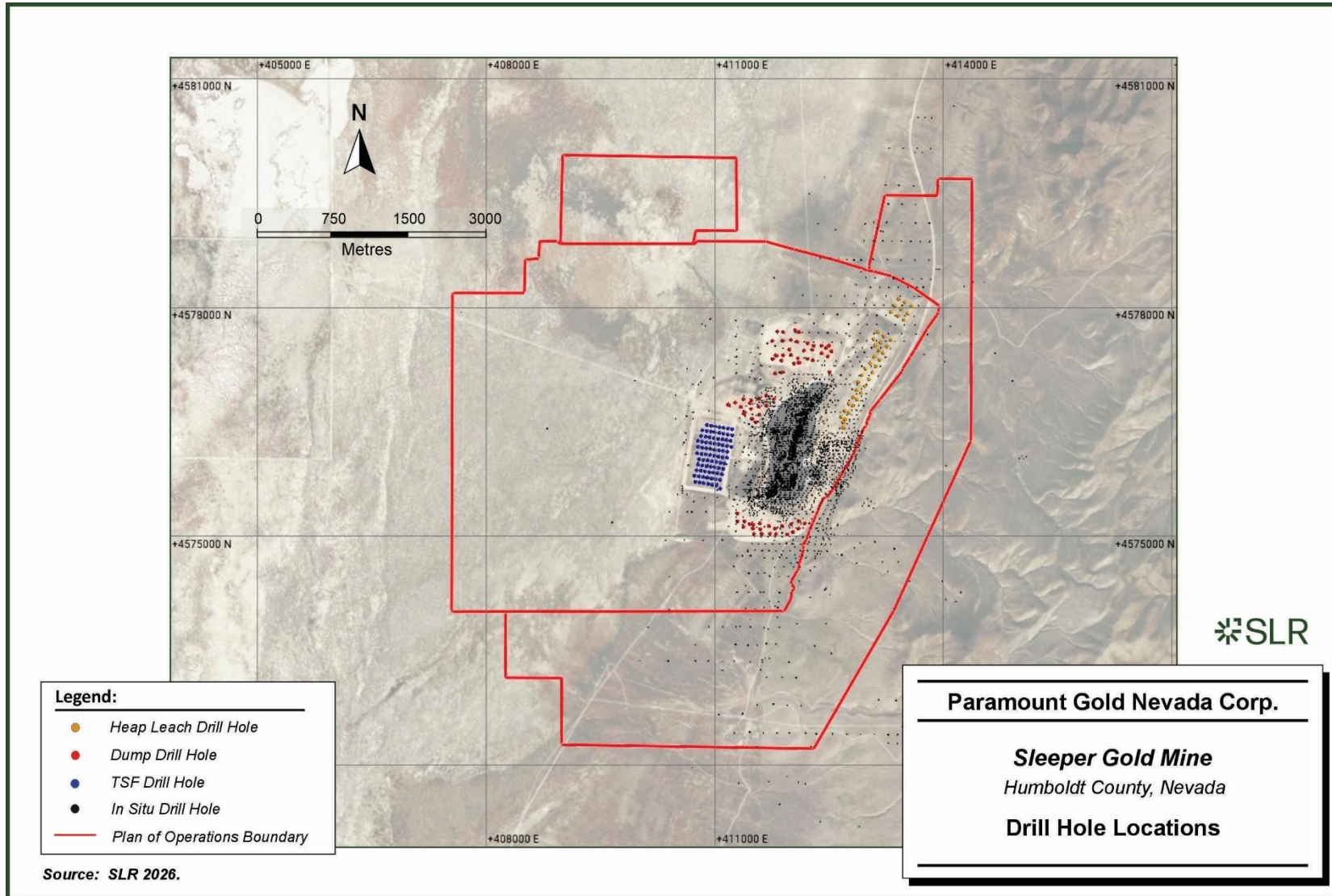
A similar variance is noted for Paramount Gold drilling. Records report 155 drill holes totaling 29,752 m, whereas the database provided to SLR contains 136 holes totaling 23,756 m. The exclusion of 13 holes (approximately 3,300 m) reflects the absence of complete or verifiable supporting data at the time of review. As this drilling is relatively recent, the omission is noted as a limitation on overall data completeness.

In contrast, New Sleeper Gold drilling shows consistency between datasets, with 69 drill holes reported and only a minor variance of approximately 300 m in total drilled length, which is not considered material. The 20 drill holes classified as “Unknown” (780 m) are present in both datasets; however, due to the lack of ownership attribution and supporting metadata, their use remains limited and subject to further verification.

Overall, the historically reported dataset comprises 4,596 drill holes totaling 656,960 m, compared to 4,455 drill holes (exploration, waste rock dumps, heap leach pads and TSF) totaling 645,033 m in the database provided to SLR, resulting in a net shortfall of 215 drill holes totaling 14,584 m. These differences are primarily attributable to incomplete X-Cal and Paramount Gold datasets. Consistent with S-K 1300 and CIM (2019) guidance, the QP has excluded data that could not be verified or adequately supported and considers the remaining dataset sufficient to support the current Mineral Resource classification, while recognizing that the excluded data represent a limitation on overall data completeness.



Figure 7-1: Drill Hole Location Map



7.2.1 Paramount Gold (2010–2021)

Drilling conducted by Paramount Gold Nevada Corp. and Silver Corp. between 2010 and 2021 represents the most recent phase of systematic exploration at the Project and was undertaken to validate historical data, refine the geological model, and test extensions of known mineralization. A total of 136 drill holes comprising approximately 23,756 m were included in the drill hole database provided to SLR and used in the Mineral Resource Estimate (MRE). Drilling was primarily focused on the Sleeper deposit core area and surrounding zones, including structurally controlled targets and underexplored areas such as West Wood and areas beneath post-mineral cover.

7.2.1.1 2010 Drilling

The 2010 program comprised 14 drill holes totaling approximately 4,123 m and represents the initial phase of Paramount Gold's drilling following acquisition of the project. This program focused on the central Sleeper deposit, including areas within and adjacent to the historical open pit, with the objective of validating historical drilling results and confirming the continuity of known mineralization. Limited step-out drilling also tested extensions of mineralization along the primary structural trends associated with the Sleeper vein system.

7.2.1.2 2011 Drilling

The 2011 program was the largest of the Paramount Gold campaigns, comprising 93 drill holes totaling approximately 9,028 m. During this phase, drilling focused on expanding mineralization within the broader low-grade halo surrounding the historical high-grade vein systems, as well as testing along-strike and down-dip extensions of the principal structures. Additional drilling targeted peripheral zones, including the West Wood area and other structurally controlled targets interpreted to host hydrothermal breccias and vein-related mineralization.

7.2.1.3 2012 Drilling

The 2012 program included 19 drill holes totaling approximately 6,158 m and was designed to follow up on targets generated from the 2011 drilling and concurrent geophysical surveys. Drilling focused on structurally controlled zones identified through gravity and IP data, including areas south of the historical pit and beneath post-mineral cover. The program emphasized refining the geometry of mineralized zones and testing newly identified structural corridors interpreted to control mineralization.

7.2.1.4 2013 Drilling

The 2013 program comprised 10 drill holes totaling approximately 4,448 m and represents the final phase of Paramount Gold's drilling during this period. Drilling was more selective and focused on priority targets identified from previous programs, including infill and step-out drilling in the core deposit area and targeted testing of structurally controlled zones and peripheral exploration areas.

7.2.1.5 2021 Drilling

The 2021 program consisted of 6 RC exploration holes drilled to the southeast of the open pit. A total of 2,645 m were drilled. One of the holes was an RC pre-collar in the West Wood zone. However, the planned core tail portion of the hole was never initiated due to budgeting issues at the time.



7.2.2 Drill Hole Orientation

Historical drilling at the Project was predominantly completed using vertical reverse circulation (RC) drill holes, reflecting the early focus on delineating near-surface mineralization and supporting open-pit mine development. This approach was appropriate for defining the broad, laterally continuous low-grade mineralized envelope; however, vertical drilling provides limited control on the true thickness and geometry of steeply dipping structures.

Subsequent drilling programs incorporated angled holes, particularly core drilling, to better define the orientation and continuity of steeply dipping vein systems, hydrothermal breccias, and structurally controlled zones. Drill hole orientations and intercept relationships indicate that high-grade mineralization is commonly associated with steeply dipping structures, and angled drilling was therefore required to adequately characterize these features and support geological modeling.

Paramount Gold drilling (2010–2021) continued to utilize primarily RC methods with a combination of vertical and locally angled holes, targeting both confirmation of historical mineralization and improved definition of structural controls. Drill orientations were selected to test down-dip and along-strike extensions of known mineralized zones and to evaluate targets identified through integrated geological and geophysical interpretation.

The QP considers that, while the predominance of vertical drilling in the historical dataset introduces some uncertainty in defining true thickness and structural geometry, the incorporation of angled drilling and the overall drilling density provides an adequate basis for interpreting mineralization continuity and supporting the current Mineral Resource Estimate.

7.2.3 Drill Hole Collar Surveys

Drill hole collar locations for historical and more recent drilling programs were established using survey methods consistent with industry practices at the time of drilling. Early drilling campaigns (1980s–1990s) generally relied on conventional ground survey techniques, including optical and manual methods, which may be subject to greater positional uncertainty relative to modern standards.

More recent programs, including those conducted during the 2000s and by Paramount Gold Nevada Corp. between 2010 and 2013, utilized improved survey techniques, including differential Global Positioning System (GPS) methods, providing greater spatial accuracy for collar positioning. Collar coordinates were compiled into a centralized database and, where possible, validated against historical records and mapping.

For certain historical drill holes, survey control data are incomplete or lack documentation regarding survey methodology and accuracy. In accordance with S-K 1300 requirements and CIM (2019) Best Practice Guidelines, the QP has assessed these limitations and considers that the overall collar dataset is sufficiently reliable to support Mineral Resource estimation, with associated uncertainties addressed during the Mineral Resource estimation process.

7.2.4 Drill Hole Coordinate System

Drill hole collar locations at the Project have been recorded using multiple coordinate systems over time, reflecting changes in surveying practices and data management by successive operators.

During initial exploration in the early 1980s, AMAX established a local mine grid coordinate system based on a truncated State Plane system referenced to NAD27, Western Nevada Zone,



in feet. This local grid was defined such that local coordinates of $X = 0$ and $Y = 0$ correspond to State Plane coordinates of $X = 640,000$ ft and $Y = 2,390,000$ ft, respectively. This coordinate system remained in use for all drilling and data management activities through August 2004.

In August 2004, X-Cal converted all relevant project data, including drill hole collar locations, to the Universal Transverse Mercator (UTM) coordinate system, NAD27, Zone 11, in meters. The transformation included the establishment of a local mine grid reference tied to UTM coordinates (local Mine Grid $X = 0$ corresponding to UTM Easting 410,125.39 m and local Mine Grid $Y = 0$ corresponding to UTM Northing 4,573,808.38 m).

All drilling completed after this conversion, including the Paramount Gold drilling programs (2010–2021), was surveyed directly in UTM NAD27 Zone 11 coordinates (meters). Paramount Gold did not resurvey historical drill hole collars, as many locations had been disturbed by mining or reclamation activities. Instead, collar data were compiled from historical records, including drill logs and electronic databases.

A review of the collar dataset indicates that most historical collar coordinates were transcribed into electronic format during the X-Cal conversion and show good agreement between original mine grid records and UTM-transformed coordinates.

In accordance with S-K 1300 and CIM (2019) Best Practice Guidelines, the QP considers the coordinate system transformation and compilation process to be appropriate for Mineral Resource estimation, with any residual uncertainty associated with historical collar locations addressed through data validation procedures and the Mineral Resource estimation process.

7.2.5 QP Comment – Drilling Data Considerations and Limitations

While the overall drilling database is extensive, certain portions of the historical drilling record are incomplete or lack detailed documentation regarding drilling methods, sampling procedures, and survey control. Some historical programs, although conducted by reputable operators, do not include sufficient supporting information on data-acquisition protocols, which introduces uncertainty and implications for the confidence and classification of Mineral Resources.

Despite these limitations, the QP considers that the available drilling data, when integrated with geological interpretation and supported by more recent drilling and validation work, provides an adequate basis for the current Mineral Resource estimates. Continued drilling, particularly using modern standards and oriented core techniques, is expected to further refine the geological model, improve confidence in structural interpretations, and support potential future upgrades in resource classification.

7.3 Hydrogeology Data

The Project is located along the eastern margin of Desert Valley in Humboldt County, Nevada, where basin-fill alluvium overlies a sequence of Mesozoic and Cenozoic bedrock units. The hydrogeologic system is well characterized based on pre-mining investigations, extensive dewatering records from mine operations (1985–1996), and post-closure monitoring data collected since 1996. SLR has reviewed numerous technical reports prepared over the past three decades, including documents submitted to state and federal regulatory agencies such as the Nevada Division of Environmental Protection (NDEP), Bureau of Mining Regulation and Reclamation (BMRR), and the BLM.

Since the Sleeper pit has previously been dewatered by a network of dewatering wells (61 drilled over the mine life), there is an extensive physical and chemical hydrogeological database



collected from these dewatering wells and a supporting network of monitoring wells (68 installed over the mine life). At full capacity, the dewatering system discharged 87,200 m³/day (16,000 US gallons per minute [gpm]) from 12 pumping wells installed into the bedrock and 28 interceptor wells installed in the basal gravel aquifer.

7.3.1 Physical Hydrogeology

Hydrostratigraphic units generally consist of layered lacustrine clays, silts, and sands overlying alluvial gravel, followed by faulted rhyolite bedrock. The lacustrine sands (known locally as the intermediate sands) are interpreted to have been beach deposits on the shores of periglacial Lake Lahontan. The intermediate sands were de-watered under an induced hydraulic gradient from the intermediate sands into the basal alluvial gravel. As such, no dewatering wells were installed in the intermediate sands (WMC 1995).

The basal gravel is the primary aquifer and the main source of recharge to the pit lake. The basal gravel is thin to non-existent on the east wall of the pit. Approximately 70% of the discharged groundwater was extracted from the basal gravel aquifer (WMC 2005). Groundwater discharged from the interceptor wells (installed in the basal gravel on the west side of the pit) is intercepted prior to discharging to the pit.

Faults transecting the rhyolite bedrock have been found to be generally non-transmissive and effectively compartmentalize groundwater flow in the bedrock. There is a fracture zone underlying the base of the pit (below 1,087 masl), known as the Deep Fracture System (DFS), that was targeted to complete bedrock wells. Approximately 22 % of the discharged groundwater was extracted from DFS bedrock wells (WMC 2005). Generally, de-pressurizing the deep fracture system induced downward flow from fractures above and allowed for efficient dewatering of the bedrock pit walls and floor.

However, in zones where pressurized shallow fracture (PSF) systems were found not to be connected to the DFS and were at risk of de-stabilizing the pit walls, additional bedrock wells were installed. Approximately 9% of the discharged groundwater was discharged from PSF bedrock wells (WMC 2005).

A total of approximately 30 dewatering wells were operational at any one time. Some redundancy was built into the dewatering well network to allow for well and pump maintenance; as such, 61 dewatering wells were drilled over the mine life (WMC 2005). Approximately 5,450 m³/day (1,000 gpm) of the discharged water was used for mine operation (heap process water, mill operations, and dust control), while the remainder was discharged into a temporary wetland comprised of engineered and permitted dyke structures that impounded 47 Mm³ (3,800 acre-feet) of water located in the middle of the Desert Valley (WMC 2005). Of the discharged water, approximately 40% infiltrated into the subsurface, while the remainder evaporated (WMC 2005). The discharge system consisted of 4.8 km of conveyance channel and 17.7 km of containment dyke and required excavation, placement, and compaction of 264,000 m³ (350,000 yd³) of material.

Basal gravel and bedrock aquifer properties have been reasonably assessed and presented in Table 7-2.



Table 7-2: Hydrostratigraphic Unit Hydraulic Properties

Hydrostratigraphic Unit	Hydraulic Conductivity (m/s)	Specific Storage ft ⁻¹	Specific Yield
Lacustrine Deposits	4E-8 to 2E-5	2E-5 to 3E-3	0.1 to 0.15
Basal Gravel Aquifer	1E-5 to 1E-4	5E-5 to 5E-4	0.1 to 0.2
Volcanic Bedrock	4E-7	3E-7	0.0001
Source: WMC 1995.			

Using the hydraulic properties presented above, a three-dimensional numerical model using MODFLOW-USG was calibrated with a 90% to 95% correlation coefficient to measured piezometric heads in the aquifers (Piteau 2021). The monthly water balance of the calibrated model is presented in Table 7-3.

Table 7-3: Monthly Water Balance for the Calibrated Pit Lake Numerical Model

Month	Water Level Elevation (masl)	Surface Area of Open Water (m ²)	Precipitation (m ³ /day)	Evaporation (m ³ /day)	Lake Water Balance (m ³ /day)
October	1,248	655,290	255	1,739	-1484
November	1,248	655,290	245	940	-696
December	1,248	655,290	250	576	-326
January	1,248	655,290	190	603	-413
February	1,248	655,290	120	875	-755
March	1,248	655,290	228	1,755	-1,527
April	1,248	655,290	315	2,076	-1,761
May	1,248	655,290	456	2,913	-2,457
June	1,248	655,290	163	3,755	-3,592
July	1,248	655,290	65	4,076	-4,011
August	1,248	655,290	38	2,870	-2,832
September	1,248	655,290	92	2,755	-2,663
Source: Piteau 2021.					

The water balance is consistent with a net evaporative loss whereby there is no significant recharge to the subsurface.

The model was run under two climactic scenarios: 1) current climactic conditions and 2) assuming a 15% increase in evapotranspiration. The model showed that, under each scenario, the pit lake was a regional groundwater receptor, that the pit lake was not recharging aquifers in any direction, and that it would continue to do so for at least 100 years into the future. The physical hydrogeology data collected to date and the calibrated model show that physical hydrogeology at Sleeper is reasonably well understood.



7.3.2 Hydrogeochemistry

A database comprising 24 years of quarterly monitoring of pit lake water quality has been developed. The data set includes depth profiling within the pit lake. Since the pumps were turned off in 1996, the pit lake water quality has consistently improved (Table 7-4). Except for isolated exceedances of fluoride, the 2020 pit lake water quality generally met the Nevada Profile III Reference values.

While the mine was operational, a groundwater quality database was developed consisting of groundwater samples collected from exploration drill holes, groundwater monitoring wells and dewatering wells distributed as outlined in Table 7-5.

No formal quality assurance/quality control (QA/QC) system was implemented in the characterization of groundwater and pit lake quality.

Groundwater quality reported from each hydrostratigraphic unit was generally diagnostic of that hydrostratigraphic unit. Generally, groundwater at the margins of the basin was younger calcium-bicarbonate type water, whereas groundwater at the center of the basin was older and trended toward a sodium-chloride type water. Since the groundwater quality from each hydrostratigraphic unit is diagnostic, the influence of leakage across hydrostratigraphic unit boundaries can be qualitatively determined. Based on hydrogeochemical data, as dewatering progressed, an increasing percentage of the groundwater discharge originates from the basal gravel aquifer but also an increasing percentage is older water originating from the center of the basin (WMC 1995).

Exceedances of U.S. Environmental Protection Agency (USEPA) water quality standards in the discharged groundwater to the temporary wetland are presented in Table 7-6.

Table 7-4: Evolution of Pit Lake Water Quality

Analyte	1996 Lake	2008 Lake	1Q2011	1Q2014	1Q2020
Alkalinity (total)	nr	62.9	53	66	75
pH (pH units)	1.9	7.6	7.78	7.77	7.27
Antimony	0.12	<0.003	0.002	<0.002	<0.0025
Arsenic	31.8	0.002	0.005	0.006	0.01
Cadmium	0.12	<0.002	<0.002	<0.002	<0.0020
Chloride	178	280	280	280	310
Copper	9.01	0.007	0.002	<0.002	<0.0020
Iron	1,348	<0.05	<0.1	<0.1	<0.20
Lithium	nr	nr	nr	nr	<0.20
Magnesium	253	52	57	59	60
Manganese	27.7	0.098	0.074	0.063	0.05
Molybdenum	nr	nr	nr	nr	<0.040
Nickel	16.1	0.06	0.045	0.034	<0.050
Nitrate	0.53	0.3	<0.5	<0.5	<0.1
Phosphorus	nr	nr	nr	nr	<1.0
Potassium	32	24	29	29	31



Selenium	0.02	0.006	<0.01	<0.01	<0.0050
Sodium	241	330	340	350	390
Strontium	nr	nr	nr	nr	1
Sulfate	6,366	1,330	1,300	1,400	1,400
Thallium	1.37	0.002	0.003	0.002	0.002
Tin	nr	nr	nr	nr	<0.20
Total Dissolved Solids	9,000	2,480	2,600	2,600	2,700
Uranium	nr	nr	nr	nr	<0.0050
Vanadium	nr	nr	nr	nr	<0.020
Zinc	39.5	0.015	0.06	0.05	<0.040

Source: Piteau 2021.
Notes:
nr analyte concentration not reported
< less than the method detection indicated
All concentrations (except pH) are reported as mg/litre unless otherwise indicated

Table 7-5: Groundwater Sample Distribution

Source	Total Number of Samples Collected
Lahontan Clays	66
Intermediate Sand	20
Basal Gravel Aquifer	57
Bedrock	14
Regional Monitoring Locations	73
Composite Dewatering Discharge	38

Source: WMC 1995.

Table 7-6: Exceedances of USEPA Water Quality Standards in Dewatering Discharge

	Primary Drinking Water	Irrigation	Livestock Watering	Aquatic Life	Wildlife Propagation
Dewatering Discharge	Arsenic Selenium	TDS Fluorine Boron	None	Fluorine Arsenic Boron Copper Zinc	Bicarbonate Alkalinity

Source: WMC 1995.
Notes:
TDS total dissolved solids



7.4 Geotechnical Data

No relevant geotechnical data have been collected by Paramount Gold recently, and the authors are not aware of any existing geotechnical data. The SLR QP recommends that Paramount Gold compile relevant historical geotechnical data.



8.0 Sample Preparation, Analyses, and Security

This section has been reviewed and edited by SLR and is derived, where applicable, from RESPEC (2023) and Wilson and SRK (2012). SLR reviewed the information for completeness, internal consistency, and compliance with SEC Regulation S-K 1300, CIM (2019) Best Practice Guidelines.

The review covered sampling methods, sample preparation and analytical procedures, QA/QC protocols, and sample security practices. Supporting documentation, including original sampling records, full QA/QC datasets, and laboratory certificates, was not available for independent verification; therefore, the review relies on information presented in the source reports.

The SLP QP considers the sampling, preparation, analytical, and security practices to be consistent with industry standards for the deposit type and period of work. Despite data limitations, the information is sufficient to support the Mineral Resource Estimate, with uncertainties addressed through data validation and reflected in the Mineral Resource classification.

8.1 Sample Method and Approach

Sampling at the Project was completed by multiple operators between 1983 and 2013 and forms the basis of the geological and assay database supporting the MRE. Sampling methods evolved over time; however, the overall approach is considered appropriate for the style of mineralization and consistent with industry practice.

8.1.1 Historical (1983–2010)

Historical sampling was conducted by AMAX (1983–1995), NGM (1989), Placer Dome (1997), X-Cal (1996–2007), and New Sleeper Gold (2004–2005). Approximately 95% of the drill hole database comprises RC drilling. RC samples were collected at the rig using cyclone and splitter systems to produce representative subsamples at regular intervals, designed to capture lithologic and mineralization variability.

During the AMAX period, sampling focused on near-surface bulk-tonnage mineralization, predominantly using vertical drill holes. Documentation is limited; however, methods are consistent with industry practice for the period. NGM and Placer Dome used similar RC-based approaches with limited documentation but no identified deviations from standard practice.

X-Cal and New Sleeper Gold implemented more structured procedures, including cyclone and splitter sampling, systematic labeling and tracking, and field duplicates at approximately 150 ft intervals. Limited diamond drilling was completed in structurally complex areas; core was logged and sampled by lithology, alteration, and mineralization, and split with half retained.

Sampling targeted both the low-grade mineralized envelope and higher-grade structurally controlled mineralization associated with veins and hydrothermal breccias. Where coarse gold was suspected, a metallic screen fire assay was used to address sampling bias.

8.1.2 Paramount Gold (2010–2021)

Sampling during the Paramount Gold and Silver Corp. programs (2010–2021) represents the most recent data collection phase and was completed to validate historical data, refine the geological model, and test extensions of mineralization. A total of 155 drill holes (29752 m) were sampled, primarily using RC drilling methods similar to those used in earlier programs.



RC samples were collected at the rig using cyclone and splitter systems at regular intervals. Intervals were defined from geological logging to capture mineralization associated with vein systems, hydrothermal breccias, and disseminated zones within the broader low-grade envelope. Sampling covered the main Sleeper deposit and peripheral targets, including structurally controlled zones and areas beneath post-mineral cover such as West Wood.

Paramount applied standardized procedures for sample collection, labeling, and tracking, using trained personnel to maintain sample integrity. Methods were consistent with earlier programs to maintain database continuity. Where coarse gold was suspected, a metallic screen fire assay was applied.

8.1.3 QP Comment

Sampling methods across all programs are appropriate for the mineralization style and intended data use. Documentation for early programs is limited; however, later programs by X-Cal, New Sleeper Gold, and Paramount demonstrate adherence to industry-standard practices.

In the opinion of the QP, the sampling approach is adequate to support the MRE, with uncertainties from historical practices addressed through data validation and Mineral Resource classification.

8.2 Sample Preparation and Analysis

8.2.1 Historical (1983–2010)

8.2.1.1 Sampling, Handling, and Chain of Custody

Sample preparation and analytical procedures for historical drilling at the Project were completed by AMAX, NGM, Placer Dome, X-Cal, and New Sleeper Gold. Documentation has improved since the late 1990s. Early programs (1983–1997) lacked detailed records of sample handling, chain of custody, and laboratory protocols. Although conducted by established operators and consistent with industry practice at the time, supporting documentation, including laboratory certificates and QA/QC records, was not available for independent verification.

Later programs, particularly X-Cal (1996–2007) and New Sleeper Gold (2004–2005), implemented more structured handling and chain-of-custody procedures. Samples were collected at drill sites and transported to commercial laboratories in accordance with documented protocols, thereby improving traceability and control.

8.2.1.2 Sample Preparation

Sample preparation during later historical programs was completed at commercial laboratories, primarily ALS Chemex (ALS Global or ALS), which is located in Elko, Nevada. Procedures followed standard workflows, including drying (if required), whole-sample crushing, subsampling, and pulverization to produce a pulp for analysis, ensuring homogeneity and minimizing bias.

Prepared pulps were retained by the laboratory or returned to the site for storage and potential verification.



8.2.1.3 Analytical Methods

Gold was analyzed primarily by fire assay, the industry-standard method. Routine samples used fire assay with atomic absorption finish. Samples with elevated gold or suspected coarse gold were analyzed by metallic screen fire assay to address nugget effects and improve accuracy.

Selected samples were analyzed for multiple elements using aqua regia or four-acid digestion followed by ICP techniques to support geological interpretation and mineralization characterization.

8.2.1.4 Laboratory Accreditation and Quality Systems

Analytical work during the historical programs was completed by independent commercial laboratories, primarily ALS Chemex (ALS Global) and, during the New Sleeper Gold programs, American Assay Laboratories (AAL), located in Sparks, Nevada.

ALS Global operates laboratories accredited to ISO/IEC 17025, requiring validated methods, calibrated instrumentation, and quality management systems to support analytical accuracy, precision, and reproducibility. Specific certification numbers for the Elko and Vancouver facilities were not provided; however, ALS laboratories are widely recognized as ISO-accredited.

AAL is accredited to ISO/IEC 17025:2017 by the International Accreditation Service (IAS) (Laboratory No. TL-536). The accreditation scope includes sample preparation, fire-assay for gold, and multi-element analysis by acid digestion and fusion. AAL maintains a formal quality management system and applicable regulatory approvals, including from the Nevada Division of Environmental Protection.

8.2.1.5 Sample Retention

Pulps generated during sample preparation were typically returned to the site for storage and potential re-analysis. The use of established laboratories and standard methods supports dataset reliability; however, incomplete documentation for early programs remains a limitation in data evaluation and Mineral Resource classification.

8.2.2 Paramount Gold (2010–2021)

Sample preparation and analytical procedures during the Paramount Gold and Silver Corp. drilling programs (2010–2021) followed documented protocols outlined in the 2023 Technical Report (RESPEC 2023) and reflect a controlled workflow from drill-site collection through laboratory analysis at accredited facilities.

8.2.2.1 Sampling, Handling, and Chain of Custody

Samples were transported by drill contractors from drill sites to the Paramount logging facility at the Sleeper site near Winnemucca, Nevada. Drill core was placed in core boxes, marked in feet, and transported daily for logging, where depths were converted to meters. Core boxes were photographed and placed on logging tables prior to logging.

Paramount geologists logged lithology, alteration, mineralization, and structural features, including fault intersections, lineations, fractures, veins, and bedding. Sample intervals were defined on geological boundaries to separate lithologies and mineralization styles, typically not exceeding 1.52 m (5 ft) and aligned with drilling runs where possible. Mineralized features were marked to ensure representative sampling.



Samples were assigned unique numeric identifiers. Tags were placed in core boxes and sample bags, with all numbers recorded in tag books. Sample numbering excluded drill hole, depth, and location to prevent bias.

Core was sampled at a dedicated station. The competent core was cut with a diamond saw; the broken core was split manually. One-half was bagged, and the remaining half was retained. Sampling technicians recorded sample numbers, intervals, and dates.

Sample bags were stored in a secure facility until shipment. Samples were organized sequentially, including QA/QC materials, inventoried, and placed in sealed rice bags with numbered seals. Each shipment contained samples from a single drill hole. Submittal forms documented shipment details, sample numbers, analyses, and duplicate requirements and were provided in hard copy and electronic format.

Reverse Circulation (RC) Drilling

Reverse circulation (RC) samples were collected at the drill rig using a cyclone system and placed in cloth bags within five-gallon buckets to capture coarse and fine fractions. Each sample was assigned a unique numeric identifier, with records linking the sample number to drill hole, depth, and interval.

Sample bags were tied, placed in crates, and stored at the drill site or in secured areas behind locked gates at the Sleeper site. Samples were handled to preserve integrity and prevent contamination or loss.

Before shipment, samples were arranged sequentially, including blanks, CRMs, and duplicates. Batches were verified and photographed as part of QA/QC.

Samples were transported to the laboratory by ALS personnel. Shipment dates and counts were recorded on handling forms, maintaining the chain of custody from drill site to laboratory receipt.

Sonic Drilling

Sonic drilling samples were collected from the drill pipe and placed in plastic bags labeled with the ending footage and orientation. Samples were transported to the Paramount facility and arranged sequentially on logging tables.

A geologist logged the samples and converted measurements to meters. Each 1 m interval was transferred into one or two sealed plastic bags (approximately 45.7 cm × 61 cm) for shipment.

Samples were placed in bins with nailed lids and transported to McClelland Laboratories, typically on the day of collection, minimizing degradation or contamination. At McClelland, samples were logged, split, and coarse crushed before transfer to ALS Chemex for final preparation and analysis.

Chain of Custody Controls

Across all drilling methods (RC, sonic, core), chain-of-custody procedures included:

- Unique numeric sample identifiers
- Recording of sample interval, drill hole, and depth in field logs and tag books
- Secure on-site storage with controlled access
- Sequential organization and verification of all samples, including QA/QC materials
- Sealed containers (rice bags or bins) with numbered security seals



- Detailed sample submittal forms documenting shipment and analytical requirements
- Direct transport to laboratories by authorized personnel (ALS or contractors)
- Documentation of sample movement using handling forms and photographs

These procedures maintained sample security, traceability, and representativity through collection, handling, and shipment. The QP considers these protocols consistent with industry best practice and sufficient to support the integrity of the analytical dataset for the Mineral Resource Estimate.

8.2.2.2 Sample Preparation

Sample preparation for Paramount drilling was completed at ALS Chemex (Elko), using standardized, ISO-accredited procedures. Samples were logged, assigned laboratory IDs, and prepared under ALS protocols.

Preparation included the following steps:

- Drying (if required)
- Primary crushing to approximately 75% passing 6 mm
- Mechanical splitting to approximately 250 g subsample
- Pulverization to approximately 85% passing 75 µm (200 mesh)

These steps reduce particle-size variability and improve sample representativity.

Contamination control included cleaner sand through the crushing circuit every five samples or with lithology changes, and between all pulverization stages.

For sonic drilling, samples were initially processed at McClelland Laboratories, where coarse crushing was completed before transfer to ALS. Samples were transported in sealed bins and delivered the same day.

Prepared pulps were shipped to ALS Vancouver for analysis.

8.2.2.3 Analytical Methods

Analytical methods for the Paramount Gold drilling programs (2010–2013) were selected to provide an accurate determination of gold and associated elements across a wide grade range and to address coarse gold effects. The program included multiple analytical methods, re-assay protocols, and verification procedures.

Gold was determined primarily by fire assay fusion. Both 30 g and 50 g aliquots were used, with 50 g charges improving the representativeness of nuggety mineralization. Routine samples used fire assay with atomic absorption (AA) finish (e.g., ALS Au-AA23).

For elevated gold values or AA over limits:

- Fire assay with gravimetric finish (ALS Au-GRA21) for >10 g/t Au
- 50 g fire assay charges to improve precision
- Metallic screen fire assay for coarse gold, separating coarse and fine fractions to mitigate nugget effects



Silver and multi-element analyses used four-acid digestion with inductively coupled plasma atomic emission spectroscopy (ICP-AES) (e.g., ALS ME-ICP61) on approximately 5 g aliquots, providing near-total digestion and analysis of approximately 32 elements.

For elevated silver values:

- >100 g/t Ag: four-acid digestion with atomic absorption finish (ALS AG-OG62)
- >1,500 g/t Ag: fire assay with gravimetric finish (ALS Ag-GRA21)

During parts of 2011–2012, silver was also analyzed by three-acid digestion with ICP and, in some cases, by 50 g fire assay with gravimetric finish. Gold was similarly analyzed using 30 g and 50 g charges with AA or gravimetric finish.

Independent check assays were completed by Inspectorate (Sparks, Nevada) using 30 g and 50 g fire assay for gold (AA or gravimetric finish) and atomic absorption or ICP methods for silver. This provided external verification of analytical results.

Laboratories applied QA/QC protocols, including blanks, CRMs, and duplicates. Samples were processed in numerical sequence to distribute QA/QC materials across batches. Results were monitored, and out-of-tolerance values triggered review and re-assay.

The combined use of fire assay, gravimetric and metallic screen methods, multi-element ICP analysis, and independent verification is consistent with industry best practice and supports the use of the data for Mineral Resource estimation

8.2.2.4 Laboratory Accreditation and Quality Systems

Analytical work was completed by ALS Chemex (ALS Global), accredited to ISO/IEC 17025:2005 for analytical testing, including gold assays, and ISO 9001:2008 for quality management. ISO/IEC 17025 requires validated methods, calibrated instrumentation, QA/QC protocols, external proficiency testing, and independent audits to support analytical accuracy, precision, reproducibility, and traceability.

Laboratory QA/QC included internal standards, blanks, duplicates, and defined re-assay protocols for out-of-limit results. These controls complemented Paramount's field QA/QC program and provided an integrated framework from sampling through analysis.

Inspectorate was used as an independent laboratory for check assays, providing external verification; however, certification details for the reporting period were unavailable.

8.2.2.5 Sample Retention

Following analysis, pulps and coarse rejects were retained by the laboratory or returned to the site for storage, allowing future verification and re-analysis.

The QP considers sample preparation, analytical methods, and laboratory quality systems, including use of ISO-accredited laboratories, consistent with industry best practice and sufficient to support the analytical dataset for the Mineral Resource Estimate.

8.3 Quality Assurance and Quality Control

Quality assurance (QA) demonstrates that assay data meet accepted precision and accuracy limits for the methods used, supporting confidence in the Mineral Resource estimate. Quality control (QC) comprises procedures to maintain data quality during sampling, preparation, and



analysis. QA/QC programs detect contamination and quantify accuracy, precision, repeatability, and overall sampling variability.

QA/QC procedures at the Project evolved over time, with limited documentation for early programs and more robust protocols in later programs (X-Cal, New Sleeper Gold, Paramount 2010–2013). The Paramount QA/QC program included certified reference materials (CRMs), blanks, duplicates, and secondary laboratory check assays to monitor accuracy, precision, contamination, and reproducibility.

QA/QC data for historical programs is incomplete and was not fully available for independent verification. The Paramount dataset includes a comprehensive QA/QC program with documented performance and validation.

8.3.1 Procedures

8.3.1.1 Historical

QA/QC procedures for early historical programs (AMAX, NGM, Placer Dome) are poorly documented, and records of standards, blanks, and duplicates were not available to SLR. Direct evaluation of analytical accuracy and precision is, therefore, limited.

Later programs (X-Cal and New Sleeper Gold) implemented formal QA/QC procedures, including:

- Insertion of certified reference materials
- Use of blanks for contamination control
- Collection of field and laboratory duplicates
- Submission of check assays to independent laboratories

Duplicate sampling was conducted at regular intervals (e.g., approximately 150 ft for RC drilling), with standards inserted at defined frequencies. Sample shipments were tracked, and results were monitored against expected values.

These procedures are consistent with industry practice; however, incomplete QA/QC datasets limit quantitative assessment of overall performance.

8.3.1.2 Paramount

The QA/QC program for the Paramount (2010–2013) drilling programs incorporated CRMs, blanks, and duplicates, together with internal laboratory QA/QC procedures and independent check assays to monitor accuracy, precision, and contamination.

QA/QC samples were inserted approximately once every 20 routine samples for each control type (CRMs, blanks, duplicates). Samples were submitted and processed in numerical sequence to ensure distribution across analytical batches. Protocols included CRM acceptance criteria, duplicate precision monitoring, and blank contamination review. Failures or out-of-tolerance results triggered batch review and re-assay where required.

The QA/QC dataset is summarized in Table 8-1, which presents counts of QA/QC samples by type relative to the total number of samples. QA/QC insertion rates are consistent and provide coverage for accuracy (CRMs), contamination (blanks), and precision (duplicates).

Based on SLR's review and noted limitations, the QA/QC program is consistent with industry best practice and supports confidence in the analytical dataset.



Table 8-1: Summary Counts of Sleeper QA/QC Analysis (X-Cal and Paramount)

Category	2003–2007 (X-Cal)		2011–2013 (Paramount)	
	Au	Ag	Au	Ag
Standard (CRM):				
Number in Use	N/A	N/A	12	6
Number of Analyses	N/A	N/A	387	16
Number of Failures	N/A	N/A	13	0
Duplicate				
Field Duplicate	822	875	200	199
Preparation Duplicate	642	309	0	0
Pulp Duplicate	1,610	2,451	0	42
Lab Preparation Duplicate	0	64	0	6
Lab Pulp Duplicate		162	11	0
Blank				
Pulp Blank	0	0	56	0
Coarse Blank	42	35	231	230
Lab Prep Blanks	0	0	8	10
Drill Hole Samples	51,325	44,980	10,134	10,137
Total Insertion Percent (%)	5.00	4.93	8.11	4.42

8.3.2 Certified Reference Material

8.3.2.1 Historical

CRMs) were used in later historical programs, including X-Cal (1996–2007) and New Sleeper Gold (2004–2005), to monitor analytical accuracy and laboratory performance.

RESPEC confirmed the use of CRMs in the 2003–2007 X-Cal program; however, supporting documentation was not available for review. CRMs were sourced from commercial providers and selected to represent relevant gold grade ranges, but records of insertion frequency, standard types, certified values, and performance metrics (bias, variance, pass/fail) were not provided to SLR.

Findings and Limitations:

- CRM use confirms the implementation of accuracy monitoring
- Insufficient documentation to assess performance against tolerance limits
- No statistical evaluation (control charts or bias analysis) available
- No systematic failures or analytical bias reported

CRM use is confirmed; however, the effectiveness of accuracy control cannot be quantitatively verified and remains a limitation in the QA/QC assessment.



8.3.2.2 Paramount Gold

Certified Reference Materials (CRMs) were used during the Paramount Gold (2010–2013) programs to monitor analytical accuracy and laboratory performance. CRMs from Mineral Exploration Geochemistry (MEG), RockLabs Ltd. (RockLabs), and CDN Resource Laboratories (CDN) were inserted at approximately one per 20 samples and selected to represent low-, medium-, and high-grade gold ranges. Some included listed silver values for multi-element verification. CRMs were distributed throughout the sample stream and processed in sequence with routine samples.

Performance was evaluated against certified values using ± 3 standard deviation (SD) acceptance limits. Most results met these criteria, indicating acceptable accuracy and no systematic bias. Performance was consistent across grade ranges, with variability within expected analytical limits.

Isolated CRM failures occurred but were not systematic or batch related. These triggered a review of associated batches and re-assay where warranted. Results indicate analytical accuracy was controlled and laboratory performance was stable for Mineral Resource estimation.

Paramount used four MEG CRMs (Reno, Nevada) and eight RockLabs CRMs (Perth, Western Australia). All 12 were certified for gold, some listed uncertified silver values. RESPEC data indicate CRM insertion rates of approximately 4% for gold and <1% for silver, reflecting limited silver-certified standards and selective silver analysis. Table 8-2 summarizes the CRMs used.

Table 8-2: Paramount Gold Certified Reference Material

Standard ID	Drill Years	Insertion Count	Certified Au (ppm)	Au SD (ppm)	Listed Ag (ppm)
MEG S107005X	2011-13	32	1.347	0.085	9.00
MEG S107006X	2011-13	34	2.850	0.364	8.00
MEG S107010X	2011-13	17	6.405	0.302	18.00
MEG-Au.09.02	2011-13	35	0.185	0.019	0.10
OxA89	2011-13	29	0.084	0.008	
OxC30	2011-13	18	0.200	0.005	
OxD87	2011-13	59	0.417	0.013	
Si25	2011-13	44	1.801	0.044	33.25
Si42	2011-13	40	1.761	0.054	
SJ63	2011-13	31	2.632	0.055	
SL61	2011-13	30	5.931	0.177	
SN16	2011-13	18	8.367	0.217	17.64

RESPEC identified three high and ten low failures in ALS gold analyses requiring review. Three of four MEG CRMs and five of eight RockLabs CRMs show slight negative bias. Three CRM pulps were also analyzed by Inspectorate (Reno, Nevada). Due to the limited Inspectorate dataset and equivalent detection limits, results from both laboratories were evaluated together. Results are summarized in Table 8-3, with failures detailed in Table 8-4.



Table 8-3: Summary of Sleeper Gold Results for CRMs 2010–2013

Standard ID	Grades in Au in ppm				Count	Date Used		Failure Counts		Bias Pct
	Target	Ave	Max	Min		First	Last	High	Low	
MEGS107005X	1.347	1.336	1.490	1.130	32	7/9/2011	8/26/2012	0	0	-0.8
MEG S107006X	2.850	3.001	3.350	2.150	34	7/13/2011	8/31/2012	0	0	5.3
MEG S107010X	6.405	5.899	6.450	5.080	17	7/9/2011	8/26/2012	0	2	-7.9
MEG-Au.09.02	0.185	0.172	0.198	0.124	35	7/9/2011	8/26/2012	0	1	-6.9
OxA89	0.084	0.080	0.089	0.073	29	9/20/2012	6/8/2013	0	0	-4.8
OxC30	0.200	0.366	3.250	0.181	18	7/9/2011	9/20/2012	1	2	83.2
OxD87	0.417	0.410	0.431	0.392	59	7/26/2012	6/8/2013	0	0	-1.8
Si25	1.801	1.796	1.915	1.395	44	7/9/2011	4/26/2013	0	1	-0.3
Si42	1.761	1.802	1.875	1.750	40	10/5/2012	6/8/2013	0	0	2.3
SJ63	2.632	2.653	2.790	2.540	31	9/20/2012	6/8/2013	0	0	0.8
SL61	5.931	5.808	6.270	4.800	30	7/26/2012	6/3/2013	0	1	-2.1
SN16	8.367	8.087	9.603	4.610	18	7/9/2011	1/30/2012	2	3	-3.4

Table 8-4: Gold Failure Details 2010–2013

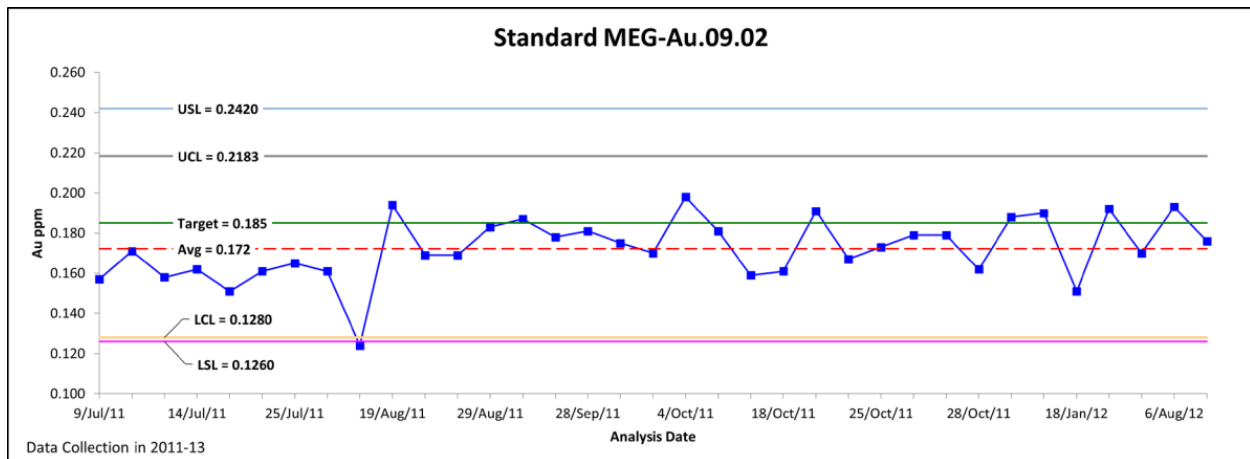
Standard ID	Hole ID	Values in Au ppm				Sample Number	Certificate
		Target for Std	Fail Type	Fail Limit	Failed Value		
MEGS107010X	PGC-11-007	6.405	Low	5.499	5.330	613065	RE11131983
MEGS107010X	PGC-11-014	6.405	Low	5.499	5.080	613897	WN11189542
MEG-Au.09.02	PGC-11-007	0.185	Low	0.128	0.124	613075	RE11131983
OxC30	PGC-12-021	0.200	High	0.215	3.250	616935	WN12209477
OxC30	NDRC-11-041	0.200	Low	0.185	0.181	612271	11-338-10754-01
OxC30	SDRC-11-051	0.200	Low	0.185	0.183	612548	11-338-10755-01
Si25	PGR-11-015	1.801	Low	1.700	1.395	609960	WN11114096
SL61	PGC-12-016	5.931	Low	5.400	4.800	614254	WN12152755
SN16	NDRC-11-041	8.367	High	9.018	9.603	612436	11-338-10754-01
SN16	NDRC-12-061	8.367	High	9.018	9.117	612745	12-338-00257-01
SN16	PGR-11-013	8.367	Low	7.716	5.330	609511A	WN11114451
SN16	PGR-11-014	8.367	Low	7.716	4.610	609762A	WN11112727
SN16	PGC-11-011	8.367	Low	7.716	7.620	613501	WN11164001



Two failures are from certificate RE11131983. Sample 616935 is likely mislabeled, as MEG S107006X was in use and falls within that range. Four failures lie near the failure limit and, given the observed negative bias, are likely to be due to bias rather than analytical error. CRMs were analyzed by ALS using atomic absorption fire-assay, not the gravimetric method used for certification.

Figure 8-1 shows the control chart for CRM MEG-Au.09.02, indicating one low-side failure. A consistent low bias is present; adjusted for this bias, the result would not be considered a failure.

Figure 8-1: Gold Control Chart for MEG-Au.09.02



Notes:

- USL Upper Specification Limit Target + 3 Std Dev (CRM)
- Target Expected Value (CRM)
- LSL Lower Specification Limit Target - 3 Std Dev (CRM)
- Items Calculated using Paramount Data
- UCL Upper Control Limit Avg + 3 Std Dev (Population)
- Avg Mean Value (Population)
- LCL Lower Control Limit Avg - 3 Std Dev (Population)

Only six CRMs had listed but uncertified silver values. ALS analyzed all silver samples using three-acid digestion with ICP finish (detection limit <0.5 ppm). Sixteen CRM silver analyses at Inspectorate used aqua regia digestion with atomic absorption finish.

Because listed values lacked standard deviations, LCL/UCL control limits for the sample population were used to evaluate performance. Table 8-5 shows no silver failures for the 2011–2013 program. Low-side bias in MEG S107006X, MEG S107010X, and SN16 is attributed to differences in analytical methods



Table 8-5: Summary of Sleeper Silver Results for CRMs 2010–2013

Standard ID	Grades in Ag in ppm				Count	Date Used		Failure Counts		Bias Pct
	Target	Ave	Max	Min		First	Last	High	Low	
MEGS107005X	9.0	8.9	9.6	8.4	3	1/18/2012	1/23/2012	0	0	-1.5
MEGS107006X	8.0	7.2	7.2	7.1	2	1/18/2012	1/18/2012	0	0	-10.6
MEGS107010X	18.0	9.8	9.8	9.8	1	1/30/2012	1/30/2012	0	0	-45.6
OxC30	0.1	0.1	0.1	0.1	2	1/18/2012	1/30/2012	0	0	0.0
Si25	33.3	31.7	34.3	28.4	3	1/23/2012	1/30/2012	0	0	-4.8
SN16	17.6	15.7	17.6	14.0	5	1/18/2012	1/30/2012	0	0	-10.9

8.3.3 Duplicates

8.3.3.1 Historical

Duplicate sampling during the historical programs was implemented primarily during the X-Cal (1996–2007) and New Sleeper Gold (2004–2005) periods, reflecting more structured QA/QC protocols. Duplicate types included field duplicates, mainly from RC drilling at regular intervals, and laboratory duplicates, including coarse reject and pulp duplicates. Sampling frequency was variable but typically followed defined intervals, such as approximately one duplicate per 150 ft or similar spacing within batches.

Duplicate sampling indicates that analytical precision was monitored during these programs. However, detailed datasets required for quantitative assessment, including duplicate-pair analysis, RPD calculations, and statistical precision measures, were not available to SLR. Formal evaluation of precision was therefore not possible.

Available documentation does not identify systematic precision issues or reproducibility concerns. Duplicate sampling practices are consistent with industry standards, and although supporting data are incomplete, there is no indication that precision materially affects the reliability of the historical dataset.

X-Cal Duplicates 2003–2007

RESPEC evaluated duplicate pairs using scatterplots (RMA regression), quantile–quantile plots, relative percent difference (RPD) plots, and absolute RPD plots. Two RPD methods were applied:

- $RPD (max) = 100 \times ((Duplicate - Original) / Lesser\ of\ (Duplicate, Original))$
- $RPD (mean) = 100 \times ((Duplicate - Original) / Mean\ of\ (Duplicate, Original))$

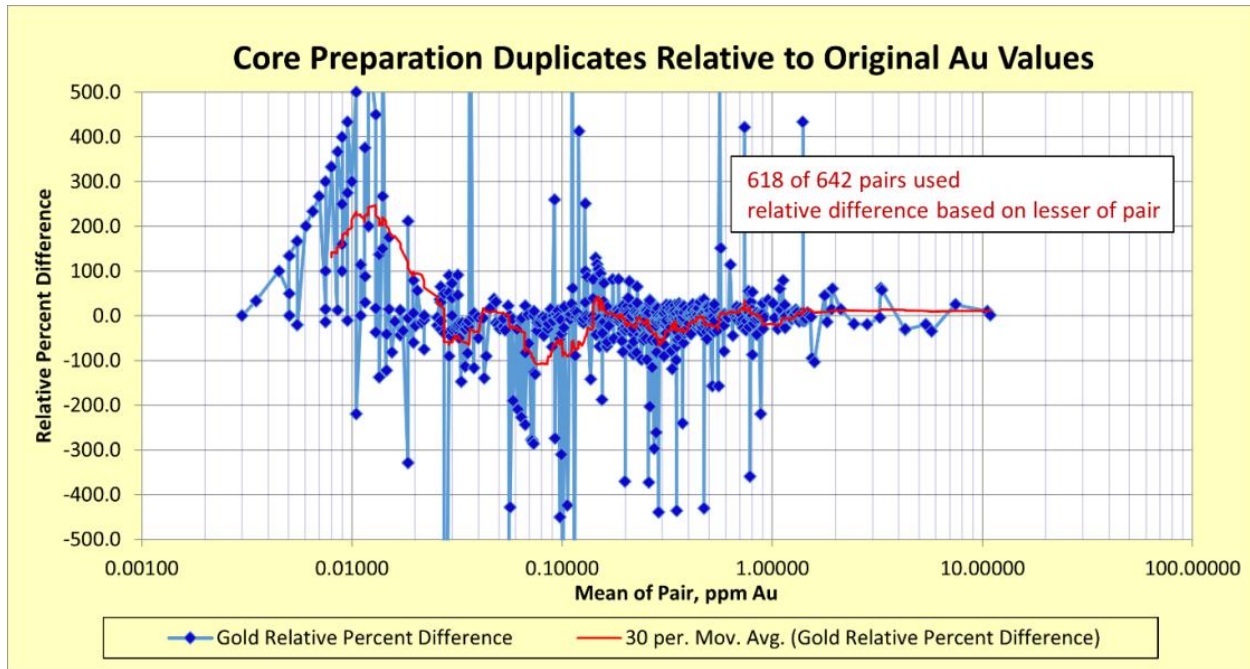
RPD (max) yields larger relative differences than RPD (mean).

Outliers were excluded from scatterplots by visual assessment, and pairs with absolute RPD >2,000% were removed from RPD plots. These outliers may remain relevant and should be considered in the overall evaluation; only pairs with incorrect sample identification are excluded. Causes of extreme variability require further review.



Preparation Duplicates: Giroux et al. (2009) reported core duplicates collected from coarse rejects returned by AAL. Selected samples were re-prepared and analyzed at ALS, representing preparation duplicates of core samples. These were not processed at the primary laboratory (AAL), which is preferred practice. Figure 8-2 presents the RPD plot for gold core preparation duplicates.

Figure 8-2: X-Cal Core Preparation Duplicates, Relative Differences 2003-2007



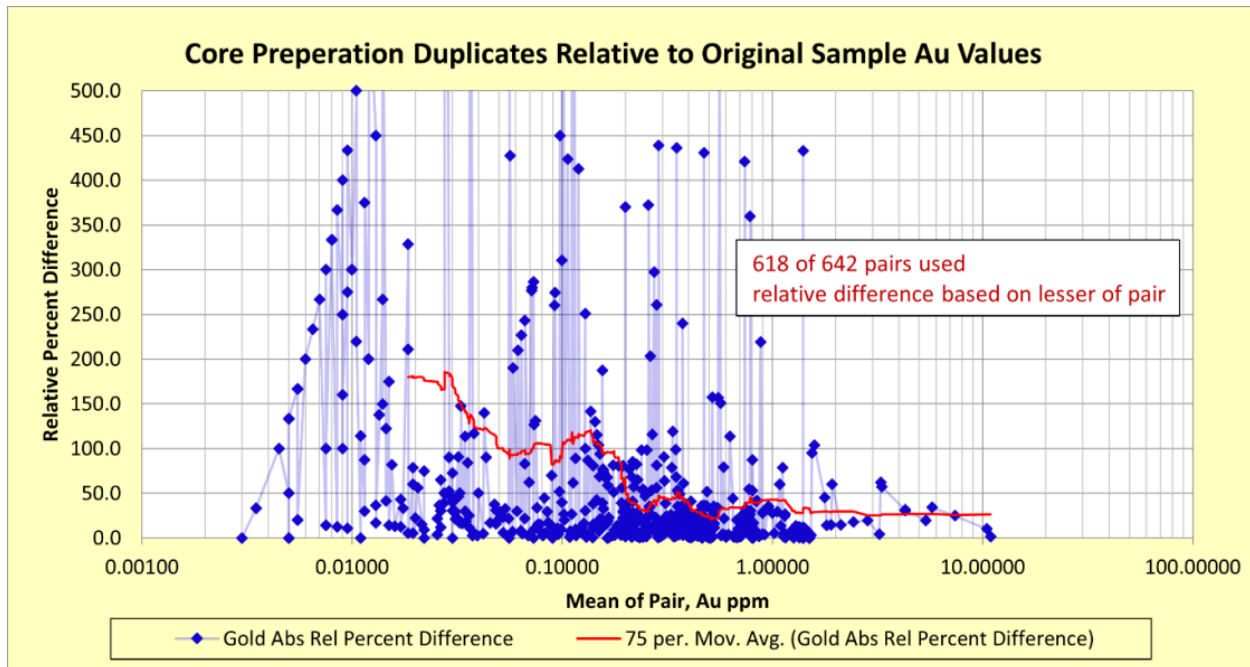
Source: RESPEC 2023

At grades >0.1 g/t Au, most duplicate pairs fall within RPD limits of $\pm 50\%$, with most within $\pm 25\%$. A small proportion of pairs exhibit higher RPDs, indicating greater variability between the original and duplicate assays. No bias is evident; however, high-variability pairs cause the moving-average line to deviate from 0% RPD. Data with a mean RPD near 0% indicates no bias.

Figure 8-3 presents absolute RPD values for each gold pair, illustrating the magnitude of variability. Figure 8-4 shows RPDs for X-Cal RC gold field duplicates.

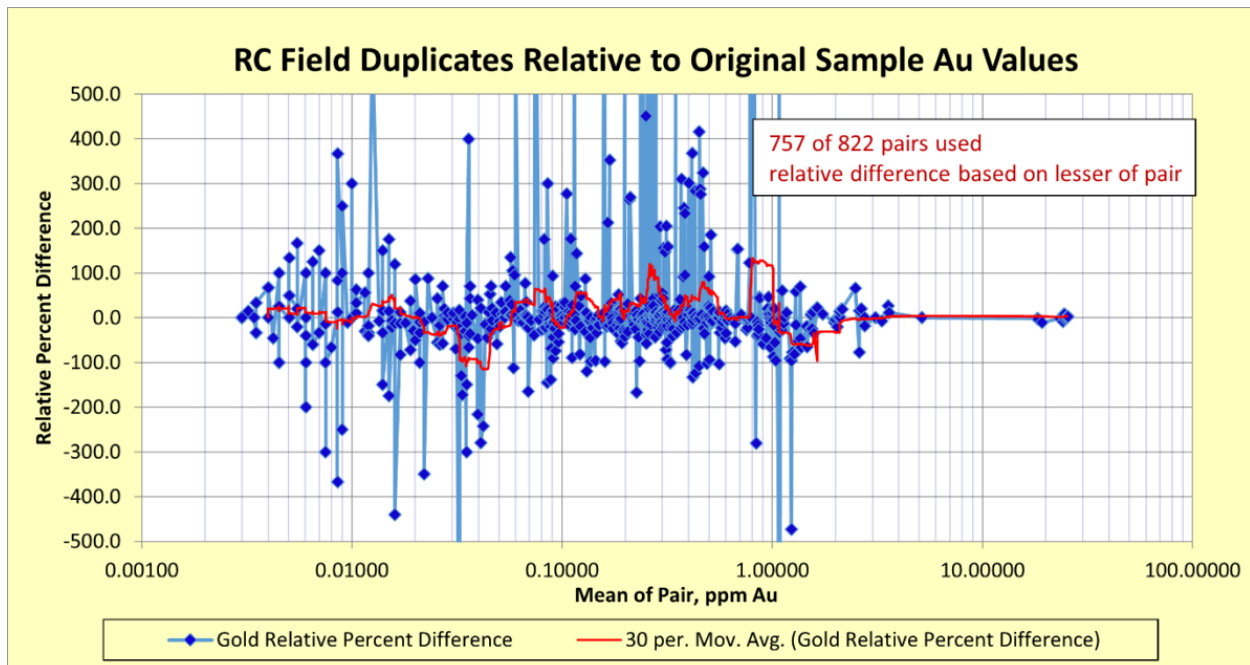


Figure 8-3: X-Cal Core Preparation Duplicates, Relative Differences 2003-2007



Source: RESPEC 2023

Figure 8-4: X-Cal Gold RC Field Duplicates, Relative Differences 2003-2007



Source: RESPEC 2023

The moving-average line is influenced by extreme outliers, limiting its utility. Statistical analysis indicates an apparent high bias in duplicate assays relative to original samples; however, this bias is eliminated when the 16% of pairs with absolute value (AV) RPD >100% are removed,



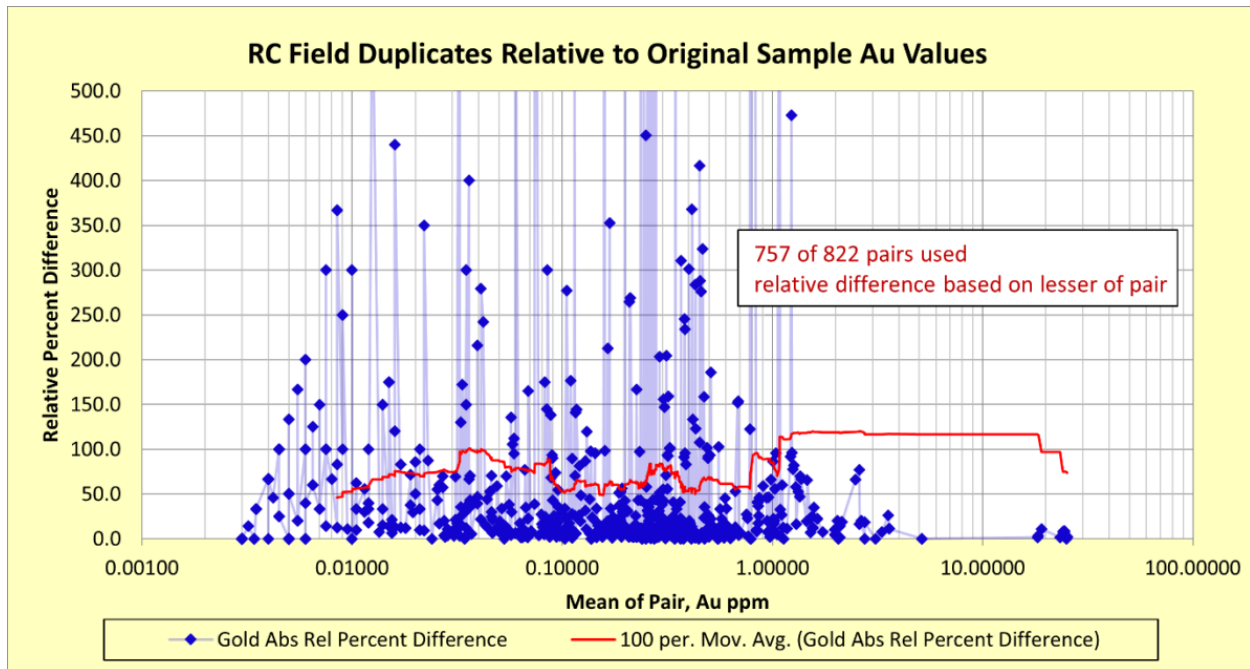
indicating it is entirely attributable to this subset of highly variable pairs. Silver RC field duplicates show similar behavior, consistent with gold and silver occurring in electrum.

The average AV RPD is 24% for pairs with AV < 100%, with most pairs < 50%, which is typical for field duplicates. The primary issue is the proportion of pairs with AV RPD >100% and the tendency for these pairs to show higher duplicate grades. Elevated variability at low grades is expected due to reduced analytical precision and amplification of percentage differences.

Excluding sample mix-ups or data errors, the most likely cause of AV RPD >100% is unrepresentative RC sample splitting at the drill rig. This may be limited to duplicate intervals if sampling protocols differed from routine intervals. Otherwise, routine RC splitting may have been non-representative in approximately 15% to 20% of cases.

Figure 8-5 presents absolute RPD values for RC duplicate pairs (RPD max). Pairs exceeding the AV RPD of 500% are truncated and shown as blue lines without apices.

Figure 8-5: X-Cal Gold RC Field Duplicates, Absolute Values of the Relative Differences 2003-2007



Source: RESPEC 2023



Field duplicates reflect inherent mineralization variability and variability from all subsampling stages: (i) coarse reject splitting; (ii) pulp preparation; (iii) assay aliquot selection; and (iv) analytical error. Variability introduced prior to duplicate splitting is captured in preparation duplicates.

At Sleeper, approximately half of the variability observed in RC field duplicates is present in core preparation duplicates. Although core duplicates were analyzed at a different laboratory, the absence of bias supports comparison of the datasets for variability assessment.

Core preparation duplicates show high variability at relevant gold grades, like RC field duplicates, but with fewer high-variability pairs and no associated bias. This supports potential RC splitting issues during the X-Cal 2003–2007 programs.

High-variability pairs should be reviewed to confirm validity and assess causes, including temporal or spatial clustering.

Elevated variability is also expected due to the nugget effect associated with gold and silver in electrum. This inherent variability introduces risk to resource estimation and should be considered when selecting an estimation methodology.

8.3.3.2 Paramount Gold

Duplicate sampling during the Paramount Gold (2010–2013) programs was systematic and included multiple precision controls: coarse reject and pulp duplicates at approximately 1 in 20 samples, and quarter-core duplicates, where one sample per batch was split and submitted under separate identifiers. Laboratories also performed internal duplicate analyses. Routine field core duplicates were not collected; however, laboratory duplicates and quarter-core splits provide an adequate framework to evaluate analytical precision. Table 8-6 summarizes field duplicate data for X-Cal and Paramount (2011–2013). No QA/QC data were available for the 2010 five-hole program (RESPEC 2023).

Duplicate results show good agreement across most grade ranges. Precision is consistent at low to moderate grades, with increased variability at higher grades reflecting coarse gold and nugget effects typical of the deposit. Elevated relative differences at higher grades occur but are not systematic. No systematic bias or material precision issues are identified. Overall, duplicate data indicate acceptable precision consistent with the mineralization style (Table 8-6) and support the reliability of the analytical dataset for the Mineral Resource Estimate.



Table 8-6: Summary of Results X-Cal Historical and Paramount Field Duplicates

Laboratory	Duplicate Type	Drill Type(s)	Element	Period	Counts			RMA Regression	Averages as Percent	
					All	Used	Outliers	$y = \text{Duplicate}$ $x = \text{Original}$	RPD	AV RPD
ALS Minerals Inspectorate ACME Labs	Field Dup	R/C	Au	2003-2007	822	757	65	$Y = 1.0047x + 0.0027$	3.56	31.12
ALS Minerals Inspectorate ACME Labs	Prep Dup	Core	Au	2003-2007	642	618	24	$Y = 1.0229x - 0.0238$	0.97	33.64
ALS Minerals Inspectorate ACME Labs	Field Dup	R/C Core	Au	2011-2013	200	192	8	$Y = 0.8866x + 0.0126$	8.02	31.38
ALS Minerals Inspectorate ACME Labs	Field Dup	R/C	Au	2011-2013	137	132	5	$Y = 1.5165x - 0.0439$	16.60	31.78
ALS Minerals Inspectorate ACME Labs	Field Dup	Core	Au	2011-2013	63	60	3	$Y = 1.037x - 0.0107$	-9.26	30.44
ALS Minerals Inspectorate ACME Labs	Field Dup	R/C Core	Ag	2003-2007	875	870	5	$Y = 0.992x + 0.126$	0.30	54.20
ALS Minerals Inspectorate ACME Labs	Field Dup	R/C Core	Ag	2011-2013	225	224	1	$Y = 1.063x + 0.241$	-27.20	66.50
Notes: AV absolute value RPD relative percent difference										



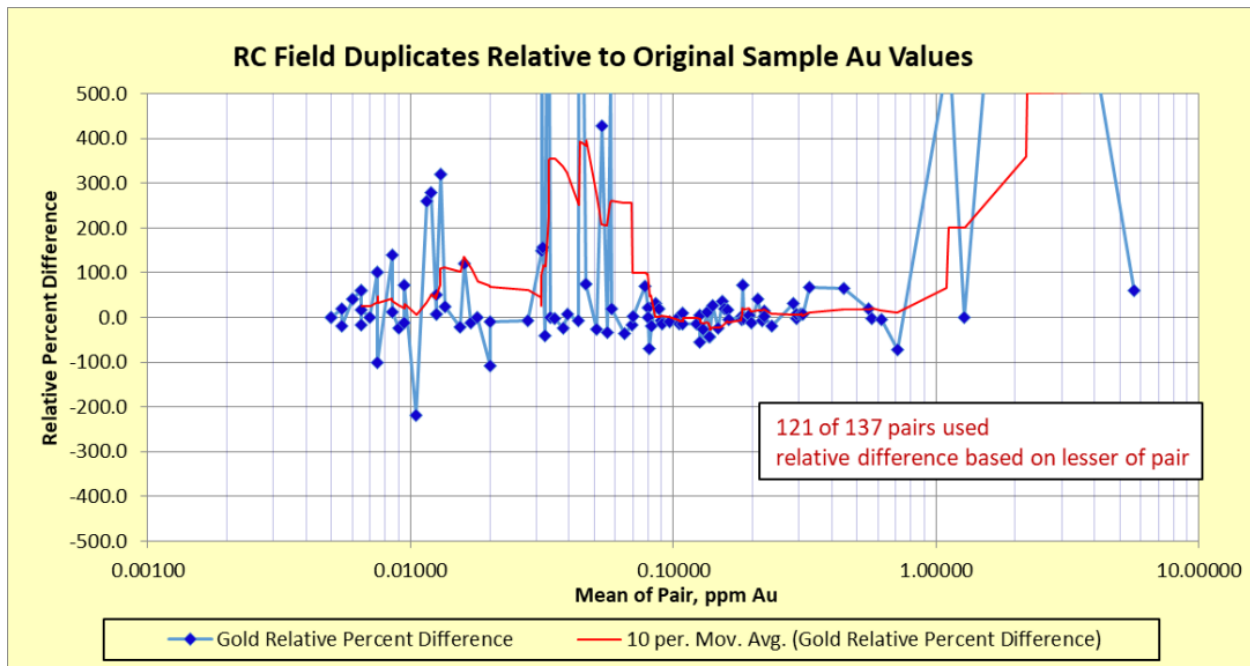
Pulp and Preparation Duplicates.

Paramount’s pulp and preparation duplicate data were in final compilation and analysis as of the 2023 Technical Report (RESPEC, 2023) and not available for review.

Field Duplicates:

A total of 137 RC field duplicates were compiled from the 2011–2013 program. Figure 8-6 presents an RPD plot for 121 pairs, excluding pairs where both values are below the detection limit.

Figure 8-6: Paramount RC Field Duplicates, Relative Differences 2010-2013



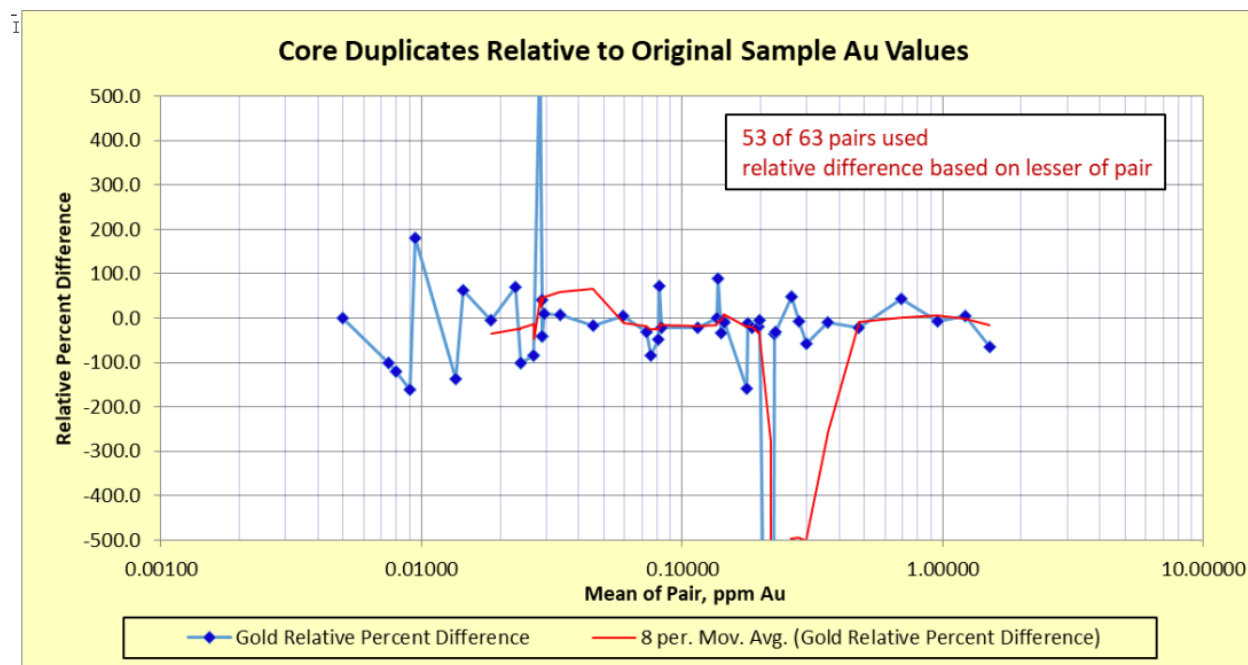
Source: RESPEC 2023

No bias is evident at grades greater than 0.1 g/t Au. Five of 51 pairs with mean grades >0.1 ppm have AV RPD greater than 100%, all within the highest-grade subset (1.1–2.2 ppm).

Fewer core field-duplicate pairs exceed detection limits (Figure 8-7). These data indicate a consistent low bias, with duplicate values lower than original assays; additional data are required to confirm. Three of 26 pairs with mean grades greater than 0.1 g/t Au have AV RPD greater than 100%.



Figure 8-7: Paramount Core Field Duplicates, Relative Differences 2010-2013



Source: RESPEC, 2023

8.3.4 Blanks

8.3.4.1 Historical

Blank samples were used during later historical programs, particularly X-Cal and New Sleeper Gold, to monitor contamination during sample preparation and analysis, confirming inclusion of contamination control in the QA/QC framework.

Blank materials were likely inert or low-grade; however, documentation of blank types, insertion frequency, and analytical results was not available to the SLR. Blank performance cannot be quantitatively assessed, and no statistical evaluation of contamination is available.

No systematic contamination issues are identified, and no sample integrity concerns are reported. However, the absence of detailed QA/QC records limits verification of blank effectiveness and remains a constraint on the QA/QC assessment of the historical dataset.

X-Cal Blanks 2003–2007

A total of 38 coarse blanks from the X-Cal drilling were analyzed for gold and, in 35 cases, for silver, with detection limits of 0.005 ppm and 0.2 ppm, respectively (Table 8-7). This represents a subset of the blanks analyzed, as many were not sufficiently described or not reported in the RESPEC dataset.

Four gold failures and one silver failure were identified using thresholds of five times the detection limit for gold and two times for silver, reflecting the higher silver detection limit (Table 8-8). Three of the four failures were preceded by higher-grade samples (Figure 8-8), indicating intermittent cross-contamination in the AAL crushing circuit between May 2004 and April 2005. The remaining failure may reflect a mislabeled sample.



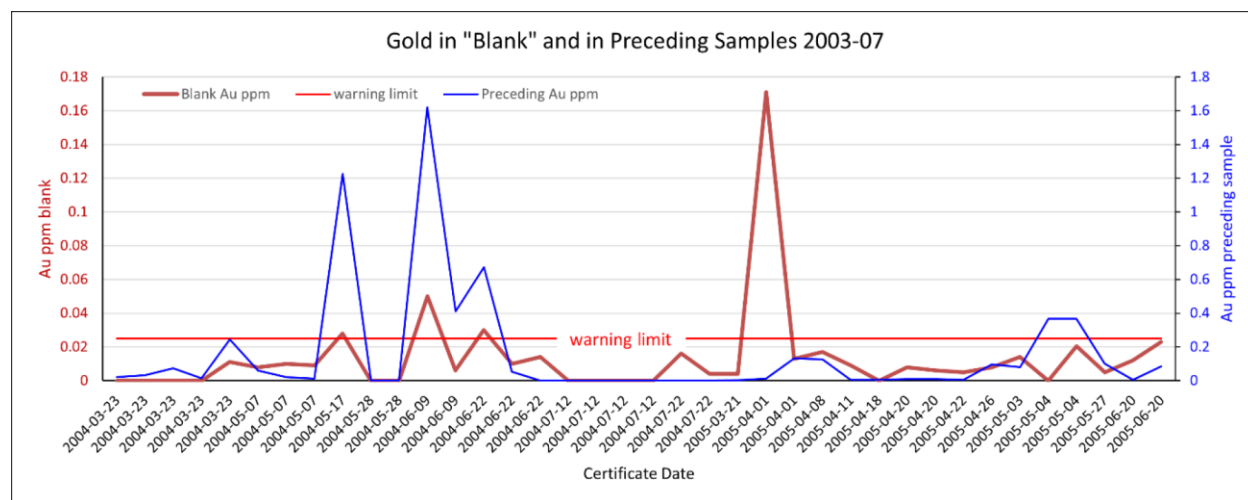
Table 8-7: X-Cal Blank Samples 2003–2007

Blank ID	Drill Program	Elem	Counts		Maximum (ppm)	Dates of Analyses	
			All	Above Warning		Start	End
Coarse Blank	2003-07	Au	38	4	0.171	23-Mar-04	20-Jun-05
Coarse Blank	2003-07	Ag	35	1	5.300	23-Mar-04	20-Jun-05

Table 8-8: X-Cal Blank Failures and Preceding Sample 2003–2007

Blank	Certificate	Elem	Method	Preceding		Blank		5x Det Limit (ppm)
				Sample	Value (ppm)	Sample	Value (ppm)	
Blank	SP065348	Au	ICP	27805	1.226	27806	0.028	0.025
Blank	SP065582	Au	F50/ICP	28127	1.620	28128	0.050	0.025
Blank	SP065732	Au	F50/ICP	28248	0.672	28249	0.030	0.025
Blank	SP068824	Au	F50/ICP	WW39-05 34018	0.011	WW39-05 34019	0.171	0.025
Blank	SP068894	Ag	AA	NS-01-05 30854	0.600	NS-01-05 30855	5.300	1.000

Figure 8-8: X-Cal Gold in Blanks and Preceding Samples 2003–2007



Source: RESPEC 2023

8.3.4.2 Paramount

Blank samples were systematically incorporated into the QA/QC program during the Paramount Gold (2010–2013) drilling programs at approximately one blank per 20 samples, consistent with industry best practice for contamination monitoring. Both coarse and pulp blanks were used, including commercially prepared blanks and inert materials. These included MEG laboratory blanks such as AuBlank40 (<0.002 ppm Au) and MEG-Blank.11.01 (<0.005 ppm Au), together with coarse blank material consisting of commercially crushed white marble with certified values below 0.005 ppm Au (Table 8-9)



Table 8-9: Blank Materials Used in Paramount QA/QC Program

Blank ID	Certified Value	Type	Origin
AuBlank40	<0.002 ppm	Coarse	MEG Labs
MEG-Blank 11.01	<0.005 ppm	Pulp	MEG Labs
Blank	<0.005 ppm	Coarse	Commercial crushed white marble

Blank samples were inserted into the sample stream and distributed throughout analytical batches to monitor contamination during sample preparation and analysis. The use of both coarse and pulp blanks allowed assessment of contamination during crushing, pulverizing, and analytical procedures.

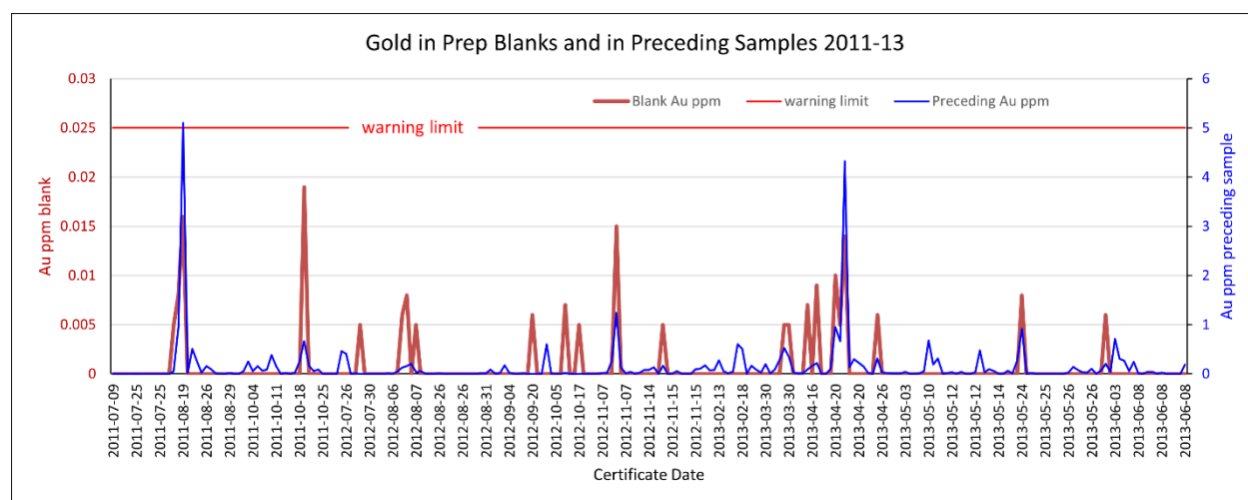
Analytical results show most blank values at or below detection limits, indicating minimal contamination. Performance was consistent across batches and laboratories, indicating controlled laboratory conditions.

Coarse blanks, including two from MEG and one prepared by Paramount using commercially crushed rock, and pulp blanks were inserted at a rate of approximately one per 30 samples (RESPEC). Values exceeding five times the detection limit were considered failures and reviewed.

A total of 231 coarse blanks were analyzed for gold and 230 for silver, with no failures. A total of 56 pulp blanks were analyzed for gold, with no failures. ALS internal blank data (eight gold, 10 silver) also showed no issues.

Figure 8-9 shows gold values for coarse blanks plotted with preceding sample values. Some elevated blank values, although not failures, correspond to high-grade preceding samples, indicating minor cross-contamination from the preceding sample.

Figure 8-9: Gold Values of Paramount Coarse Blanks and Preceding Samples



Source: RESPEC, 2023

Occasional elevated blank values were recorded but were isolated and not systematic. These results triggered a review of associated batches and adjacent samples to assess potential contamination. No persistent contamination trends or material impact on the analytical dataset were identified.



Blank results indicate that contamination during sampling, preparation, and analysis was effectively controlled. The absence of systematic blank failures supports the integrity of the analytical dataset and confirms that field and laboratory procedures were effective in limiting cross-contamination.

8.4 Sample Security

Sample security at the Project was maintained through field handling procedures, controlled storage, documented chain-of-custody protocols, and laboratory custody practices. The level of control and documentation improved over time, with the most comprehensive procedures implemented during the Paramount Gold (2010–2013) programs.

8.4.1 Historical (1983–2010)

Sample security procedures during the historical programs were generally consistent with industry practice, but documentation for early operators, including AMAX, NGM, and Placer Dome, was limited. Samples were collected by trained personnel and sent to commercial laboratories for preparation and analysis; however, detailed records of the chain of custody, storage conditions, and access controls were not available to SLR for independent verification.

During the later historical programs, particularly those completed by X-Cal and New Sleeper Gold, more formal sample security procedures were implemented. Samples were stored in secured areas, including fenced compounds or controlled-access facilities, before shipment. Shipments to laboratories were documented, and the laboratories maintained custody during preparation and analysis.

These procedures are consistent with accepted industry practice. However, the lack of detailed supporting documentation limits SLR's ability to fully evaluate the effectiveness of sample security for the historical datasets. There is no indication in the available information of sample tampering, loss, or material compromise of sample integrity.

8.4.2 Paramount (2010–2013)

Sample security during the Paramount drilling programs included controls from drill site collection through laboratory analysis. Drill contractors transported samples from the drill sites to the Paramount logging and sampling facility at the Sleeper site near Winnemucca, Nevada, where they were logged, processed, and stored in a secure, controlled-access facility.

Drill core was stored in core boxes within the secured facility. Reverse circulation and sonic samples were stored in designated secure areas before shipment. Trained personnel handled samples, and access to storage areas was controlled to prevent unauthorized handling.

Before shipment, samples were organized, inventoried, and packaged in sealed containers, including rice bags or bins secured with numbered security seals. Each shipment contained samples from a single drill hole and included sample submittal documentation listing sample numbers, requested analyses, and QA/QC instructions. Sample batches were verified and photographed before shipment to confirm completeness and integrity.

ALS personnel or authorized contractors transported samples to the laboratory. All transfers were documented on sample handling forms, maintaining a continuous chain of custody from the project site to the laboratory. On receipt, the laboratories logged the samples into internal tracking systems and maintained custody through preparation and analysis.



After analysis, pulps and coarse rejects were retained by the laboratory or returned to the project site for secure storage, allowing future verification and re-analysis.

These sample security procedures are consistent with industry's best practice and support confidence in the integrity, traceability, and security of the analytical dataset used to support the Mineral Resource Estimate.

8.5 QP Opinion

In the QP's opinion the sample preparation, security and analytical procedures are suitable to support the disclosure of the MRE in this TRS.

Sampling (1983–2013) is appropriate for the mineralization style. RC drilling (approximately 95%) using cyclone and splitter systems, with limited diamond drilling, supports both bulk-tonnage and structurally controlled mineralization. Later programs (X-Cal, New Sleeper Gold, Paramount) show improved controls. Early programs lack documentation but show no material deficiencies; uncertainties are addressed through classification.

Sample preparation and analytical methods are consistent with industry standards. Accredited laboratories (ALS, AAL), standard preparation, fire assay, and the use of metallic screen and gravimetric methods, where required, are appropriate. Multi-element ICP and check assays support data validity.

QA/QC is robust in the Paramount (2010–2013) dataset, including CRMs, blanks, duplicates, check assays, and re-assay protocols. CRM results show acceptable accuracy with minor, non-systematic bias. Blanks show no systematic contamination. Duplicates show acceptable precision, with higher variability at elevated grades consistent with nugget effects.

Historical QA/QC data are incomplete, limiting quantitative assessment. No systematic bias, contamination, or precision issues are identified. Elevated variability in X-Cal RC duplicates, including RPD outliers and potential splitting issues, has been taken into account in classification.

Sample security is adequate. Paramount programs demonstrate a controlled chain of custody, secure storage, documented tracking, and sealed shipments. Historical documentation is limited; no evidence of tampering or loss is identified.

Key limitations are listed:

- Incomplete QA/QC and custody records for early programs (1983–1997)
- Limited analytical certificates for verification
- Elevated variability in X-Cal RC duplicates from splitting and nugget effects

These are addressed through validation, reliance on later datasets, and classification.

The dataset is sufficiently accurate and reliable to support the MRE and meets the requirements of S-K 1300 and CIM (2019), with uncertainties reflected in the Mineral Resource classification.



9.0 Data Verification

Data verification comprises a systematic process to confirm that exploration and analytical data were collected using appropriate procedures, accurately transcribed into the Project database, and are suitable for use in the preparation of this Technical Report.

All available data relevant to the Project were compiled, digitized, and incorporated into a database by personnel from Paramount Gold. The QP audited the database for completeness, accuracy, and reliability.

The QP is of the opinion that database verification procedures for the Sleeper project comply with industry standards and are adequate for the purposes of Mineral Resource estimation.

Project data was provided to the QP in the form of Microsoft Excel spreadsheets and subsequently imported into Leapfrog Geo and Maptek Vulcan software for independent modeling and resource interpolation.

Verification procedures included checks for:

- Unique, missing, or overlapping intervals
- Total depth consistency
- Duplicate hole identification
- Boundary compliance

Database certification was conducted by the QP through a combination of visual inspections and statistical checks, including cross-referencing lithology, assay values, and spatial data against original hard copy records. Identified inconsistencies were either corrected using primary source documents or excluded from the Mineral Resource estimation

9.1 RESPEC Data Validation

A SLR review shows that RESPEC undertook a comprehensive data verification program to confirm that the Sleeper project database is reliable and suitable for Mineral Resource estimation.

This work included multiple site visits between 2021 and 2023, during which RESPEC personnel inspected drill core and RC cuttings, reviewed logging, sampling, and data management procedures, assessed sample storage conditions, and collected GPS collar locations for comparison with the database. RESPEC also examined original drill logs, assay certificates, and supporting records, and reviewed geological interpretations used in modeling.

The drill hole database was subjected to detailed validation testing to identify data integrity issues such as missing or duplicated collar information, inconsistent survey data, invalid assay intervals, and gaps or overlaps in geological and analytical records. Where discrepancies were identified, they were evaluated, corrected where appropriate, and documented using the original data sources provided by Paramount. Collar locations were verified against historical drill logs and electronic records, including validation of coordinate system conversions from local mine grid to UTM. Downhole survey data were reviewed against available records and found to be generally consistent, although many historical holes lack survey data, limiting full verification. Assay data verification included comparison of the database against original laboratory certificates, with a complete digital audit of available electronic records and partial manual verification of scanned certificates.



Additional confidence in the dataset was obtained through review of QA/QC programs and results, including resampling programs completed by Paramount to validate historical assays.

9.2 SLR Data Verification

The QP conducted a site visit on April 2, 2026. During the visit, the QP reviewed the historical mine site, waste rock dump areas, exploration facilities, and infrastructure relevant to the evaluation of the Project. Historical drill sites were examined, selected drill collar locations were confirmed with GPS, and detailed discussions were held with Paramount technical staff regarding exploration plans, drilling methods, analytical procedures, and geological controls on mineralization. The Paramount technical team demonstrated a strong understanding of deposit geology and assay interpretation.

9.2.1 Limitations

No material restrictions were encountered during the QP's independent verification of the Sleeper drill hole database; however, the following limitations were identified:

- **Bulk Density:** A comprehensive bulk density sampling program has not been completed for all geological units used in the Mineral Resource model. Additional bulk density data are required to improve confidence in tonnage estimates.
- **QA/QC Records:** Documentation supporting the use of certified reference materials, blanks, and duplicates for historical channel sampling is unavailable. A formal QA/QC program is recommended for future drilling and sampling campaigns.
- **Alteration Logging:** A review of the oxidation model indicates that oxide and sulfide classifications were interchanged across a portion of the historical drill hole database. Comparisons with historical mining records from AMAX are inconsistent with the logged oxidation data, further evidence of this issue. Resolution of these discrepancies and validation of oxidation state logging are recommended to improve confidence in the geological and metallurgical interpretations.
- **Downhole Surveying:** Most historical drill holes lack deviation surveys and are assumed to be vertical. This assumption introduces uncertainty in the interpretation of true mineralization geometry and thickness.

9.3 QP Opinion

Although some historical information (including portions of QA/QC documentation, downhole surveys, and legacy records) could not be independently verified, the drill hole database compiled by Paramount and validated by RESPEC aligns with S-K 1300 industry practices. The SLR QP is of the opinion that the database is reliable, internally consistent, and suitable for use in the Mineral Resource Estimate.

The Project's extensive production history and prior operational use of these data support their adequacy. Historical grade control and metallurgical studies corroborate reported gold grades, although recent independent assay verification is lacking for certain legacy datasets.

Data with incomplete collars or insufficient documentation were excluded where necessary and are not considered material to the estimate. Sampling methods from historical and recent programs are consistent with industry standards. While additional QA/QC documentation and targeted resampling are recommended to further improve confidence, the database is considered appropriate for Mineral Resource estimation.



10.0 Mineral Processing and Metallurgical Testing

10.1 Introduction

The metallurgical information reviewed for the Project includes historical operating performance, bottle roll and column leach testing, flotation investigations, and later oxidation studies.

For this Initial Assessment, the proposed processing method is heap leach treatment of selected oxide, mixed, and waste rock dump material with Merrill-Crowe recovery. Processing of sulfide, historical heap leach pad (HLP), and historical tailings materials is considered separately through on-site flotation, with rougher concentrate assumed to be sold or toll treated off site. Sulfide processing test work remains preliminary and requires additional variability test work, concentrate quality, and commercial review.

10.2 Nature and Extent of Metallurgical Testing and Analytical Procedures

SLR reviewed historical oxide milling and heap leaching records; bottle roll and column leach testing on oxide, mixed and waste rock dump composites; flotation investigations on selected historic HLP, tailings, waste, and sulfide-related materials; and later bio-oxidation and pressure-oxidation studies. For the current study, the McClelland bottle roll and column leach programs provide the principal support for the coarse-crush agglomerated heap leach flowsheet, while flotation test work supports preliminary consideration of a separate flotation route for sulfide, historic HLP, and tailings materials.

Table 10-1 lists the principal metallurgical reports reviewed for the project. Later technical reports were used as summary references, while the McClelland, Hazen, SGS, MRDI, KCA, and other historical studies provided the primary metallurgical support for interpretation of processing options and recovery assumptions.

Table 10-1: Metallurgical Reports Reviewed

Report / Document	Date	Laboratory / Organization	Comment
Sampling and Metallurgical Evaluation of Existing Leach Heaps and Mill Tailings	1997	Mineral Resources Development Inc. (MRDI)	Existing heap and tailings metallurgical study.
Sleeper Project Sampling and Metallurgical Test Program	1999	Kappes, Cassidy & Associates (KCA)	Internal report for X-Cal Resources Ltd.
Sleeper Mine Tailings and Heap Evaluation as Potential Gold Resources	2007	Edouard K. Zoutomou / X-Cal Resources Ltd.	Existing tailings and heap evaluation study.
Phase 2 Metallurgical Evaluation – Waste Rock Dump, Westwood and Facilities Composites	2012	McClelland Laboratories Inc. (including ALS and Inspectorate results)	Existing waste rock dump, West Wood, and Facilities cyanidation test work.
Pressure Oxidation Pretreatment and Cyanide	2013	Hazen Research, Inc.	POX subcontract work reported within the 2015 McClelland study.



Report / Document	Date	Laboratory / Organization	Comment
Leaching of Sleeper Mine Samples			
Metallurgical Tests and Analyses on 12 Sleeper Project Core Composites	2014	McClelland Laboratories Inc.	Bottle roll, column leach, and related cyanidation test work on core composites.
Biooxidation and Pressure Oxidation Testing – Sleeper Drill Core Composites	2015	McClelland Laboratories Inc.	Sulfide-focused metallurgical test work including biooxidation and cyanidation.
Mineralogical study appendix to 2015 McClelland report	2015	SGS Canada Inc.	Supporting mineralogical/deportment study.
Technical Report and Preliminary Economic Assessment – Sleeper Project (Amended)	2017	Metal Mining Consultants Inc.	Technical Report summarizing prior metallurgical work; not a laboratory report.
2022 Sleeper S-K 1300 Technical Report Summary	2022	RESPEC / Woods Process Services LLC	TRS compiling historical metallurgical work; not a laboratory report.

The analytical procedures described in the reviewed reports are conventional for scoping-level evaluation of gold-silver heap leach and flotation performance and include head assays, bottle roll tests, column leach tests, flotation tests, and reagent-consumption measurements. These procedures are standard industry practice for preliminary assessment of cyanide amenability, leach kinetics, reagent demand, and flotation response. No non-conventional analytical procedure has been identified as the basis for either the heap leach case or the preliminary flotation case. Certain recovery values remain provisional where direct representative test work is limited.

10.3 Sample Representativeness

The metallurgical dataset includes several distinct oxide and mixed material groups evaluated as potential heap leach feed, including Facilities Oxide, West Wood Oxide, and Sleeper Oxide, together with Facilities Mixed, Sleeper Mixed, and West Wood Mixed material. These groups represent separate source areas within the Project and are treated individually because the available test work support, cyanide amenability, recovery response, and reagent demand differ by material type. The available metallurgical testing and analysis are adequate for preliminary evaluation of selected oxide, mixed, and waste rock dump material as early heap leach feed. Facilities Oxide is the best-supported heap leach feed type in the database, and selected West Wood Oxide and waste rock dump composites also support a phased heap leach processing scenario. Available flotation work is sufficient to justify preliminary consideration of a separate flotation-concentrate route for sulfide, HLP, and tailings materials, but not yet for definitive design or pre-feasibility-level recovery prediction.

Sample representativeness is weaker for the sulfide, HLP, and tailings materials now grouped in the separate flotation case. The current data does not support inclusion of these materials in the same heap leach recovery framework used for oxide, mixed, and waste materials. Historic HLP, tailings, and sulfides require additional metallurgical testing, analysis, and economic evaluation before they can be assigned definitive recoveries, concentrate terms, and operating cost.



10.4 Testing Laboratories

The test work reports identify McClelland Laboratories in Sparks, Nevada as the principal metallurgical laboratory for the bottle roll, column leach, flotation, and related process test work programs used in the oxide, mixed, waste rock dump, and sulfide evaluations. Supporting specialized work was also completed by Hazen Research and SGS Canada, and project QA/QC documentation (Metal Mining Consultants Inc. 2017) references ALS and Inspectorate for analytical and check-assay work. Based on the files reviewed, the SLR QP understands these laboratories to have been independent of the project owner.

Table 10-2 summarizes the accreditation details, which are shown only where identified during review. “No public certification record identified” indicates that no specific accreditation record was located during the present review. All listed organizations are considered independent of the mine owner based on the available information.

Table 10-2: Laboratory Accreditation Summary

Laboratory / Organization	Location	Certification/ accreditation	Affiliation with mine/ owner
McClelland Laboratories, Inc. (MLI)	Sparks, Nevada	2012–2015 accreditation: <i>IAS-accredited to ANSI/ISO/IEC 17025:2005; accreditation in place since November 12, 2012.</i>	Independent Laboratory
Hazen Research, Inc.	Golden, Colorado	No public certification record identified	Independent Laboratory
SGS Canada Inc. / SGS Minerals Services	Ontario, Canada	Accredited to ISO/IEC 17025	Independent Laboratory
Kappes, Cassidy & Associates (KCA)	Reno, Nevada	No public certification record identified	Independent Technical Consultant

10.5 Relevant Metallurgical Results

Historical operating records show that Sleeper successfully processed oxide material by both milling and heap leaching, supporting oxide material as the clearest near-term development path. The prior assessments and mine history, therefore, provide a precedent for a large-scale oxide heap leach concept supplied by open-pit mining and, where justified, rehandling of selected existing waste rock dump material.

10.5.1 Oxides

Facilities oxide is the strongest candidate for initial processing utilizing heap leach and Merrill-Crowe processing. The column and bottle roll results show favorable gold recovery and cyanide amenability, a coarse crush size of P80 19 mm, with column gold recoveries averaging 83.9% and bottle roll recovery of about 81% Au. West Wood oxide also showed a positive heap leach response with an average column gold recovery of 76.5%, although with greater variability and higher reagent demand. Sleeper oxide bottle roll gold performance was favorable at 93.9%, but the database does not provide the same level of direct column confirmation as Facilities oxide.



10.5.2 Waste Rock Dumps

Selected waste rock dump material also shows potential for a heap leach case. Historical testing concluded that the dump composites evaluated were amenable to agglomerated heap leach cyanidation at coarse crush size, with column gold recoveries ranging from the mid-60% range to the low-80% range, depending on dump area and composite. Reagent consumption was variable and, in some cases, high. Waste material is therefore technically amenable to heap leaching, but economic performance is sensitive to recovery, crush-size, and reagent assumptions.

10.5.3 HLP, Tailings, and Sulfide Flotation

Historical metallurgical data indicate that HLP, tailings, and sulfide materials are more amenable to flotation recovery than through direct heap leaching. The available database is limited and variable in scope, but it provides a reasonable preliminary basis for evaluation of a flotation process at the IA level. Historical tailings work reported cleaner flotation-related recoveries of 63% Au and 33% Ag at P₇₅ 200 mesh (75 µm) in the 1997 program and approximately 50.8% Au and 64.8% Ag, at P₈₅ 400 mesh (37 µm), in the 1999 program, demonstrating that precious metals can be recovered from these materials, although performance was variable and the work did not establish a final commercial flowsheet.

Sulfide rougher and cleaner flotation test work was completed at P₈₀ 200 mesh (75 µm) by McClelland in 2012. The rougher flotation results showed generally favorable recovery performance and are therefore included for the flotation results. For Facilities sulfide material, rougher flotation testing returned gold recoveries of 70.7% and 91.2%, with reported silver recoveries of 43.6% and less than 48.8%. For West Wood argillic-silicic sulfide material, rougher flotation gold recoveries ranged from 57.7% to 79.7%, averaging 70.8%, with an average silver recovery of about 57.0%. For West Wood strong silicic sulfide material, rougher flotation gold recoveries ranged from 65.0% to 84.9%, averaging 75.1%, with an average silver recovery of 67.1%. McClelland noted that these flotation results were scoping-level in nature and that additional optimization and locked-cycle testing would be required.

Existing heap leach pad material has not been supported by a sufficiently robust and dedicated flotation testing program and was historically evaluated primarily for in-place or re-leach potential rather than as flotation feed. At this time, HLP material is considered with the existing tailings for a flotation-processing case based on the closest available historical flotation analogs. The QP considers this approach acceptable for initial assessment only. Additional variability testing, concentrate characterization, and economic viability are required before HLP, tailings, and sulfide materials can be assigned recoveries and operating costs for a flotation flowsheet.

The principal processing factors identified in the test work are sulfide content, refractory gold locking, variable leach kinetics, and elevated reagent demand in certain materials. Sulfide-rich, HLP, and tailings materials are not included in the heap leach case and are instead considered through flotation, followed by sale or toll treatment of rougher concentrate. For IA purposes, a 12% discount to flotation recoveries is applied to reflect toll milling fees and related downstream charges.

10.5.4 Deleterious Elements

Review of the available multi-element dataset for the oxide, mixed, and waste rock dump materials indicates that mercury, arsenic, antimony and sulfur are the primary deleterious constituents requiring additional evaluation for the Sleeper Project. The West Wood Oxide samples show elevated mean mercury and antimony concentrations, while the Facilities Mixed



and North Dump materials show elevated arsenic and antimony. The North Dump also reports elevated total sulfur concentrations.

The identified deleterious elements are not currently considered to be prohibitive to heap leach development, however, the elevated mercury, arsenic, antimony, and total sulfur in selected material groups warrant additional metallurgical and precipitate-quality test work prior to pre-feasibility level design.

Initial refinery capital cost allowances include a mercury retort to address the elevated mercury concentrations identified in selected material groups. This allowance is intended to provide an IA level provision for mercury management during doré production and refinery handling. Additional test work, precipitate characterization, and doré/refinery assessments are recommended in future study phases to confirm the required mercury-control measures and refine the associated capital and operating cost assumptions.

10.6 Recovery Assumptions and Basis for Estimation

Recovery assumptions used for the preliminary economic evaluation were derived from available test work and adjusted to reflect confidence levels across the resource. For heap leach materials, column leach results were given greater weight than bottle roll results because they are more representative of coarse-crush heap leach conditions and kinetics. When only bottle-roll data were available, conservative adjustments were applied. Sulfide, HLP, and tailings materials are considered separately on the basis of flotation performance, with payable recoveries reduced by 12% to reflect toll milling fees and related concentrate handling charges.

10.6.1 Sleeper Oxide

The recovery value assigned to Sleeper oxide was based on reported bottle roll test results; however, because no directly comparable representative column leach result is presently available for that material, the reported bottle roll recoveries of 93.9% Au and 11% Ag were discounted by 10% for use in the recovery model. This adjustment is intended to provide a conservative approximation of expected heap leach performance and to recognize the generally more optimistic nature of bottle roll extraction results relative to column leach performance under field-relevant conditions.

10.6.2 Sleeper Mixed and West Wood Mixed

Recovery values assigned to Sleeper mixed and West Wood mixed material are estimated assumptions rather than direct outputs from a complete set of representative column leach tests. These values were developed from metallurgical interpretation of the available data, including oxidation state, relative cyanide amenability, bottle roll, and limited column response, and comparison with analogous oxide and mixed composites. These recoveries are suitable only for initial assessment and should be confirmed by additional representative column leach testing.

10.6.3 HLP, Tailings, and Sulfides

For the IA, flotation recoveries assigned to HLP, tailings, and sulfide materials were derived from the available historical test work and reduced by 12% to reflect the assumed toll-milling and downstream concentrate treatment charges associated with off-site processing of rougher concentrate. These values are preliminary planning assumptions only and should not be interpreted as demonstrated commercial recoveries.



10.6.3.1 HLP and Tailings – Gold

The recovery assumptions for HLP and tailings were based on the average of the historical tailings flotation results from the 1997 and 1999 test programs. Using reported recoveries of 63% Au from the 1997 program and approximately 50.8% Au from the 1999 program results in average unadjusted recoveries of 56.9.0% Au. After application of the 12% discount, the assumed recoveries for both HLP and tailings are 50.0% Au. This assumption is necessarily approximate because direct flotation test work on HLP material is limited, and the historical HLP studies were not designed to support a modern flotation circuit.

10.6.3.2 Facilities Sulfide

The Facilities sulfide recovery assumption was based on the average of the two available McClelland rougher flotation tests. The average unadjusted gold recovery was 80.95%, which results in an applied recovery of 71.2% Au after the 12% discount.

10.6.4 West Wood Strong Silicic and West Wood Argillic

The West Wood strong silicic recovery assumption was based on the average West Wood strong silicic rougher flotation results reported by McClelland. Average unadjusted recoveries were 75.1% Au, resulting in applied recoveries of 66.1% Au after the 12% discount. The West Wood argillic-silicic recovery assumption was based on the average West Wood argillic-silicic rougher flotation results. Average unadjusted recoveries were 70.8% Au, resulting in applied recoveries of 62.3% Au after discount.

These recovery assumptions provide a consistent preliminary basis for evaluating flotation treatment of HLP, tailings, and sulfide materials in the IA. However, the underlying test work remains limited, variably representative, and unsupported by pilot-scale confirmation, finalized concentrate specifications, or project-specific commercial toll-treatment terms. Additional metallurgical test work is required before these materials can be assigned a proven processing route with demonstrated recoveries and acceptable operating costs.

10.6.5 HLP Tailings and Sulfides Ag

No silver recovery has been applied to the HLP, tailings, or sulfide flotation cases at this time. Although historical testing reported some silver recovery, the available dataset is limited and variable, and it is not yet supported by sufficient concentrate characterization or downstream payable assumptions. Silver is therefore excluded from the current flotation recovery model and treated as upside potential only, pending additional metallurgical and commercial evaluation.

10.6.6 Summary of Assumptions

Metallurgical recovery assumptions applied in the IA are summarized in Table 10-3. The table distinguishes between recoveries supported by representative column leach test work, adjusted values derived from bottle roll testing, and provisional estimates assigned where direct representative test work is limited. Oxide, mixed, and waste rock dump materials are evaluated within the heap leach framework, whereas historic HLP, tailings, and sulfide materials are considered separately through a preliminary flotation-concentrate route.



Table 10-3: Recovery Assumptions and Process Basis by Material Type

Material Type	Test Basis	Au Rec (%)	Ag Rec (%)	Recovery Basis	Note
Facilities Oxide	Column	83.9	8.1	Column Average	Historical column basis
Sleeper Oxide	Bottle Roll	84.5	9.9	Adjusted Bottle Roll	10% discount applied
West Wood Oxide	Column	76.5	9.0	Column Average	Historical column basis
Facilities Mixed	Column	71.3	22.3	Column Value	Historical column basis
Sleeper Mixed	Limited data	70.0	15.0	Estimated	IA-level assumption
West Wood Mixed	Limited data	65.0	10.0	Estimated	IA-level assumption
North Dump	Column	79.0	40.5	Column Value	Historical column basis
South Dump	Column	69.8	43.9	Column Average	Historical column basis
West Dump	Column	81.4	54.6	Column Value	Historical column basis
HLP and Tailings Material	Flotation/ Limited data	50.0	-	Separate process route	Preliminary flotation/toll milling case
Facilities Sulfide	Flotation	71.2	-	Separate process	Preliminary flotation/toll milling case
West Wood Strong Silicic Sulfide	Flotation	66.1	-	Separate process	Preliminary flotation/toll milling case
West Wood Argillic Sulfide	Flotation	62.3	-	Separate process	Preliminary flotation/toll milling case

For heap leach materials, column leach results were given greater weight than bottle roll results because they better reflect coarse-crush heap leach conditions and leach kinetics. In several cases, column recoveries equaled or exceeded corresponding bottle roll results because some bottle roll tests were run at coarse size and did not reach asymptotic recovery, whereas most column tests were run longer and more closely approached asymptotic extraction under heap-representative conditions. Figure 10-1 presents the comparison of bottle roll and column test results by material type.

No uniform discount has been applied to the reported column-based recoveries at this stage. Although column results are often reduced to approximate field performance, the available data shows substantial variability by material type, particularly within the waste rock dump domains, and does not support a single discount factor across all heap leach materials. Additional variability and confirmatory testing are recommended before applying any blanket reduction.

An exception was made for Sleeper Oxide, for which no representative column leach result is currently available. In this case, the reported bottle roll recovery was reduced by 10% for use in the recovery model to provide a conservative estimate of expected coarse-crush heap leach performance pending confirmatory column testing.

Recoveries for Sleeper Mixed and West Wood Mixed were assigned as IA-level estimates because the available test work is insufficient to support fully representative column-based



recovery assumptions. These values were derived from metallurgical interpretation of the available data and comparison with analogous oxide and mixed composites.

For heap leach consumables, the NaCN consumption value used for capital and operating cost development was derived as 33% of the average laboratory column test consumption. Lime/cement consumption was conservatively based on the average laboratory-scale consumptions, excluding the 40 kg/t North Dump value, with no deduction applied. The historical data shows extreme variability and does not support a representative reduction factor without further test work. Figure 10-2 presents the reagent consumption comparison.

Existing HLP, tailings, and sulfide materials are shown separately because they are not included in the heap leach recovery framework. For IA purposes, these materials are considered through a preliminary flotation process, with rougher concentrate assumed to be sold or toll treated off site. Applied gold recoveries for these materials include a 12% deduction to reflect toll milling and related downstream treatment charges. No silver recovery has been applied to the flotation cases at this stage, and silver is treated as upside potential pending additional metallurgical, concentrate-quality, and commercial evaluation.



Figure 10-1: Comparison of Reported Metallurgical Recovery Results

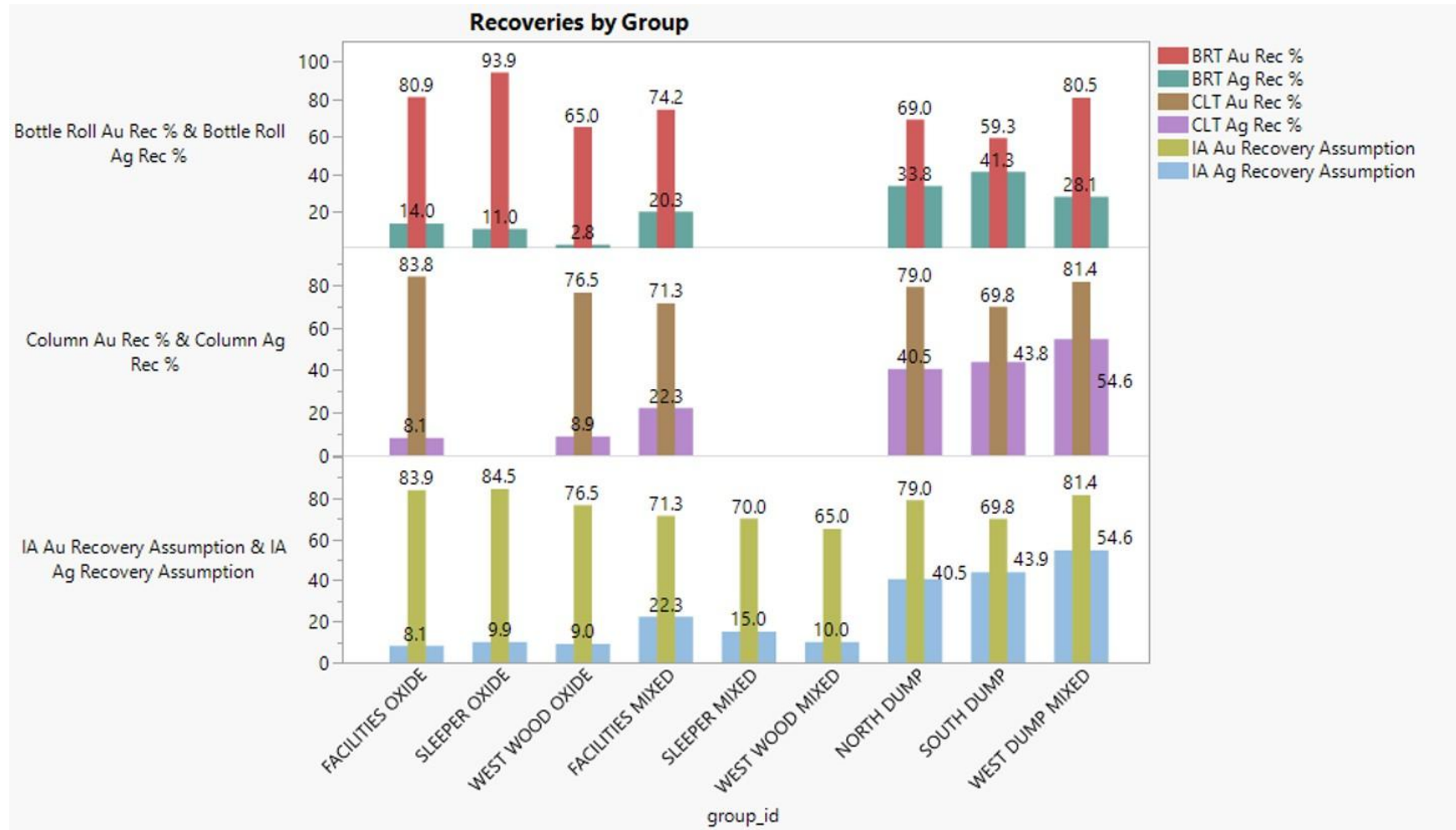
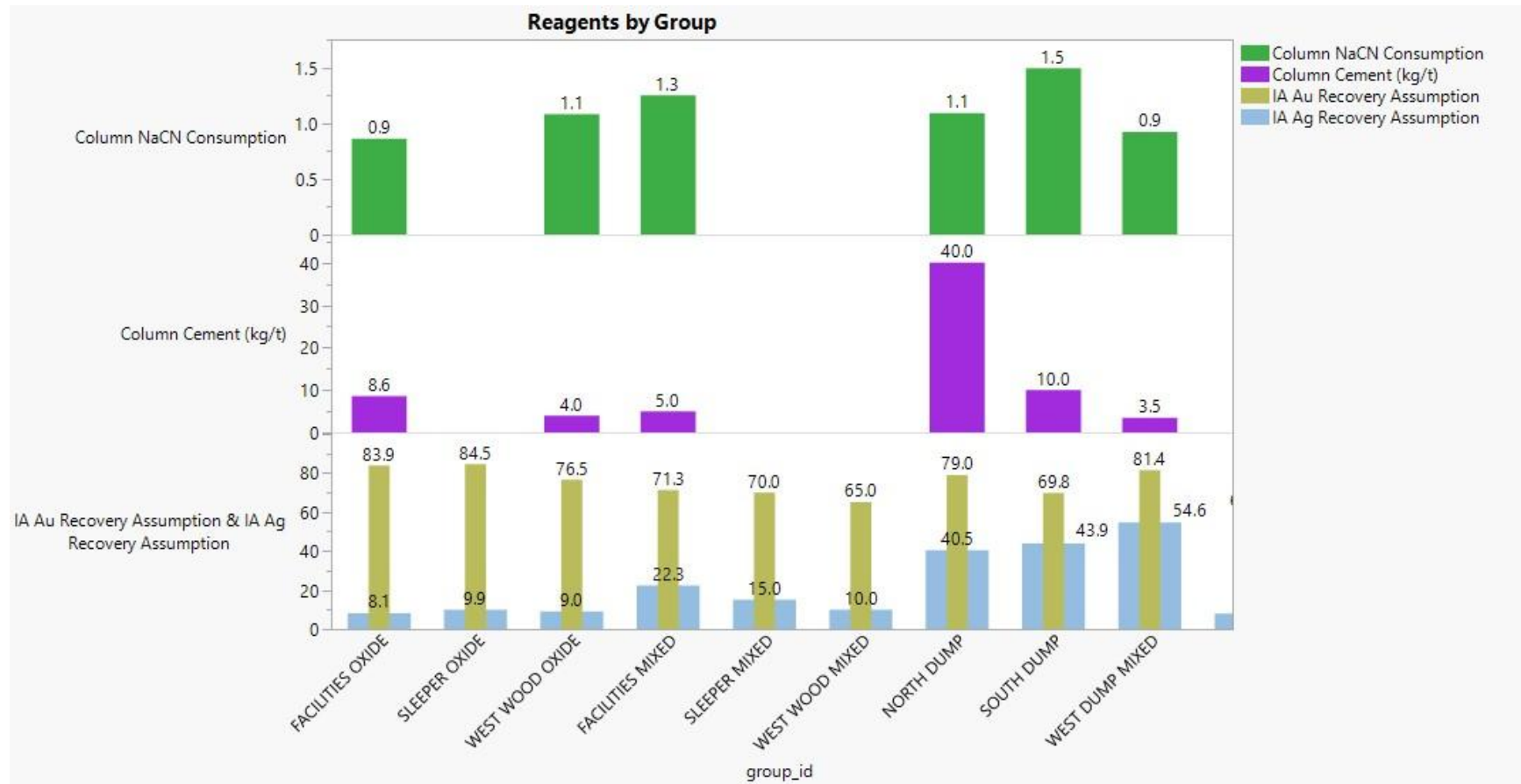


Figure 10-2: Material Specific Reagent Consumption and IA Heap Leach Recovery Assumptions by Material Type



10.7 QP Opinion - Adequacy of Data

In the opinion of the QP, the available metallurgical data are adequate for an IA focused on heap leach processing for oxide, mixed, and existing waste rock dump material.

There is also sufficient metallurgical test work to support the estimation of Mineral Resources from sulfide materials, including existing HLP and tailings material. The proposed processing method for these Mineral Resources is flotation.

The data are not yet adequate to support definitive recoveries, concentrate terms, and operating costs for the flotation case at pre-feasibility level. Additional variability testing, concentrate characterization, marketing review, and process-specific cost definition are required before those materials can be incorporated into a more advanced development scenario.



11.0 Mineral Resource Estimates

The information presented herein has been reviewed, edited, and, where appropriate, directly derived from RESPEC (2023). The Mineral Resource estimate, prepared by RESPEC Company LLC (RESPEC), has been independently reviewed and validated by SLR QPs for completeness, internal consistency, and technical accuracy.

The SLR QPs confirm that the Mineral Resource estimate complies with disclosure requirements of SEC Regulation S-K 1300. The estimate is supported by appropriate geological interpretation, drilling and sampling data, analytical and QA/QC procedures, and industry-standard geostatistical methods. It incorporates inputs and assumptions sufficient to demonstrate reasonable prospects for economic extraction (RPEE). In situ Mineral Resources are classified as Measured, Indicated, or Inferred. Material contained in waste rock dumps, heap leach pads, and tailings storage facilities (TSF) is classified as Inferred. Mineral Resources do not constitute Mineral Reserves.

SLR's review included assessment of the database, geological and domain interpretations, compositing, grade capping, variography, interpolation parameters, classification criteria, and block model validation. The SLR QP assumes responsibility for the estimate and considers it reasonable, suitable for disclosure, and compliant in all material respects with applicable reporting requirements.

This TRS presents an updated Mineral Resource estimate for the Project, with an effective date of April 29, 2026. The estimate incorporates a review of historical drilling for surface material and supersedes prior disclosures, reflecting updated geological interpretation, revised economic parameters, and application of RPEE through open-pit optimization and metallurgical recovery assumptions.

11.1 Summary

The Mineral Resource estimate for the Project was completed using a conventional three-dimensional block modeling approach developed by RESPEC. The workflow included database validation, geological and oxidation domain modeling, density assignment, compositing and grade capping, followed by gold and silver grade interpolation and open-pit constraint using industry-standard software and methodologies.

Gold and silver mineralization domains were defined based on lithology, structure, alteration style, oxidation state, and grade continuity. Separate estimation domains were constructed for gold and silver to reflect differences in grade distribution and continuity. Mineralized domains encompass stockwork, breccia, and vein-related mineralization hosted primarily within altered volcanic units in the hanging wall of the range-bounding fault system. Oxidation was independently modeled and classified into oxide, mixed, and sulfide material, based on its metallurgical significance.

Grade estimation was validated using standard industry practices, including statistical comparison of raw assays, capped values, and composites, as well as comparative estimates generated using inverse distance squared (ID²). Additional validation included swath plots, visual assessment of grade distributions in plan and cross-section, and direct comparison of block estimates against drill hole assays to confirm geological and analytical consistency.

The updated Mineral Resource estimate, prepared by SLR, supersedes prior disclosures for the Project and includes gold and silver only; no other commodities are reported.



In situ Mineral Resources are constrained within an optimized conceptual open-pit shell demonstrating RPEE. Pit optimization assumes open-pit mining and heap leaching, with metallurgical recoveries supported by test work and economic parameters appropriate for the deposit.

The Mineral Resource Estimates (MRE) for the Project are reported by estimation domain consistent with the geological, processing, and material type distinctions illustrated in Figure 11-1. Domain classifications include open-pit oxide material, open-pit sulfide material, and surface material domains comprising west, north, and south dumps, multiple heap leach domains, and tailings storage facility (TSF) material. These domains were defined to reflect differences in lithology, oxidation state, material origin, and anticipated processing response

Mineral Resources are classified in accordance with S-K 1300 definitions (Table 11-1).

The SLR QP is of the opinion that, with consideration of the recommendations summarized in Sections 1 and 23 of this TRS, any issues relating to all relevant technical and economic factors likely to influence the prospect of economic extraction can be resolved with further work.



Figure 11-1: Sleeper Mineral Resource Domains

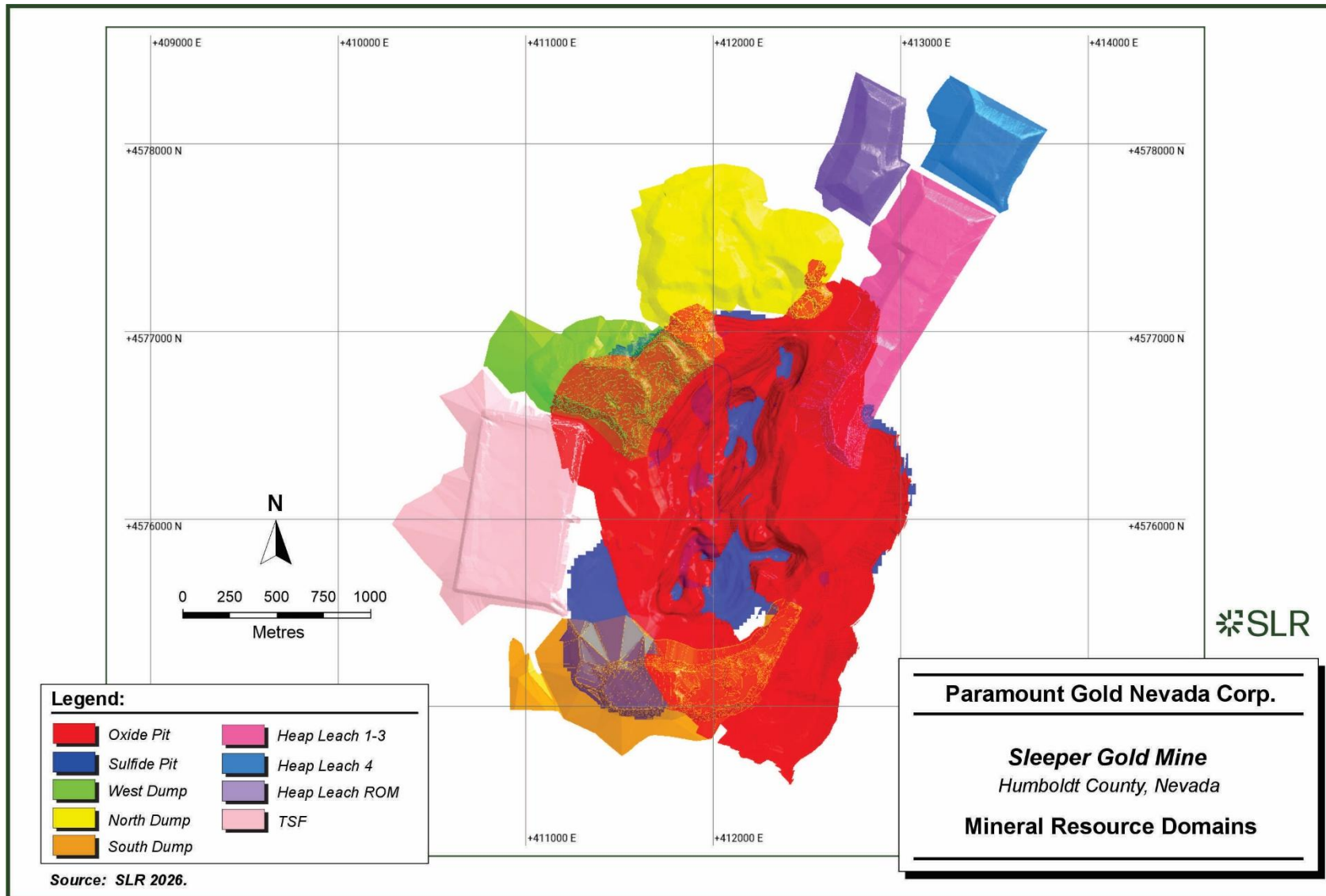


Table 11-1: Summary of Mineral Resources Estimate – April 29, 2026

Category	Tonnage (000 t)	Grade (g/t Au)	Grade (g/t Ag)	Contained Metal (000 oz Au)	Contained Metal (000 oz Ag)	Metallurgical Au Recovery (%)	Metallurgical Ag Recovery (%)
Measured Oxide/Mixed Pit (non-sulfide)	2,004	0.293	3.019	19	195	75.2%	17.1%
Measured Oxide/Mixed Pit (sulfide)	178	0.316	4.307	2	25	70.6%	0.0%
Measured Sulfide Pit	3,347	0.621	3.724	67	401	66.5%	0.0%
Total Measured In Situ	5,528	0.492	3.487	88	620	69.8%	6.2%
Indicated Oxide/Mixed Pit (non-sulfide)	77,899	0.261	3.613	653	9,049	74.2%	17.3%
Indicated Oxide/Mixed Pit (sulfide)	15,941	0.328	4.934	168	2,529	68.7%	0.0%
Indicated Sulfide Pit	85,336	0.393	3.848	1,078	10,558	66.5%	0.0%
Total Indicated In Situ	179,176	0.330	3.842	1,900	22,135	70.1%	7.5%
Total Measured + Indicated In Situ	184,704	0.335	3.832	1,987	22,755	70.0%	7.5%
Inferred Dumps	46,893	0.279	1.941	420	2,927	77.1%	44.6%
Inferred Heap Leach	31,600	0.301	8.363	306	8,497	40.0%	0.0%
Inferred TSF	11,165	0.599	6.221	215	2,233	50.1%	0.0%
Total Inferred Surface	89,658	0.327	4.738	942	13,657	60.6%	23.3%
Inferred Oxide/Mixed Pit (non-sulfide)	48,656	0.235	2.384	367	3,729	76.6%	14.4%
Inferred Oxide/Mixed Pit (sulfide)	4,960	0.286	3.543	46	565	68.9%	0.0%
Inferred Sulfide Pit	94,761	0.311	2.657	948	8,095	66.5%	0.0%
Total Inferred In Situ	148,377	0.285	2.597	1,361	12,390	69.9%	4.7%
Total Inferred Surface + In Situ	238,035	0.301	3.403	2,303	26,047	97.9%	8.8%



Notes:

1. The definitions for Mineral Resources in S-K 1300 were followed for Mineral Resources
2. The Mineral Resource estimate is reported on a 100% ownership basis.
3. The point of reference for the Mineral Resource is before the crusher (in situ).
4. Open Pit Mineral Resources are reported at a cut-off grade ranging from 0.074 g/t to 0.217 g/t Au, depending on area and constrained by a preliminary optimized pit shell with a pit slope angle of 45° for rock and 22° for alluvium and a bench height of 10 m.
5. The optimized pit shell and cut-off grades were generated by assuming metallurgical gold recovery ranging from 63.7% to 85.0% and silver recoveries ranging from 0.0% to 54.6%, standard treatment and refining charges, mining costs of US\$2.40/t moved for open pit, processing costs of \$5.51/t oxide/mixed and \$10.44 sulfide processed, and general and administrative costs of \$0.46/t processed
6. Minimal mining width was 60 m for oxide/mixed material and 20 m for sulfide material
7. Mineral Resources are estimated using a long-term gold price of US\$3,100 per ounce
8. Bulk density ranges from 1.5 t/m³ in the tailings storage area to 2.7 t/m³ for in situ material
9. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.
10. Numbers may not add due to rounding.



11.2 Resource Database

As of the effective date of this report, Paramount and its predecessor operators have completed more than 4,455 drill holes at the Project. These include a mix of reverse-circulation (RC), diamond core (DD), sonic, and limited-auger drilling conducted between 1983 and 2013.

The Mineral Resource database used for the in situ estimate contains 4,258 drill holes, of which 3,994 are located within or near the Mineral Resource model area and were considered in the resource estimation. Drill holes located outside the modeled mineralized zones, including those intersecting unmineralized alluvium or barren volcanic and metasedimentary units, were excluded from the Mineral Resource estimate.

Drill holes associated with the heap leach and waste rock dumps were treated as separate estimation domains; however, the estimated mineralized material from these domains is included in the Mineral Resource Estimate.

The Project Mineral Resource database includes surveyed drill hole collar locations, down-hole survey data (dip and azimuth), gold and silver assay data, geological and alteration logs, oxidation state information, and supporting QA/QC records collected from multiple drill programs. Drill holes or assay intervals deemed unreliable due to data integrity issues or potential contamination were marked and excluded from grade estimation in accordance with SLR’s modeling protocols.

The compilation, validation, and appropriateness of the drilling database for Mineral Resource estimation were reviewed by SLR QP, who agrees that the dataset is suitable for supporting the Mineral Resource estimate under SEC Regulation S-K1300, subject to the classification limitations discussed elsewhere in this report.

Table 11-2: Summary of Drill Hole Data used in Mineral Resource Estimation

Area	No. Holes	Total Depth (m)	Average Depth (m)	Number of Records		
				Survey	Lithology	Assay
In Situ	4,258	640,572.96	150.43	10,709	287,878	320,560
North Dump	34	1316.4	38.71	34	0	868
South Dump	22	789.36	35.88	22	0	425
West Dump	18	552.01	30.66	18	0	381
Heap Leach 1-3	31	772.83	24.45	31	0	827
Heap Leach 4	9	205.17	22.79	9	0	270
TSF	83	824.61	9.93	80	0	553
Grand Total	4,455	645,033.34	312.85	10,903	287,878	323,884

11.3 Geological Interpretation

The Project is located within the northern Nevada rift, where gold–silver mineralization is hosted in a structurally controlled epithermal system within Middle Miocene volcanic rocks. The geological model reflects this fault-controlled geometry and incorporates the established regional volcanic stratigraphic framework. The model integrates lithological, structural, alteration, oxidation, and assay data from multiple drilling campaigns to define the

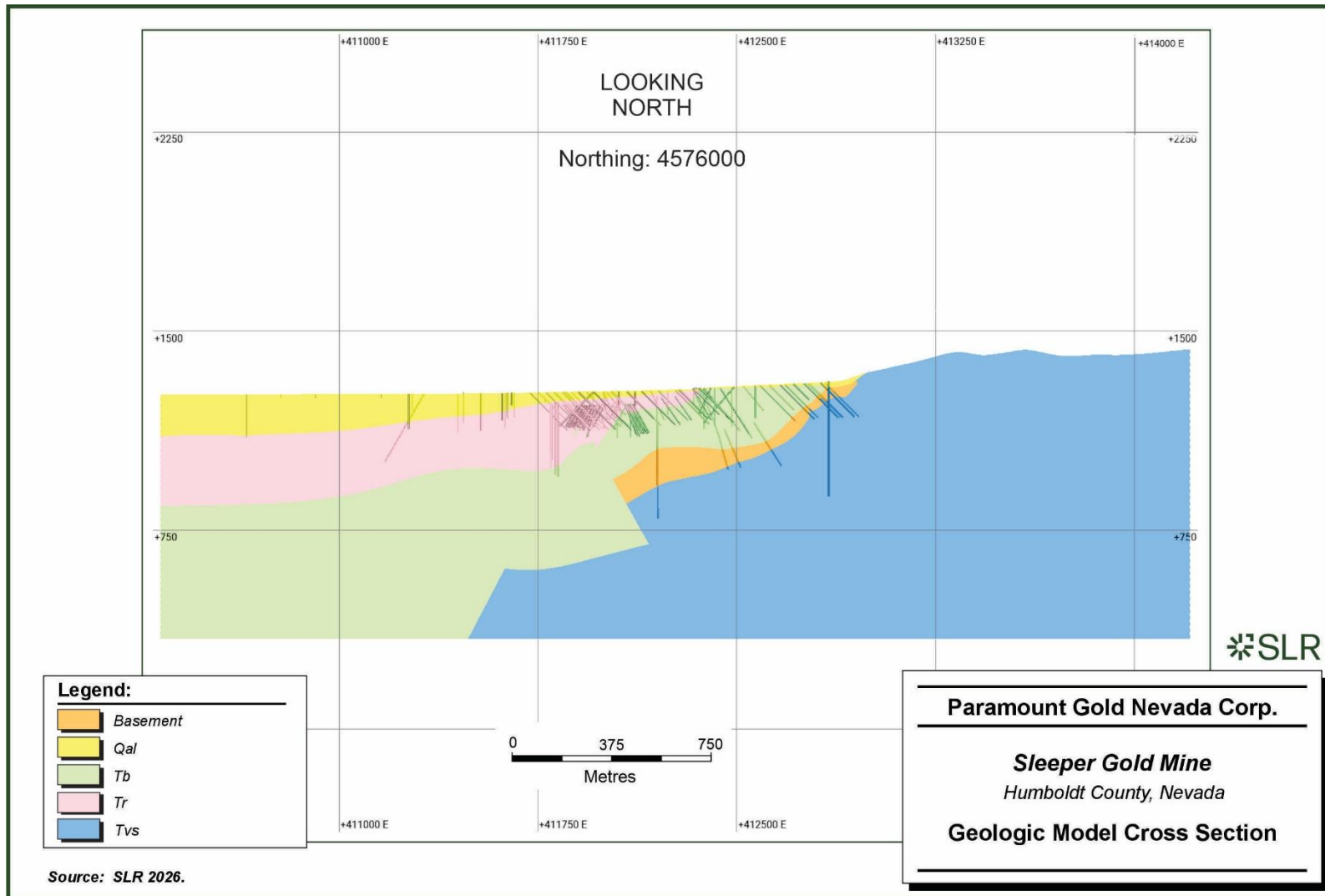


three-dimensional distribution of mineralized rock. Geological interpretation focuses on the volcanic host sequence and the principal fault systems that control the geometry and continuity of mineralization and constrain the Mineral Resource model, as illustrated in Figure 11-2. The geological model was reinterpreted and refined by SLR based on the original geological modeling framework described in RESPEC (2023).

At the local scale, the geological model defines fault-bounded mineralized zones characterized by vein-, breccia-, and stockwork-style mineralization. These zones are spatially associated with structural features, lithological contrasts, and areas of enhanced permeability and extend along strike and down-dip from the historical mining area into adjacent zones. In addition, distinct estimation domains were created within the heap leach and waste rock dumps to account for differences in material type, grade distribution, and metallurgical behavior relative to in-situ mineralization.



Figure 11-2: Sleeper Geologic Model Cross Section



Source: SLR 2026.



11.3.1 Mineralization

In situ mineralization at the Project was subdivided into three grade-based mineral domains to support Mineral Resource estimation and to reflect differences in grade distribution, continuity, and variability of gold and silver mineralization. The domains were defined primarily on gold-grade populations, with silver domains guided by the spatial distribution of gold, given their strong genetic and spatial association, and consisted of a low-grade, mid-grade, and high-grade domain.

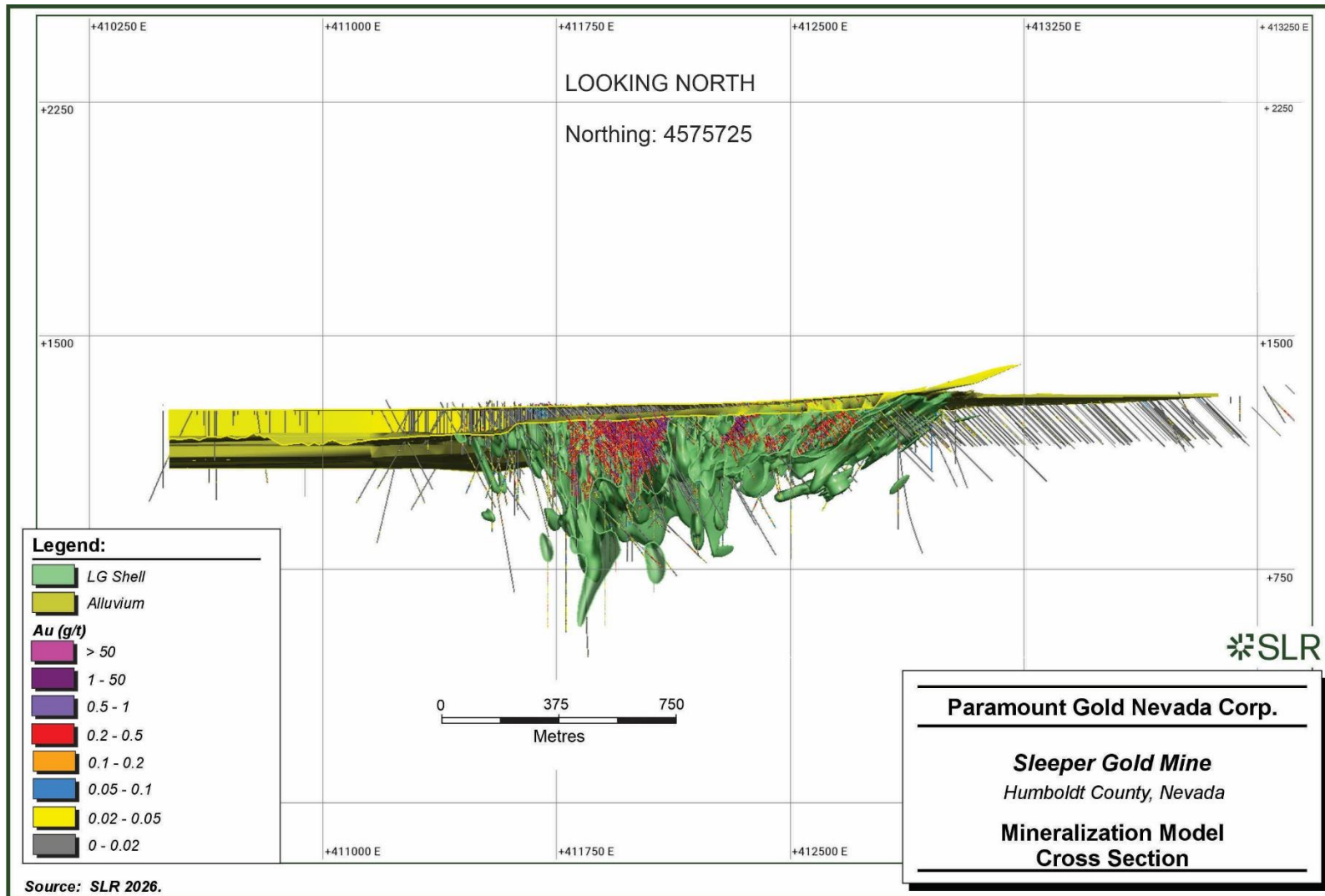
The low-grade (LG) domain represents disseminated and stockwork mineralization that forms a laterally and vertically extensive envelope surrounding higher-grade mineralization, as illustrated in Figure 11-3. This domain comprises most of the mineralized volume and is characterized by relatively continuous grades and lower variance. This domain is modeled at a cut-off grade of 0.1 g/t Au to 1.0 g/t Au and 1.80 g/t Ag to 10 g/t Ag.

The mid-grade (MG) domain comprises narrow veins and hydrothermal breccias that extend down-dip and laterally from areas of historically mined high-grade mineralization. Mineralization within this domain exhibits moderate continuity and increased grade variability relative to the low-grade domain. Boundaries between the low- and mid-grade domains are generally sharp and grade-controlled. This domain is modeled at a cut-off grade of 1.0 g/t Au to 8.0 g/t Au and 10 g/t Ag to 20 g/t Ag.

The high-grade (HG) domain represents discrete, discontinuous zones of bonanza-grade mineralization associated with banded quartz–chalcedony veins and localized hydrothermal breccias. These zones are typically narrow, steeply dipping, structurally controlled, and exhibit high-grade variability. Contacts between the mid- and high-grade domains are commonly gradational. This domain is modeled at a cut-off grade of > 8.0 g/t Au and >20 g/t Ag.



Figure 11-3: Sleeper Mineralization Model Cross Section



11.3.2 Oxidation Model

An oxidation model was developed to support in-situ Mineral Resource estimation and associated metallurgical recovery assumptions by defining the spatial distribution of oxide, mixed, and sulfide material. The oxidation model was re-interpreted and refined based on the original oxidation framework described in RESPEC (2023). The review of the historical database identified instances in which oxide and sulfide intervals were locally exchanged or inconsistently coded. These inconsistencies were addressed through SLR's reinterpretation, which incorporated geological context and supporting information to correct oxidation assignments for the current Mineral Resource estimate.

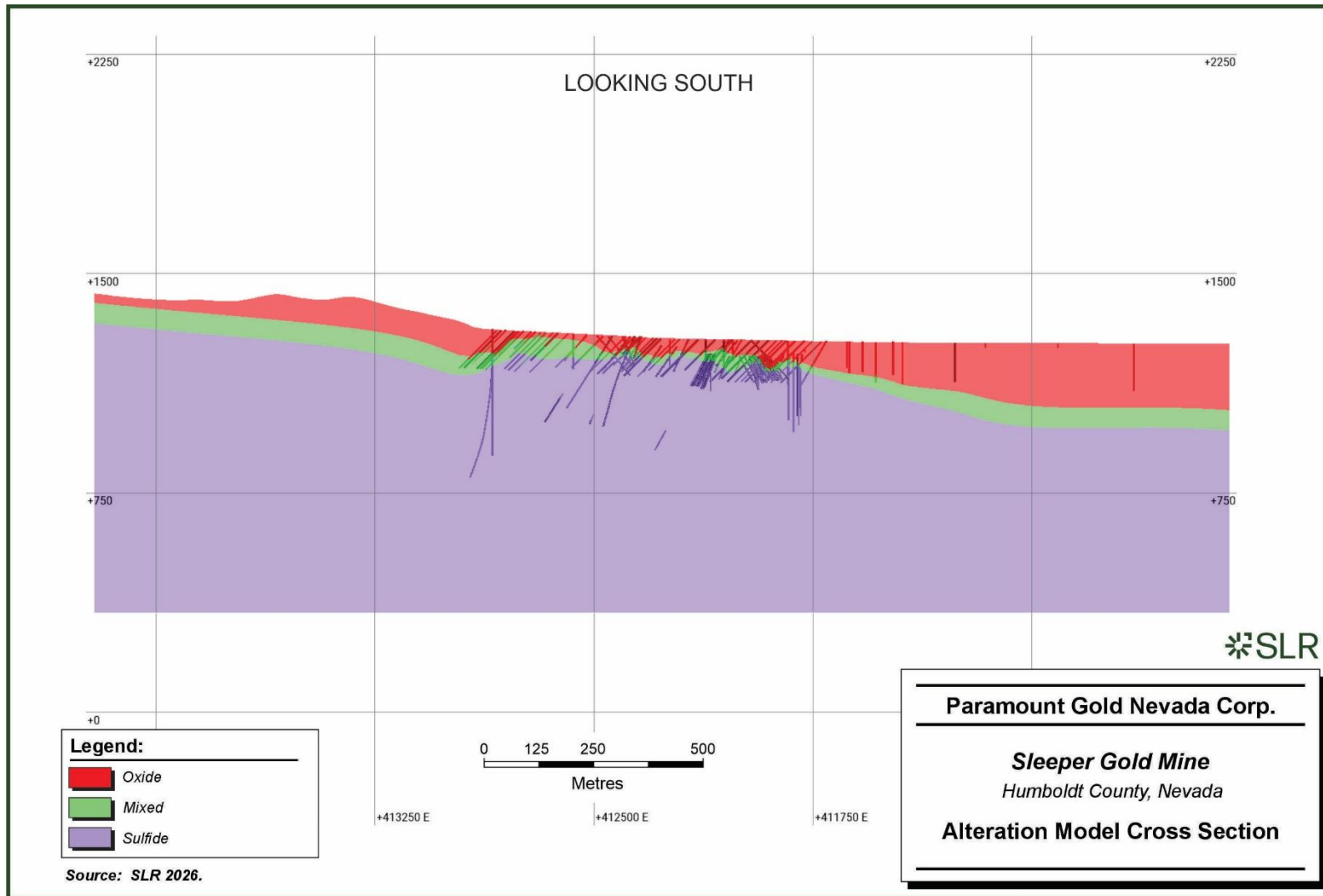
Oxidation-state interpretation was based on geological logging, alteration characteristics, and historical mining information, with oxide material representing fully oxidized mineralization, mixed material representing partially oxidized mineralization, and sulfide material representing relatively unoxidized mineralization dominated by primary sulfide assemblages. Oxidation domains were modeled independently of lithology and mineralization domains and constrained using drill hole data and sectional interpretations, reflecting a general transition from oxide material near the surface to sulfide material at depth, with locally variable boundaries influenced by structure and permeability.

While the identified oxidation coding issues were corrected within the current SLR reinterpretation, the SLR QP recommends additional verification and review for future Mineral Resource estimation updates, particularly where oxidation state affects metallurgical routing, recovery assumptions, and economic parameters.

In the opinion of the SLR QP, the refined oxidation model is appropriate for the current in situ Mineral Resource estimation in accordance with SEC Regulation S-K 1300 and CIM (2019) Best Practice Guidelines, subject to the limitations noted above.



Figure 11-4: Sleeper Alteration Model Cross Section



11.4 Resource Assays

Gold and silver assay intervals were coded to mineralization domains prior to any statistical treatment or grade estimation. Domain coding was based on the interpreted geological and mineralization models and confirmed that assays were assigned solely to geologically consistent populations. This method prevented the mixing of mineralized and non-mineralized material and ensured that subsequent statistical analysis, capping, compositing, and interpolation were performed within appropriate geological controls.

Only assays from accepted drill holes and intervals were coded for resource estimation. Intervals impacted by identified down-hole contamination or other data quality issues were excluded from further analysis.

11.5 Treatment of High-Grade Assays

11.5.1 Capping Levels

Gold and silver assay data for the Sleeper deposit were coded by mineral domain, including modeled mineralized domains, Outside domains, and alluvium (Qal), prior to grade interpolation as part of the in-situ mineral resource estimation. Domain coding ensured that assay data were assigned to geologically appropriate populations and that subsequent statistical analysis, capping, and interpolation honored geological controls. Assay data were then evaluated for high-grade outliers to ensure that estimated block grades are representative of the underlying mineralization and not unduly influenced by extreme values. The Sleeper deposit exhibits significant grade variability and localized nugget effects, characteristic of low-sulfidation epithermal gold-silver mineralization; accordingly, assay capping and high-grade restrictions were applied as complementary risk-management measures consistent with accepted industry practice.

Assay capping was conducted on a domain-by-domain basis, recognizing that grade distributions, continuity, and variability differ between mineralized domains, Outside domains, and alluvium (Table 11-3). Domain-specific gold and silver capping thresholds were established using statistical analysis, including histogram, log-probability plot, and descriptive statistics reviews. The selected caps were designed to limit the influence of rare, extreme assay values while preserving the overall grade tenor and geological character of each domain. Assay values exceeding the selected domain caps were reduced to the cap value prior to compositing and grade estimation.

Table 11-3: Sleeper In Situ Gold and Silver Capping Levels by Domain

Domain	Au Samples Capped	Au Cap (g/t)	Ag Samples Capped	Ag Cap (g/t)
Outside	19	6	76	20
Low-Grade	107	3	154	35
Mid-Grade	0	N/A	8	65
High-Grade	0	N/A	0	N/A
Alluvium (Qal)	23	5	0	N/A



11.6 Compositing

Capped gold and silver grade assay intervals from drill holes were combined into 3.05 m composite lengths for in situ grade estimation to ensure consistent sample support. This composite length was chosen to honor historical assay data originally sampled at 5 ft intervals and then converted to metric units, aligning closely with the original sampling support used in most drilling at the Sleeper deposit. The selected composite length is appropriate, given the drill spacing and the style of mineralization (Table 11-4 and Table 11-5). Figure 11-5 illustrates a histogram of the distribution of composite lengths.

Material sampled from waste rock dumps and heap leach pads was combined into 5 m intervals to reflect the broader sampling support and the generally lower spatial variability typical of these areas. Compositing strictly respected mineral domain boundaries, ensuring no composite included assay data from more than one domain. Residual intervals at the ends of drill holes, at domain boundaries, or at dump and heap leach pad boundaries were composited using length-weighted averaging.

The resulting gold and silver composites were reviewed statistically to confirm that the compositing methodology produced stable and representative grade distributions suitable for block-model interpolation. In the opinion of the QP, the compositing procedures applied are appropriate for the nature of the available data and support the estimation of Mineral Resources.

Figure 11-5: Histogram of Sample Lengths in the Estimation Domains

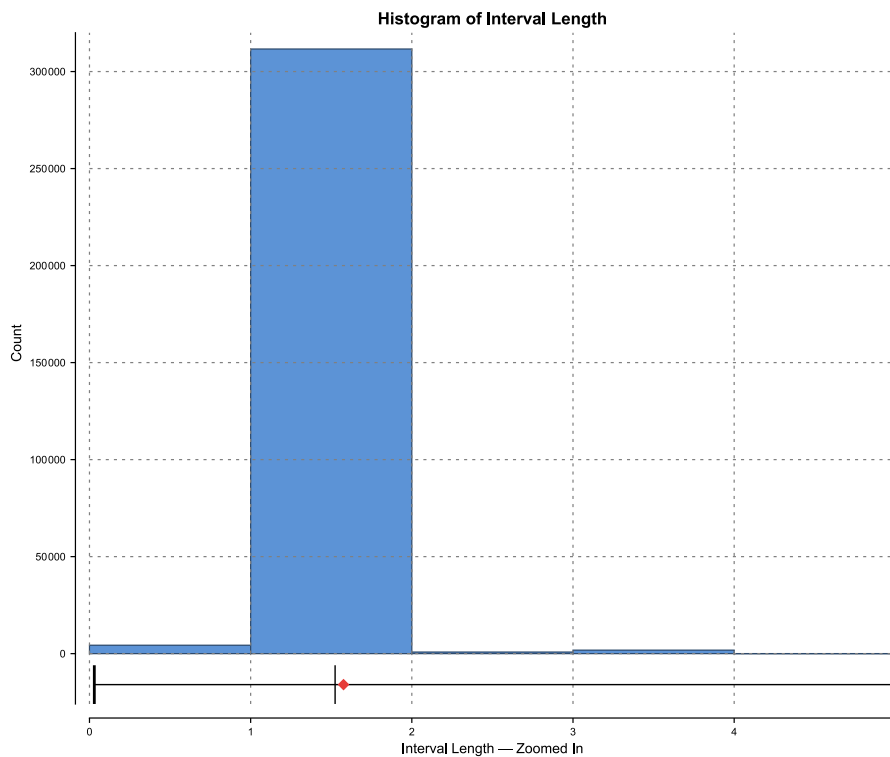


Table 11-4: Sleeper In Situ Gold Composite by Domain

Domain		Pre-Capping Au (g/t)	Post-Capping Au (g/t)
Low-Grade Gold	Median	0.24	0.24
	Mean	0.30	0.30
	SD	0.33	0.23
	Maximum	34.00	3.00
Mid-Grade Gold	Median	1.46	1.46
	Mean	1.84	1.84
	SD	1.16	1.16
	Maximum	27.63	27.63
High-Grade Gold	Median	11.02	11.02
	Mean	19.52	19.52
	SD	31.33	31.33
	Maximum	297.73	297.73
Alluvium (Qal)	Median	0.71	0.71
	Mean	1.43	1.10
	SD	2.25	1.11
	Maximum	15.23	5.00
Outside Gold	Median	0.03	0.03
	Mean	0.09	0.06
	SD	6.48	0.13
	Maximum	1497.58	6.00



Table 11-5: Sleeper In Situ Silver Composite by Domain

Domain		Pre-Capping Ag (g/t)	Post-Capping Ag (g/t)
Low-Grade Silver	Median	3.33	3.33
	Mean	4.24	4.02
	Std Dev	7.34	3.07
	Maximum	478.01	35.00
Mid-Grade Silver	Median	13.31	13.31
	Mean	14.06	13.81
	Std Dev	10.75	4.17
	Maximum	402.73	65.00
High-Grade Silver	Median	33.43	33.43
	Mean	55.17	55.17
	Std Dev	90.94	90.94
	Maximum	1683.41	1683.41
Alluvium (Qal)	Median	5.94	5.94
	Mean	6.32	6.32
	Std Dev	2.81	2.81
	Maximum	13.03	13.03
Outside Silver	Median	0.31	0.31
	Mean	0.63	0.60
	Std Dev	2.44	0.98
	Maximum	274.70	20.00

11.7 Spatial Analysis

11.7.1 Variography

Spatial continuity was evaluated to assess the suitability of the data for geostatistical interpolation and to determine whether variogram models could be reliably developed. This review considered grade distributions, spatial continuity, and potential directional trends within the mineralized domains. The available dataset did not demonstrate sufficient variability or well-defined spatial structure to support the development of robust and defensible variogram models.

Given the limited variability and the absence of a clearly defined anisotropy, formal variography was not undertaken, and grade estimation was completed using inverse distance squared (ID²) and inverse distance cubed (ID³) interpolation methods, which do not require variogram inputs. A planar ellipsoid search strategy was applied to reflect the general geometry of the mineralized zones and to provide appropriate spatial weighting of sample data during estimation.



11.8 Bulk Density

Bulk density values used for the Mineral Resource estimate were assigned by material type, lithology, and, where applicable, redox domain. Bulk density values were applied to convert block model volumes to tonnage. A total of 2,546 in situ bulk density measurements were available from historical drilling programs completed by X-Cal and Paramount. Density determinations were derived from water-immersion measurements on drill core samples. The density data were reviewed for reasonableness and statistically summarized prior to application in the resource model.

For the in situ Mineral Resource estimate, the dataset has a sample-weighted average applied density of approximately 2.33 g/cm³. The strongest sample support is in Tertiary Sleeper Rhyolite Mixed (970 samples) and Tertiary Sleeper Basalt Mixed (800 samples), both assigned 2.33 g/cm³. Tertiary Intrusive Felsic is also well supported, with 398 samples and an applied density of 2.36 g/cm³.

In situ density assignments show expected lithological variation. Quaternary Alluvium was assigned 1.90 g/cm³; West Wood Breccia, Breccia, and Tertiary Sleeper Volcanic Sediment range from 2.35 g/cm³ to 2.46 g/cm³; Tertiary Sleeper Rhyolite ranges from 2.18 g/cm³ to 2.33 g/cm³; Tertiary Sleeper Basalt ranges from 2.24 g/cm³ to 2.33 g/cm³; and Mesozoic Basement was assigned the highest density at 2.64 g/cm³. These values are consistent with the expected density contrast between unconsolidated cover, volcanic host rocks, intrusive units, and basement.

Density values were assigned deterministically to block model cells based on lithology and oxidation state and were not interpolated. This approach provides consistent and stable tonnage estimates given the distribution, spatial coverage, and quality of the available density measurements. Representative values were selected for each lithologic and redox domain based on measured data and supplemented by geological judgment where direct measurements were limited.

Lower densities assigned by SLR to the waste rock dumps, heap leach, and TSF reflect deposited, crushed, stacked, or rehandled material with greater void space than competent in situ bedrock. The applied density of 1.80 g/cm³ for waste rock dumps is reasonable for broken, rehandled waste rock in a Nevada open-pit gold setting. The applied density of 1.65 g/cm³ for heap leach material reflects crushed and stacked leach material. The applied density of 1.50 g/cm³ for tailings is consistent with lower-density deposited tailings material.

In the opinion of the SLR QP, the density assignment methodology and applied values are appropriate for the style of mineralization and the available data and are adequate for use in estimating Mineral Resources.

The applied densities used in the Mineral Resource estimation are summarized in Table 11-6.



Table 11-6: Sleeper Density Values by Lithology

Material / Lithology	Redox Domain	No. Samples	Density Range (g/cm ³)	Applied Density (g/cm ³)
Waste Rock Dumps	All	521	Not reported	1.80
Heap Leach	All	187	Not reported	1.65
TSF	All	Not reported	Not reported	1.50
Quaternary Alluvium	All	7	1.76–2.42	1.90
West Wood Breccia	All	20	2.04–2.56	2.35
Breccia	All	1	2.42–2.42	2.42
Tertiary Intrusive Felsic	All	398	0.06–2.90	2.36
Tertiary Intrusive Mafic	All	0	Not reported	2.30
Tertiary Sleeper Rhyolite	All	115	1.86–3.11	2.18
Tertiary Sleeper Rhyolite	Oxide	84	1.68–2.42	2.18
Tertiary Sleeper Rhyolite	Mixed	970	1.39–3.83	2.33
Tertiary Sleeper Basalt	Sulfide	28	1.88–2.48	2.24
Tertiary Sleeper Basalt	Oxide	51	1.91–2.65	2.33
Tertiary Sleeper Basalt	Mixed	800	1.58–3.74	2.33
Tertiary Sleeper Volcanic Sediment	Sulfide	26	2.06–2.80	2.46
Mesozoic Basement	All	46	2.32–3.24	2.64

11.9 Block Models

The in situ mineralization geology model was developed by RESPEC using Seequent Leapfrog Geo software, while grade estimation for the in situ Mineral Resource Estimate was completed in MineSight. SLR imported the completed in situ block model estimate into Leapfrog Geo for review, validation, and integration with the waste rock dump, heap leach, and tailings models. The waste rock dump, heap leach, and tailings Mineral Resource Estimates were prepared by SLR using Seequent Leapfrog Geo, version 2025.3. Collectively, these models provide the basis for domain-controlled estimation, validation, integration, and final Mineral Resource reporting.

11.9.1 RESPEC In situ

The in situ block model was constructed using an unrotated approach. Each block was assigned to the geological domain containing its centroid, ensuring appropriate domain representation and that grade estimation and reporting were constrained to the relevant geological controls. The model was oriented with an azimuth, dip, and plunge of 0.0° and employed a parent block size of 10 m (X) × 10 m (Y) × 10.0 m (Z) to reflect the geometry of the mineralized zones and the anticipated selective mining unit dimensions, while honoring the interpreted geological surfaces and wireframes. The block model was prepared by RESPEC and includes representations of the in situ mineralized zones (Table 11-7).



Table 11-7: Summary of In Situ Block Model Extents

Description	Easting (X) (m)	Northing (Y) (m)	Elevation (Z) (masl)
Block Model Origin (lower left corner)	410,520	4,573,830	1600
Parent Block Dimension (m)	10	10	10
Number of Blocks	333	412	120
Rotation	0	0	0

11.9.2 SLR Waste Rock Dumps and Heap Leach

The heap leach and dump block model was constructed in Leapfrog Edge (version 2025.2.1) using an unrotated, sub-blocked approach. Each block was assigned to the geological domain containing its centroid, ensuring appropriate domain representation. The model was oriented with an azimuth, dip, and plunge of 0.0° and employed a parent block size of 10 m (X) by 10 m (Y) by 5 m (Z) to reflect the deposit geometry and anticipated selective mining unit dimensions, while honoring modeled geological surfaces. A summary of the block model extents is provided in Table 11-8.

Table 11-8: Summary of Waste Rock Dumps and Heap Leach Block Model Extents

Description	Easting (X) (m)	Northing (Y) (m)	Elevation (Z) (masl)
Block Model Origin (lower left corner)	410,020	453,830	1600
Parent Block Dimension (m)	10	10	5
Number of Blocks	383	462	240
Rotation	0	0	0

11.9.3 SLR Tailing Storage Facility

The TSF block model was constructed in Leapfrog Edge (version 2025.2.1) using an unrotated, sub-blocked approach. Each block was assigned to the geological domain containing its centroid, ensuring appropriate domain representation. The model was oriented with an azimuth, dip, and plunge of 0.0° and employed a parent block size of 10 m (X) by 10 m (Y) by 5. m (Z) to reflect the deposit geometry and anticipated selective mining unit dimensions, while honoring modeled geological surfaces. A summary of the block model extents is provided in Table 11-9.

Table 11-9: Summary of TSF Block Model Extents

Description	Easting (X) (m)	Northing (Y) (m)	Elevation (Z) (masl)
Block Model Origin (lower left corner)	410,020	453,830	1600
Parent Block Dimension (m)	10	10	5
Number of Blocks	383	462	240
Rotation	0	0	0



11.9.4 SLR Vulcan Block Model

For final Mineral Resource Estimate reporting, the in situ, waste rock dump, heap leach, and tailings block models were combined into one regularized 10 m × 10 m × 10 m block model using Maptek Vulcan software. The consolidated Vulcan model provided a consistent reporting framework across all material types and was used for final MRE tabulation and disclosure.

11.10 Search Strategy and Grade Interpolation Parameters

Gold and silver grades for the Sleeper deposit were estimated for the in situ Mineral Resource estimate using domain-controlled inverse-distance interpolation methods applied to the three-dimensional block model. Grade interpolation was completed separately by mineralized domain to ensure that estimates honored the geological controls, grade populations, and spatial continuity characteristics established during domain modeling.

The primary estimation method was inverse-distance weighting, with inverse distance cubed (ID^3) applied to the mid-grade and high-grade domains and inverse distance squared (ID^2) applied to the low-grade domains. These domain-specific distance powers were selected to reflect differences in grade variability, continuity, and nugget effect, while balancing local grade influence against excessive smoothing. Ordinary kriging (OK) and nearest-neighbor (NN) estimates were also generated for validation and comparison against the inverse-distance estimates.

Interpolation used domain-specific search ellipsoids, orientations, and maximum search distances consistent with the geometry of the mineralized zones. Sample selection was controlled by minimum, maximum, and maximum-per-hole constraints to reduce spatial bias and limit over-representation of closely spaced drill data. Although the RESPEC (2023) report does not expressly use the term “hard boundaries,” the estimation workflow is consistent with hard-boundary estimation, as composite samples were restricted to their respective grade domains and were not used across domain contacts. Partial-volume block coding was used to represent domain proportions within blocks; however, the report does not document the use of soft-boundary interpolation or cross-domain sample sharing.

In the opinion of the SLR QP, the grade interpolation approach is appropriate for the in situ Mineral Resource estimate. The use of domain-controlled estimation, domain-specific search parameters, and validation checks is consistent with SEC Regulation S-K 1300 reporting expectations and CIM (2019) Best Practice Guidelines.

11.10.1 High Grade Restriction

In addition to assay capping, high-grade restrictions (HGRs) were applied during grade interpolation to limit the spatial influence of elevated composite grades. The restrictions were implemented using grade–distance limits, whereby composites above defined threshold grades were restricted to a shorter search distance, generally less than the primary search ellipse and commonly approximating one-half of the main search distance.

High-grade restriction thresholds were selected by estimation domain based on statistical review, grade distribution analysis, and visual assessment of the apparent continuity of high-grade values. This approach was used to reduce the potential for grade smearing and localized overestimation, particularly in domains characterized by high-grade variability or nugget effect. Thresholds and restriction distances were defined on a domain-specific basis to reflect geological continuity, grade population characteristics, and confidence in spatial continuity (Table 11-10).



The effects of assay coding, capping, and high-grade restrictions were evaluated by comparing pre- and post-capping statistics and reviewing grade distributions. Based on this review, the selected controls appropriately limited the influence of extreme values without materially altering mean grades or distorting the underlying domain grade populations.

Table 11-10: Sleeper Estimation Parameters by Domain

Domain	Min Samples	Max Samples	Max per Hole	Search Major	Search Semimajor	Search Minor (Vertical)	ID Power	Au Grade Cap	Au Distance (m)	Ag Grade Cap	Ag Distance (m)
Low-Grade	1	12	3	1	1	0.5	2	1.6	75	10.5	75
Mid-Grade	1	12	3	1	1	0.33	3	8	75	30	75
High-Grade	1	12	4	1	1	0.33	3	100	75	290	75
Outside Domains	2	12	3	1	1	0.5	2	1.1	20	11	20
Qal	1	9	3	1	1	0.5	3	1.5	20	11	20

In the opinion of the SLR QP, the combined application of domain-specific assay coding, assay capping, and high-grade restrictions is appropriate for the style of mineralization and the quality and variability of the available data and supports the estimation of Mineral Resources.

11.11 Reasonable Prospects for Economic Extraction for Mineral Resources

Mineral Resources must demonstrate reasonable prospects for economic extraction (RPEE), which generally implies that the quantity and grade estimates meet certain economic thresholds and that the Mineral Resources are reported at an appropriate cut-off grade, taking into account extraction scenarios.

Metal prices used to determine Mineral Reserves are based on consensus long-term forecasts from banks, financial institutions, and other sources. For Mineral Resources, metal prices are typically higher than those used for Mineral Reserves.

A reporting cut-off grade was established for the Project based on assumed costs for an open pit mining and heap leaching operation and commodity prices that provide a reasonable basis for establishing RPEE for Mineral Resources.

These cost references were modified to align with the Project's assumed production rate. These cost and price assumptions have been used to inform an optimization process using the Whittle optimized pit shell software. Metallurgical recoveries and process costs were applied by metallurgical domains (Table 10-3)

11.11.1 Cut-off Grade Estimation

To demonstrate RPEE in accordance with SEC Regulation S-K 1300, Mineral Resources were constrained within pit shells developed using Whittle pit optimization software. The optimization incorporated gold and silver prices of US\$3,100/oz and US\$34/oz, with payable metal factors of 99% and royalties of 3%. Selling costs of US\$6.00/oz Au and US\$0.50/oz Ag were applied.

The Whittle pit-optimization metallurgical recoveries were applied on a material-type basis, reflecting variability across oxide, mixed, and sulfide domains.



The pit optimization utilized material-specific processing costs ranging from US\$5.51/t (heap leach) to US\$10.44/t (sulfide processing), with general and administrative costs of US\$0.46/t processed. Mining costs of US\$2.40/t moved were applied in the pit optimization but excluded from the cut-off grade (COG) calculation.

Open-pit Mineral Resources are reported within the selected Whittle pit shells (an Oxide/Mixed Pit and a Sulfide Pit) at material-specific cut-off grades derived from the above economic parameters and metallurgical assumptions. The applied cut-off grades (g/t Au) by material type are summarized in Table 11-11. Figure 11-6 illustrates the spatial distribution of material types across the project area.

These cut-off grades reflect differences in metallurgical recovery (Au recovery ranging from 40.0% to 84.5% for leachable materials and from 50.1% to 71.2% for sulfides; Ag recovery ranging from 0% to 54.6%) and processing routes. Sulfide material is assigned a higher cut-off grade due to increased processing costs and lack of defined recoveries within the current flowsheet assumptions.

The Whittle pit shell serves solely as a reporting constraint and does not represent a Mineral Reserve, mine plan, or final pit design. Mineralized material below the applicable cut-off grade or outside the optimized pit shell is excluded from the reported Mineral Resources.

For reporting, the block model was reblocked to a 10 m bench height consistent with the open-pit mining assumption. No additional mining dilution or mining recovery factors were applied. The applied cut-off grades and pit constraint are considered appropriate to support RPEE and Mineral Resource disclosure.



Figure 11-6: Sleeper Material Type/Area Distribution Map

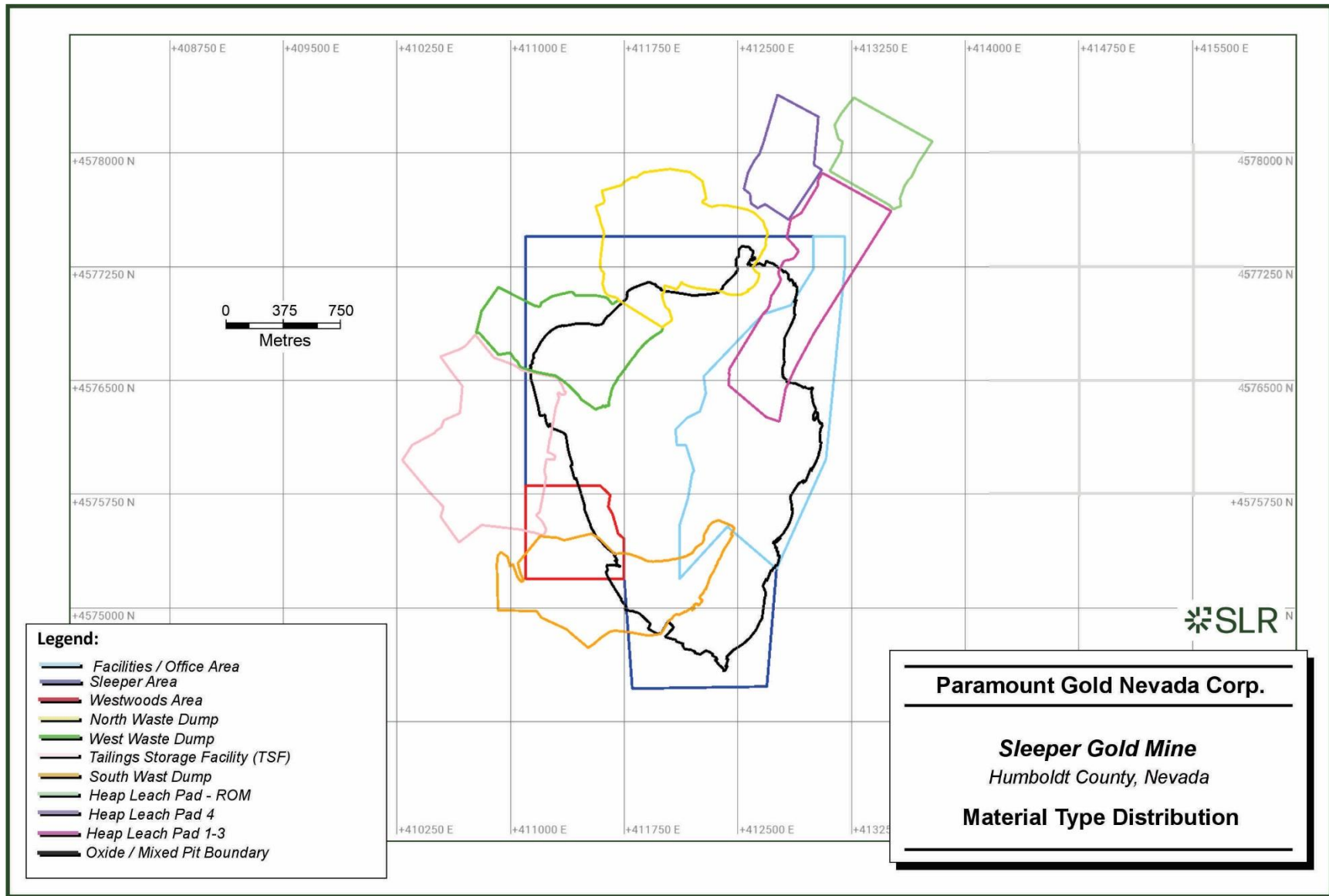


Table 11-11: Sleeper Cut-off Grade Parameters by Domain

Area	Unit	West Wood Sulfide	Facilities / Office Sulfide	TSF	Heap	North Dump	South Dump	West Dump	Alluvium
Block Model Codes	Type	Sulfides	Sulfides	Mixed	Mixed	Oxide	Oxide	Oxide	Oxide
Recovery Code	RecCode ¹	15	14	13	12	11	10	9	8
Price Au	US\$/oz	3,100	3,100	3,100	3,100	3,100	3,100	3,100	3,100
Price Ag	US\$/oz	34	34	34	34	34	34	34	34
Payable	%	99%	99%	99%	99%	99%	99%	99%	99%
Selling Cost Au	US\$/oz	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00
Selling Cost Ag	US\$/oz	0.50	0.50	0.50		0.50	0.50	0.50	0.50
Royalties	%	3%	3%	3%	3%	3%	3%	3%	3%
Net Price Au	US\$/g	95.53	95.53	95.53	95.53	95.53	95.53	95.53	95.53
Recovery Au	%	64.2%	71.2%	50.1%	40.0%	79.0%	69.8%	81.4%	60.0%
Recovery Ag	%	0.0%	0.0%	0.0%	0.0%	40.5%	43.9%	54.6%	8.0%
Mining (excluded from COG)	\$/t mined	2.40	2.40	2.40	2.40	2.40	2.40	2.40	2.40
Processing	\$/t processed	10.53	10.26	10.15	4.00	5.51	5.51	5.51	5.51
G&A		0.46	0.46	0.46		0.46	0.46	0.46	0.46
COG	gr/tonne	0.179	0.157	0.222	0.105	0.079	0.089	0.077	0.104



Area	Unit	Facilities / Office Oxide	Facilities / Office Mixed	Sleeper Oxide	West Wood Oxide	Sleeper Mixed	West Wood Mixed	Sulfides
Block Model Codes	Type	Oxide	Mixed	Oxide	Oxide	Mixed	Mixed	Sulfides
Recovery Code	RecCode ¹	7	6	5	4	3	2	1
Price Au	US\$/oz	3,100	3,100	3,100	3,100	3,100	3,100	3,100
Price Ag	US\$/oz	34	34	34	34	34	34	34
Payable	%	99%	99%	99%	99%	99%	99%	99%
Selling Cost Au	US\$/oz	6.00	6.00	6.00	6.00	6.00	6.00	6.00
Selling Cost Ag	US\$/oz	0.50	0.50	0.50	0.50	0.50	0.50	0.50
Royalties	%	3%	3%	3%	3%	3%	3%	3%
Net Price Au	US\$/g	95.53	95.53	95.53	95.53	95.53	95.53	95.53
Recovery Au	%	83.9%	71.3%	84.5%	76.5%	70.0%	65.0%	66.5%
Recovery Ag	%	8.1%	22.3%	9.9%	9.0%	15.0%	10.0%	0.0%
Mining (excluded from COG)	\$/t mined	2.40	2.40	2.40	2.40	2.40	2.40	2.40
Processing	\$/t processed	5.51	5.51	5.51	5.51	5.51	5.51	10.44
G&A		0.46	0.46	0.46	0.46	0.46	0.46	0.46
COG	g/t Au	0.074	0.088	0.074	0.082	0.089	0.096	0.171

Note:

- 1 Recovery Code: RECCODE is a variable added to the block model to designate material type based on the metallurgical recovery factor for reporting Mineral Resources



11.11.2 Factors Affecting the Mineral Resource

Mineral Resources, which are not Mineral Reserves, do not have demonstrated economic viability. The Mineral Resource Estimate is reported within a Whittle optimized open-pit shell and at material-specific cut-off grades derived from the economic, metallurgical, and cost parameters summarized in Section 11.11.1. At the time of reporting, the SLR QP is not aware of any title, taxation, socio-political, marketing, or other relevant issues that materially impact the Mineral Resource estimate beyond those outlined below.

Key factors that may materially affect the Mineral Resource estimate are listed:

- Changes to metal price assumptions (US\$3,100/oz Au and US\$34/oz Ag) and associated payable factors (99%) and royalties (3%), which directly influence net realized metal values and cut-off grades.
- Changes to cut-off grade assumptions, including processing costs, which underpin the material-specific cut-off grades applied for reporting.
- Changes to metallurgical recovery assumptions by material type, which directly impact economic value and cut-off grade determination.
- Changes to the assumptions and parameters used in the Whittle pit optimization, including slope angles, cost inputs, and economic criteria used to define the reporting pit shell for RPEE as described in Sections 13.1 and 13.2 of this report.
- Changes to geological interpretations, including mineralized domain geometry, continuity, and grade distribution, which may affect block model estimation and classification.
- Changes resulting from additional drilling, sampling, or data acquisition that modify the understanding of geological controls, grade continuity, or domain boundaries.
- Changes to estimation methodology, including treatment of high-grade values (e.g., capping and high-grade restrictions), which may influence grade distribution and local estimates.
- Changes to assigned bulk density values, which directly impact tonnage estimates.

11.11.3 QP Comments on the Prospect of Economic Extraction

The Mineral Resources are reported within Whittle optimized open-pit shells using a gold price of US\$3,100/oz and material-specific cut-off grades derived from appropriate cost, recovery, and economic assumptions. These parameters are consistent with current market conditions and industry benchmarks for comparable Nevada gold operations.

In the QP's opinion, the combination of metal price assumptions, metallurgical recoveries, processing costs, and pit optimization parameters provides a reasonable basis for demonstrating RPEE. The use of material-specific cut-off grades and a Whittle pit shell constraint appropriately reflects the variability in processing performance and economic value across material types and supports the technical and economic plausibility of the reported Mineral Resources.

11.12 Classification

Mineral Resources for the Project were classified as Measured, Indicated, and Inferred in accordance with SEC Regulation S-K 1300, using a conservative, block-level classification



methodology that integrates drill-hole confidence, data density, proximity to supporting data, geological continuity, and verification status, consistent with CIM (2019) Best Practice Guidelines. Classification was applied only to blocks located within modeled mineral domains and constrained to material demonstrating reasonable prospects for economic extraction.

Resource classification was controlled using quantitative criteria summarized in Table 11-12 incorporating drill hole confidence codes, sample counts, and distance to the nearest informing samples:

- Measured Mineral Resources were defined within modeled domains where drill hole confidence codes are ≥ 0.9 , supported by at least seven samples with a closest sample distance of ≤ 10 m.
- Indicated Mineral Resources were defined within modeled domains where drill hole confidence codes are ≥ 0.55 , supported either by at least seven samples within ≤ 22 m, or by at least two samples within ≤ 10 m.
- Inferred Mineral Resources comprise remaining modeled domain material not meeting Measured or Indicated criteria, or material supported by drill hole confidence codes ≥ 0.5 with at least one sample within ≤ 10 m.

Drill hole confidence codes were assigned by the drilling program based on the availability and quality of supporting documentation used for data verification, including assay certificates and down-hole surveys, and range from 1.0 (full documentation available) to 0.0 (no supporting documentation). These confidence attributes were propagated to the block model and used as a primary control on classification. Drill intervals with insufficient documentation or identified data quality concerns were excluded from resource estimation.

In the opinion of the SLR QP, the resulting Measured, Indicated, and Inferred Mineral Resource classifications appropriately reflect the current level of geological confidence and data reliability for the Sleeper deposit. Additional data verification and targeted infill drilling is required to support future upgrades of Inferred material to higher-confidence resource categories.

Table 11-12: Summarized Methodology for Resource Classification

Class	Confidence Code	Sampling & Distance Criteria	Data Quality / Documentation
Measured	≥ 0.9	≥ 7 samples with the closest sample ≤ 10 m	Fully verified data; complete assay certificates and down-hole survey documentation
Indicated	≥ 0.55	≥ 7 samples ≤ 22 m or ≥ 2 samples ≤ 10 m	Assay data available with partial supporting documentation; some limitations in historical records
Inferred	≥ 0.5	≥ 1 sample with the closest sample ≤ 10 m	Limited supporting documentation; data verification is incomplete or reliant on historical drilling

11.13 Block Model Validation

Block model validation was conducted to ensure the Mineral Resource estimate for the Project is consistent with the input data, geological interpretation, and estimation methodology.

The process included:



- Global Statistical comparison of block grades against composite grades to evaluate estimation bias and smoothing.
- Visual inspection of grade distribution, domain boundaries, and composite alignment using cross-sections and 3D views.
- Swath plots to assess grade trends along principal directions and confirm the model reflects spatial patterns in the data.

The QP found grade continuity to be reasonable and confirmed that the block grades were reasonably consistent with local drill hole composite grades.

11.13.1 Global Statistics

Statistical comparisons were conducted between composite grades and estimated block grades to evaluate the consistency of the interpolation. This analysis helps identify potential smoothing or bias and ensures that the block model reasonably reflects the input data, as shown in Table 11-13 through Table 11-16.

Table 11-13: Summary of Composite vs Block Model Mean Au (ppm) Oxide/Mixed Pit – In Situ

Area	Oxide		Mixed		Sulfide	
	Comp	Block Model	Comp	Block Model	Comp	Block Model
Count	23,429	108,433	13,763	57,481	8,633	13,613
Mean	0.11	0.08	0.26	0.19	0.32	0.24
SD	0.37	0.13	0.40	0.17	1.11	0.21
CV	3.47	1.71	1.58	0.88	3.49	0.85
Variance	0.14	0.02	0.16	0.03	1.24	0.04
Min	0.00	0.00	0.00	0.00	0.00	0.00
Lower Quartile	0.00	0.00	0.06	0.07	0.08	0.13
Median	0.01	0.01	0.16	0.16	0.18	0.21
Upper Quartile	0.10	0.11	0.31	0.26	0.35	0.30
Max	13.96	4.27	21.53	4.63	79.26	6.72



Table 11-14: Summary of Composite vs Block Model Mean Au (ppm) Sulfide Pit – In Situ

Area	Oxide		Mixed		Sulfide	
	Comp	Block Model	Comp	Block Model	Comp	Block Model
Count	9,781	40,769	3,001	19,406	33,856	114,569
Mean	0.05	0.05	0.13	0.08	0.43	0.26
SD	0.22	0.09	0.36	0.13	2.15	0.38
CV	4.62	1.87	2.70	1.52	5.04	1.47
Variance	0.05	0.01	0.13	0.02	4.63	0.14
Min	0.00	0.00	0.00	0.00	0.00	0.00
Lower Quartile	0.00	0.00	0.01	0.01	0.04	0.10
Median	0.00	0.01	0.03	0.04	0.16	0.22
Upper Quartile	0.03	0.07	0.10	0.10	0.38	0.32
Max	14.11	2.51	6.23	2.36	244.75	35.02

Table 11-15: Summary of Composite vs Block Model Mean Au (ppm) Dumps

Area	North Dump		West Dump		South Dump	
	Comp	Block Model	Comp	Block Model	Comp	Block Model
Count	231	17,725	102	9,886	111	11,780
Mean	0.32	0.30	0.14	0.15	0.13	0.14
SD	0.31	0.20	0.23	0.14	0.19	0.09
CV	0.96	0.68	1.58	0.90	1.41	0.69
Variance	0.09	0.04	0.05	0.02	0.04	0.01
Min	0.00	0.01	0.00	0.00	0.00	0.00
Lower Quartile	0.06	0.15	0.02	0.06	0.00	0.07
Median	0.25	0.27	0.05	0.11	0.03	0.12
Upper Quartile	0.47	0.44	0.16	0.19	0.26	0.19
Max	1.37	0.99	1.48	1.24	1.36	1.10



Table 11-16: Summary of Composite vs Block Model Mean Au (ppm) Heaps and TSF

Area	Heap Leach 1-3		Heap Leach 4		TSF	
	Comp	Block Model	Comp	Block Model	Comp	Block Model
Count	142	15,896	45	5,498	207	10,061
Mean	0.28	0.28	0.37	0.35	0.65	0.61
SD	0.13	0.09	0.11	0.06	0.15	0.13
CV	0.45	0.30	0.31	0.17	0.23	0.21
Variance	0.02	0.01	0.01	0.00	0.02	0.02
Min	0.06	0.00	0.20	0.20	0.00	0.04
Lower Quartile	0.20	0.23	0.29	0.31	0.55	0.51
Median	0.25	0.28	0.35	0.34	0.66	0.61
Upper Quartile	0.34	0.32	0.43	0.37	0.77	0.72
Max	0.79	0.68	0.62	0.58	1.09	1.04

The SLR QP reviewed the statistical results and observed that the estimated block grades are consistent with the composite grades, with no material bias or over-smoothing. The QP considers the statistical comparison results to be reasonable and supportive of the reported Mineral Resource Estimate.

11.13.2 Visual Comparison

Cross-sections, long sections, and 3D views were reviewed to verify that block grades align with composite data and are properly constrained within mineralized domains. Cross sections through the oxide/mixed pit and the sulfide pit are shown in Figure 11-7 and Figure 11-8, respectively.

The QP confirms that the visual inspection shows good agreement between block estimates and input composites. No inconsistencies or estimation artifacts were observed.



Figure 11-7: East-West Cross Section Oxide Pit

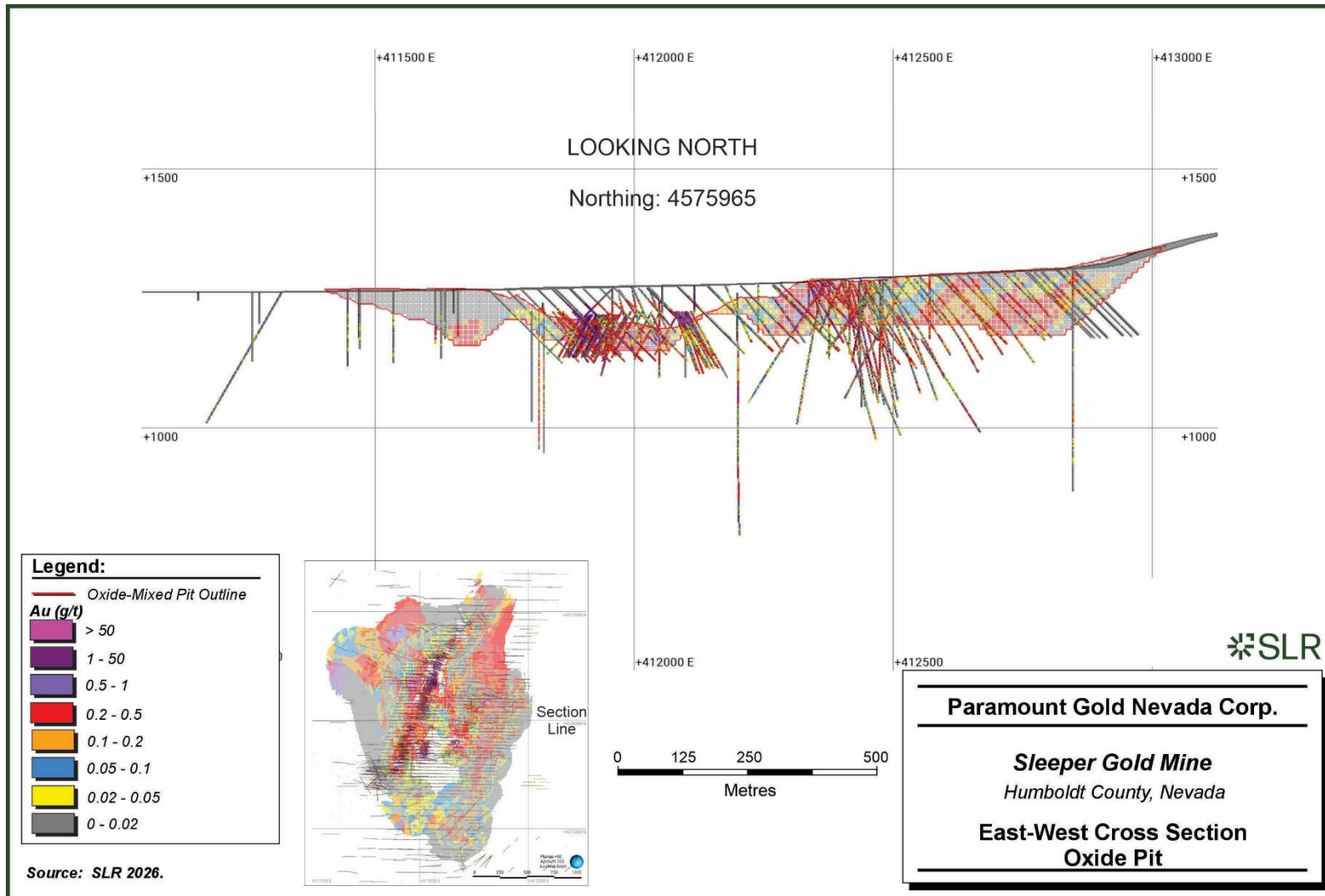
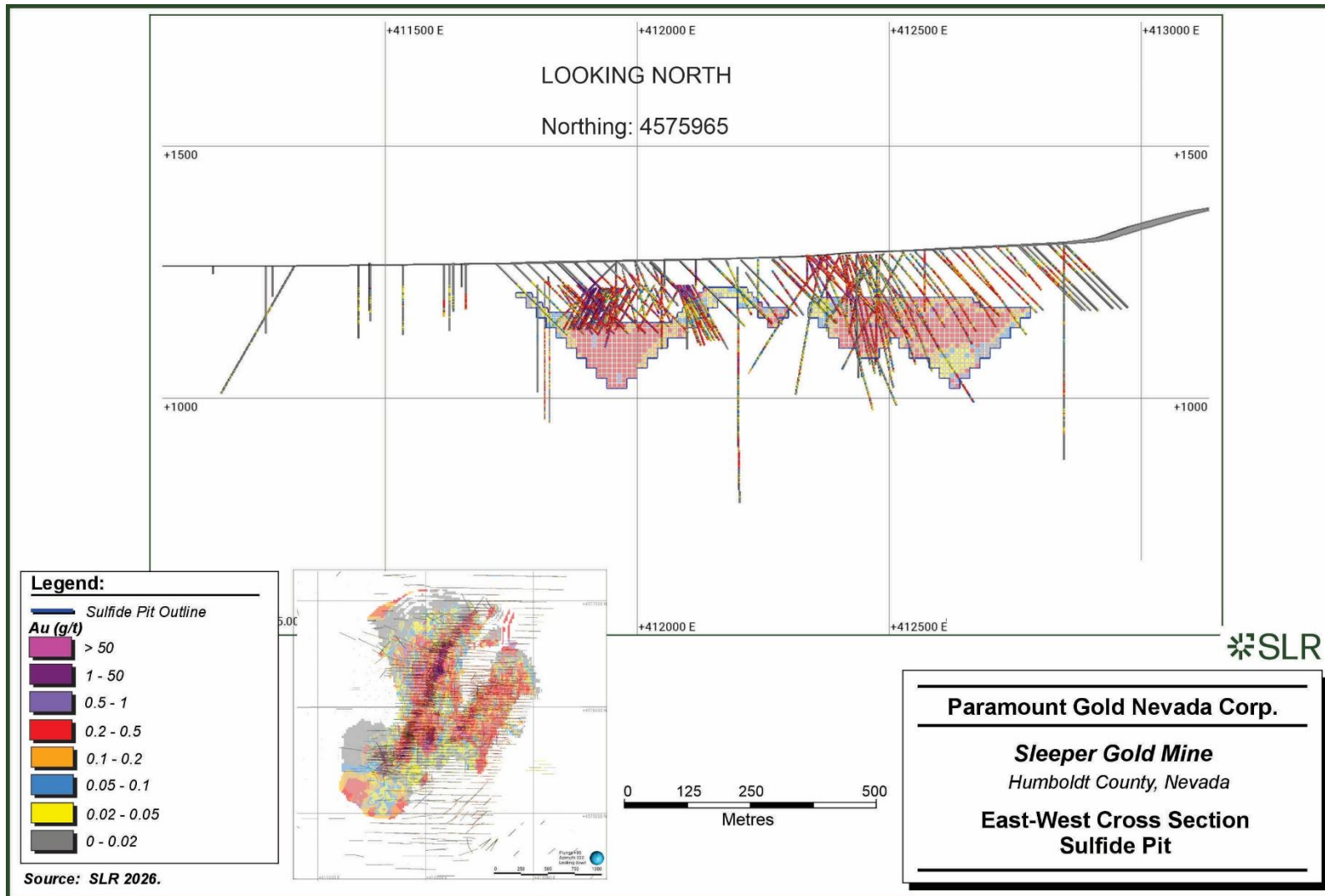


Figure 11-8: East-West Cross Section Sulfide Pit



11.13.3 Swath Plots

Swath plots were generated to compare composite and block grades along the easting, northing, and elevation directions. These plots are used to assess local grade trends and continuity, and to verify that the block model appropriately reflects the spatial grade distribution observed in the underlying data. Representative examples for the Waste rock dumps, Heap Leach Pads, and Tailings Storage Facilities (TSF) are presented in Figure 11-9 through Figure 11-11.

The QP reviewed the swath plots and confirmed that the block models satisfactorily reproduce the grade trends observed in the composite data. No significant smoothing or anomalous behavior is evident, and there is good spatial correlation between composite grades and block model grades.



Figure 11-9: Swath Plots in the X, Y, and Z Directions – Waste Rock Dumps

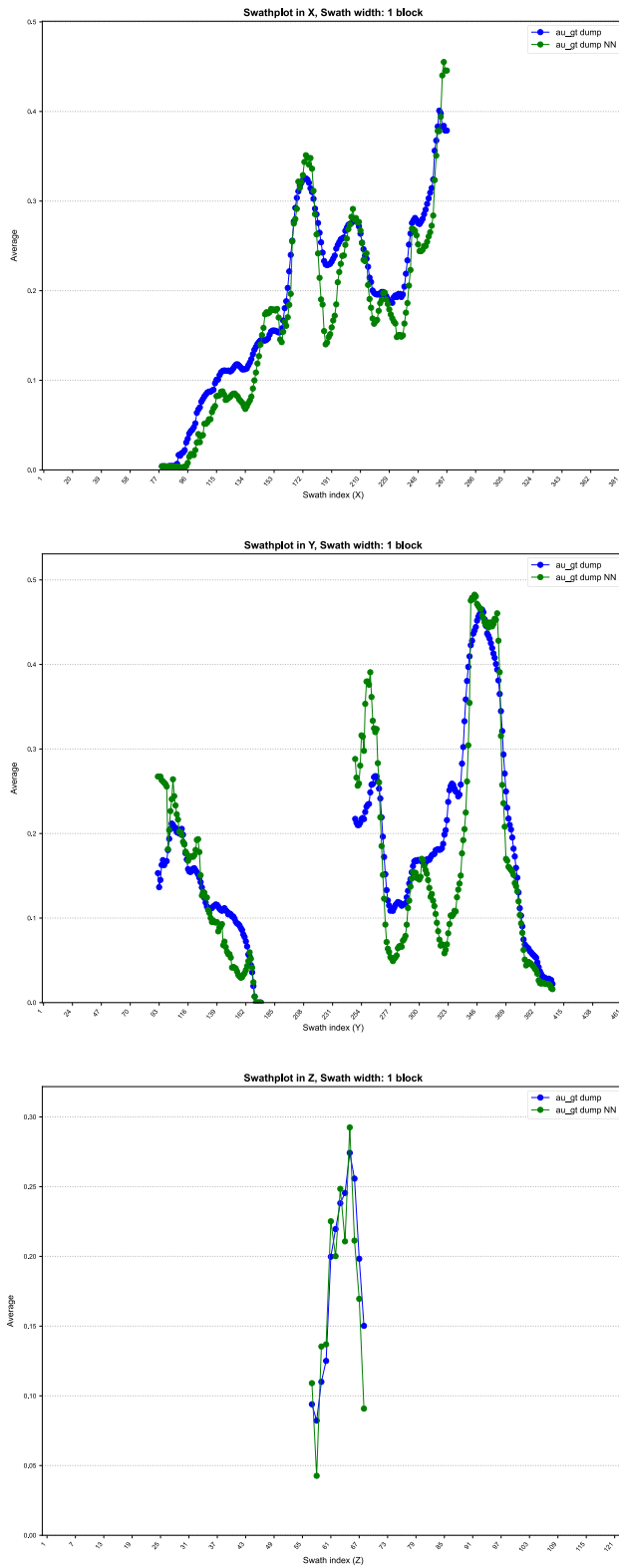


Figure 11-10: Swath Plots in the X, Y, and Z Directions – Heap Pads

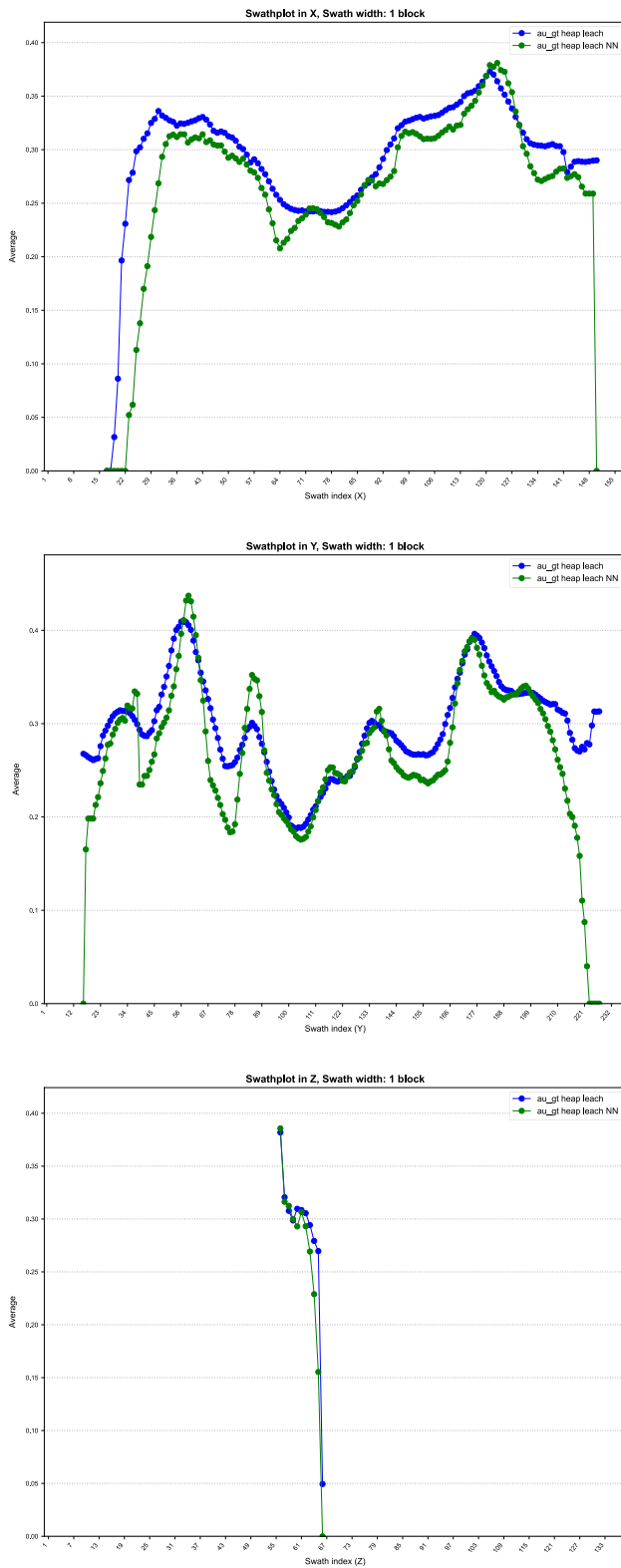
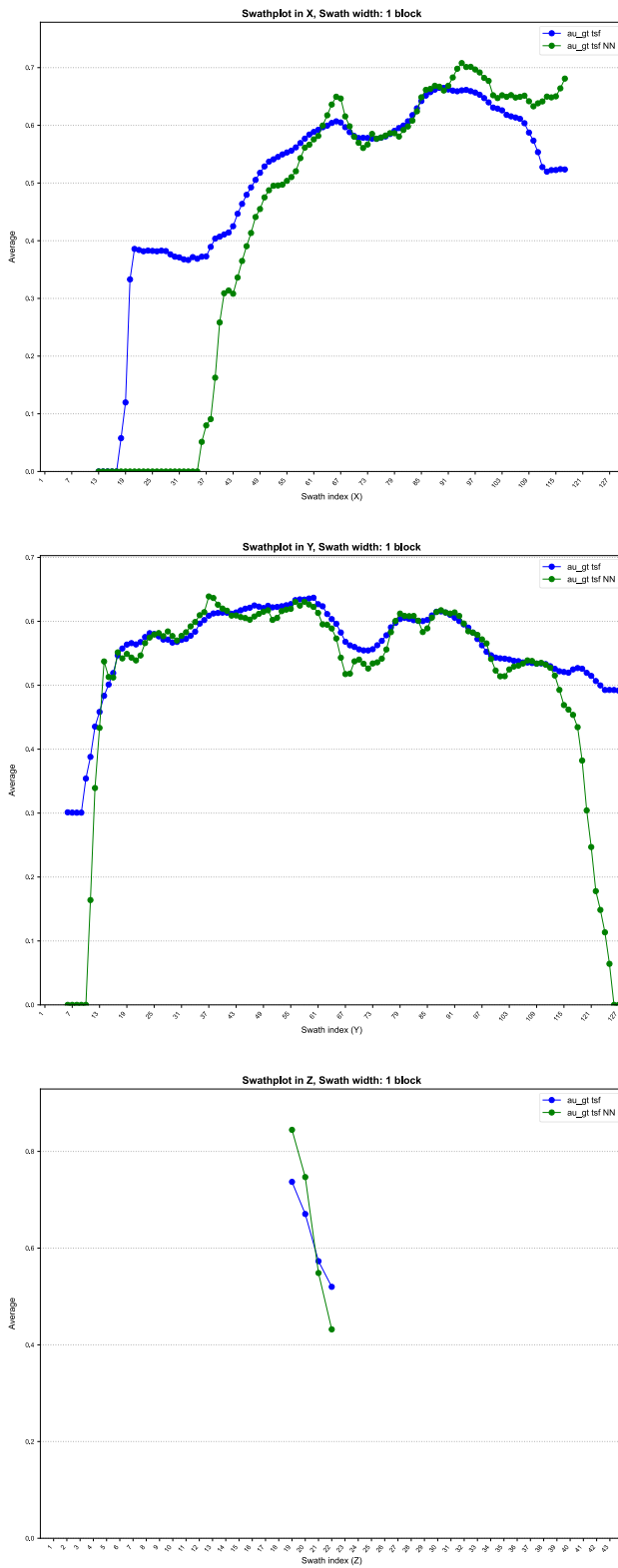


Figure 11-11: Swath Plots in the X, Y, and Z Directions – TSF



11.14 Sensitivity to Reporting Cut-off

The reported Mineral Resource estimates for the Project are sensitive to the metal price assumptions used to establish the reporting cut-off parameters. To evaluate this sensitivity, Mineral Resource tonnage and average grade estimates derived from the block model were assessed for oxide and mixed open pit scenarios across a range of gold price assumptions from US\$1,500/oz to US\$4,500/oz. The analysis applies to Measured + Indicated Mineral Resources and incorporates corresponding revenue factors, metallurgical recovery assumptions, and waste-to-ore strip ratios (Table 11-17 and Figure 11-12).

At lower gold price assumptions, reported Mineral Resource tonnage is limited to higher-grade material, resulting in lower total tonnes, higher average gold grades, and relatively low strip ratios. As the gold price assumption increases, additional lower-grade material becomes reportable, resulting in a material increase in reported Mineral Resource tonnage, a corresponding decrease in average gold grade, and progressively higher strip ratios. Metallurgical recovery assumptions remain relatively consistent across the evaluated price range.

A gold price of US\$3,100/oz was selected for the cash flow estimate presented in this report. For purposes of by-product valuation, this assumption corresponds to a silver price of US\$34/oz, equivalent to a silver-to-gold price ratio of approximately 0.011:1, or silver pricing representing approximately 1.1% of the assumed gold price.

This sensitivity analysis demonstrates that the reported Mineral Resource estimates are materially dependent on the selected metal price assumptions and associated reporting cut-off parameters and supports the conclusion that the reported Mineral Resources have RPEE within the range of metal price assumptions evaluated, consistent with the requirements of Regulation S-K 1300.

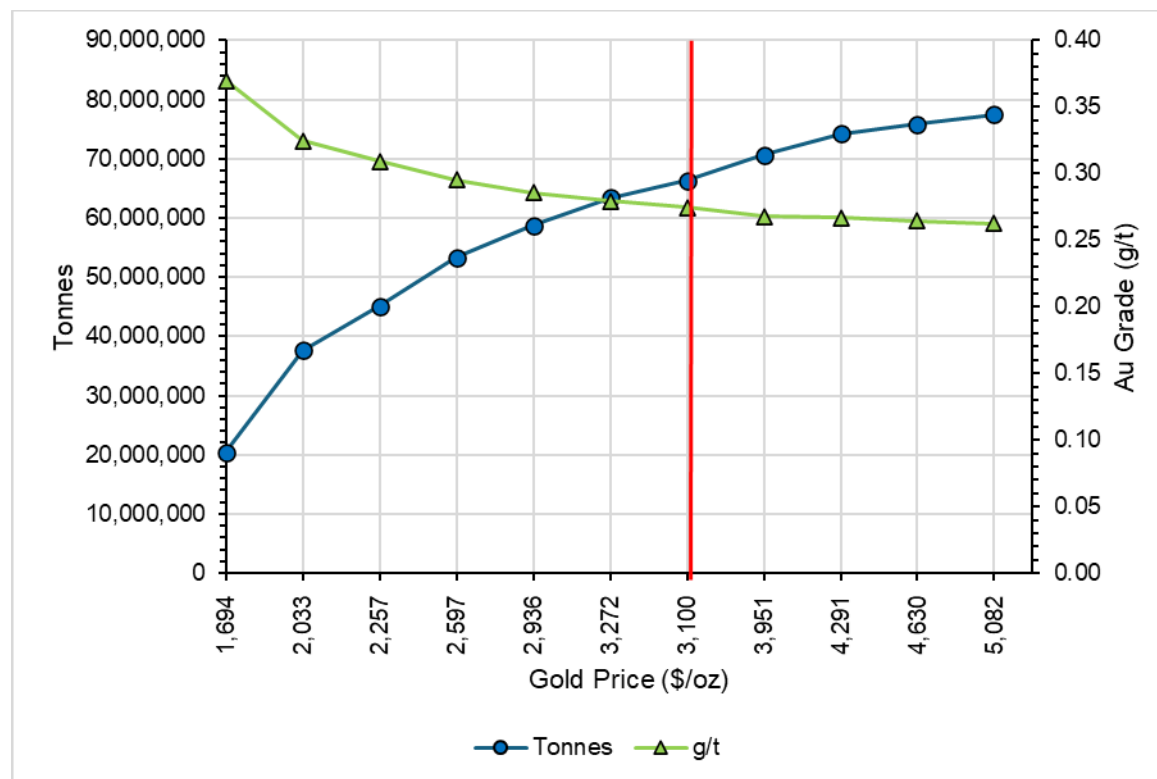
Table 11-17: Open Pit Grade vs Tonnage for Measured + Indicated Resources (Oxide/Mixed Pit Constrained)

Gold Price (\$/oz)	RF	Total Rock (t)	Resource M+I (t)	Strip Ratio (W:O)	Au Grade (g/t)	Ag Grade (g/t)	Au Rec (%)	Ag Rec (%)
1,694	0.48	35,732,409	20,468,964	0.75	0.37	4.49	74.99	16.72
2,033	0.58	68,197,241	37,612,499	0.81	0.32	4.16	74.61	17.56
2,257	0.65	81,659,853	45,065,866	0.81	0.31	4.07	74.55	17.67
2,597	0.74	99,200,686	53,323,671	0.86	0.30	4.02	74.50	17.73
2,936	0.84	110,812,588	58,689,771	0.89	0.29	3.93	74.54	17.62
3,272	0.94	124,512,625	63,344,842	0.97	0.28	3.84	74.57	17.58
3,100	1.00	132,050,829	66,288,945	0.99	0.27	3.79	74.56	17.53
3,951	1.13	144,294,460	70,633,066	1.04	0.27	3.71	74.50	17.54
4,291	1.23	165,570,401	74,237,792	1.23	0.27	3.63	74.42	17.43
4,630	1.32	171,018,579	75,830,152	1.26	0.26	3.60	74.40	17.41
5,082	1.45	177,363,755	77,429,268	1.29	0.26	3.56	74.38	17.39

Notes:
RF revenue factor



Figure 11-12: Open Pit Grade Tonnage Curve for Measured + Indicated Mineral Resources



11.15 Comparison with Previous Estimate

The Mineral Resource estimate prepared by SLR (2026) was compared with the RESPEC (2023) Mineral Resource estimate to assess changes in tonnage, grade, contained metal, classification, and the assumptions supporting the determination of RPEE.

The 2026 SLR estimate reports increases in Mineral Resources across all classification categories relative to the 2023 RESPEC estimate. Measured Mineral Resources increased from 4.9 Mt at 0.537 g/t Au and 3.615 g/t Ag to 5.5 Mt at 0.492 g/t Au and 3.487 g/t Ag, representing a modest increase in tonnage with slightly lower grades. Indicated Mineral Resources increased from 158.3 Mt at 0.356 g/t Au and 4.059 g/t Ag to 179.2 Mt at 0.330 g/t Au and 3.842 g/t Ag, an increase of approximately 13% in tonnage with broadly comparable grades. Inferred Mineral Resources increased from 119.9 Mt at 0.315 g/t Au and 2.454 g/t Ag to 238.0 Mt at 0.301 g/t Au and 3.403 g/t Ag, nearly doubling the reported tonnage.

The increase in Inferred Mineral Resources is primarily attributable to the inclusion of additional surface Mineral Resources, including waste rock dumps, heap leach materials, and TSF materials totaling 89.7 Mt, together with expanded pit-constrained oxide/mixed and sulfide Mineral Resources. More broadly, the changes reflect updated geological and block models, enhanced database validation, revised estimation parameters, and updated economic assumptions, including a long-term gold price of US\$3,100/oz and optimized pit shells and cut-off grades based on current mining, processing, and metallurgical recovery assumptions.

Mineral Resources are not Mineral Reserves and do not have demonstrated economic viability.



11.15.1 In Situ Mineral Resources (Pit-Constrained)

For in situ mineralization, excluding surface materials, the 2026 estimate reports Measured Mineral Resources of 5.5 Mt at 0.492 g/t Au, Indicated Mineral Resources of 179.2 Mt at 0.330 g/t Au, and combined Measured and Indicated Mineral Resources of 184.7 Mt at 0.335 g/t Au, compared with 163.2 Mt at 0.361 g/t Au reported by RESPEC (2023). Inferred in situ Mineral Resources total 148.4 Mt at 0.285 g/t Au, compared with 119.9 Mt at 0.315 g/t Au in the previous estimate.

These results represent a moderate increase in tonnage of approximately 13% for Measured and Indicated Mineral Resources and approximately 24% for Inferred Mineral Resources, with a corresponding decrease in average gold grade. The changes are attributable to updated geological interpretations, revised domain wireframes, incorporation of additional drilling and improved database validation, and expansion of optimized pit shells under higher metal price assumptions, which support the inclusion of additional marginal material. Contained gold remains broadly consistent with the previous estimate, indicating no evidence of material global estimation bias

11.15.2 Surface Materials (Dumps, Heap Leach, TSF)

A significant difference between the estimates is the treatment of surface materials, which are reported entirely as Inferred Mineral Resources in the 2026 estimate. SLR (2026) reports 89.7 Mt at 0.327 g/t Au and 4.738 g/t Ag, containing approximately 942 koz Au and 13.7 Moz Ag, comprising waste rock dumps, heap leach pads, and TSF materials.

In contrast, in 2023 15.8 Mt of Inferred dump material was reported and heap leach pad and TSF inventories were not separately estimated. The expanded surface Mineral Resource inventory in the 2026 estimate reflects the incorporation of additional datasets and operational inventories, improved delineation and classification of anthropogenic deposits, and the separation of material types to support appropriate processing and metallurgical recovery assumptions. The higher long-term gold price assumption of US\$3,100/oz also supports lower cut-off grades and demonstrates reasonable prospects for eventual economic extraction for additional lower-grade material.

11.15.3 Metallurgical Recovery Assumptions

Metallurgical recovery assumptions differ materially:

- RESPEC (2023): Generalized recoveries by material type, including high silver recoveries for sulfide material (up to 70%)
- SLR (2026): Process- and material-specific recoveries applied at a detailed domain level, including:
 - o Variable gold recoveries (generally approximately 63.7% to 85.0% basis for pit optimization inputs)
 - o Zero silver recovery assigned to sulfide material
 - o Distinct recovery assumptions for dumps, heap leach, and TSF materials reflecting leachable characteristics

These revisions represent a more conservative and operationally realistic basis for RPEE. While recovery assumptions do not affect reported grades or contained metal, they materially influence the derivation of the cut-off grade and the economic evaluation.



11.15.4 Classification

The distribution of Mineral Resources by classification remains broadly consistent. The 2026 estimate reports modest increases in Measured and Indicated tonnage, reflecting:

- Improved database validation and reconciliation;
- Refinement of geological domains and estimation controls; and
- Incorporation of additional drilling and updated interpretations.

No material changes to classification methodology or confidence criteria are identified.

11.15.5 Cut-off Grades

Cut-off grades in the 2026 estimate range from 0.074 g/t to 0.217 g/t Au, depending on material type and location, and are constrained by optimized pit shells developed using updated economic assumptions.

The primary differentiator relative to the 2023 estimate is the increase in assumed gold price of US\$1,800/oz to US\$3,100/oz, which has the following impacts:

- Lowers economic cut-off grades
- Expands pit limits
- Increases total tonnage reported
- Incorporates additional lower-grade material

The overall reporting framework remains consistent, but the economic basis for RPEE is materially more favorable in the 2026 estimate.

11.15.6 QP Opinion

In the opinion of the QP, the 2026 Mineral Resource estimate represents a reasonable, transparent, and defensible update to the 2023 estimate. The increase in tonnage and contained metal is primarily attributable to the following:

- Inclusion and improved delineation of surface materials
- Expansion of in situ mineralization under revised economic assumptions
- Higher gold price assumptions supporting lower cut-off grades and expanded pit shells

The reduction in average grade is consistent with the inclusion of marginal material and does not indicate estimation bias. Metallurgical recovery assumptions have been revised to a more conservative and operationally supportable basis consistent with S-K 1300 requirements.

11.16 Mineral Resource Reporting

Table 11-18 presents a detailed breakdown of the Mineral Resource estimate by classification category and area, in accordance with the reporting requirements of S-K 1300. The QP has reviewed and accepted the application of relevant modifying factors, including the results of open pit optimization, as described in Section 11.11. These constraints define the spatial volumes within which the Mineral Resources are considered to have RPEE and may therefore be reported in accordance with S-K 1300.



Table 11-18: Detailed Summary of Mineral Resources by Area – April 29, 2026

Category	Area	Tonnage (000 t)	Grade (g/t Au)	Grade (g/t Ag)	Contained Metal (000 oz Au)	Contained Metal (000 oz Ag)	Metallurgical Au Recovery (%)	Metallurgical Ag Recovery (%)
Measured								
Oxide/Mixed Pit	Facilities/Office Mixed	1,148	0.327	3.194	12.1	117.9	71.3%	22.3%
	Facilities/Office Oxide	560	0.264	2.543	4.8	45.8	83.9%	8.1%
	Sleeper Mixed	220	0.234	4.031	1.7	28.5	70.0%	15.0%
	Sleeper Oxide	76	0.177	0.957	0.4	2.3	84.5%	9.9%
	West Wood Mixed						65.0%	10.0%
	West Wood Oxide						76.5%	9.0%
	Oxide/Mixed Pit (non-sulfides)	2,004	0.293	3.019	18.9	194.5	75.2%	17.1%
	Sulfide	24	0.261	3.843	0.2	2.9	66.5%	0.0%
	Facilities/Office Sulfide	154	0.325	4.378	1.6	21.7	71.2%	0.0%
	Oxide/Mixed Pit (sulfides)	178	0.316	4.307	1.8	24.6	70.6%	0.0%
	Subtotal Measured Oxide/Mixed Pit	2,182	0.295	3.124	20.7	219.2	74.8%	15.7%
Sulfide Pit	Sulfide	340	0.409	2.405	4.5	26.3	66.5%	0.0%
	West Wood Sulfide	928	1.206	4.826	36.0	144.0	64.2%	0.0%
	Facilities/Office Sulfide	1,899	0.372	3.291	22.7	201.0	71.2%	0.0%
	Facilities/Office Mixed	21	0.354	2.500	0.2	1.7	71.3%	22.3%
	Facilities/Office Oxide						83.9%	8.1%
	Sleeper Mixed	7	0.285	0.870	0.1	0.2	70.0%	15.0%
	Sleeper Oxide					22.0	84.5%	9.9%
	West Wood Mixed	77	0.764	8.881	1.9	5.5	65.0%	10.0%
	West Wood Oxide	74	0.612	2.325	1.5		76.5%	9.0%
	Subtotal Measured Sulfide Pit	3,347	0.621	3.724	66.8	400.7	68.8%	0.6%
Total Measured		5,528	0.492	3.487	87.5	619.9	71.2%	6.5%



Category	Area	Tonnage (000 t)	Grade (g/t Au)	Grade (g/t Ag)	Contained Metal (000 oz Au)	Contained Metal (000 oz Ag)	Metallurgical Au Recovery (%)	Metallurgical Ag Recovery (%)
Indicated								
Oxide/Mixed Pit	Facilities/Office Mixed	41,658	0.275	4.373	368.5	5,856.6	71.3%	22.3%
	Facilities/Office Oxide	15,030	0.226	2.644	109.3	1,277.7	83.9%	8.1%
	Sleeper Mixed	16,910	0.260	2.981	141.5	1,620.7	70.0%	15.0%
	Sleeper Oxide	4,300	0.245	2.123	33.9	293.5	84.5%	9.9%
	West Wood Mixed						65.0%	10.0%
	West Wood Oxide						76.5%	9.0%
	Oxide/Mixed Pit (non-sulfides)	77,899	0.261	3.613	653	9,049	74.2%	17.3%
	Sulfide	8,618	0.360	4.996	99.8	1,384.2	66.5%	0.0%
	Facilities/Office Sulfide	7,323	0.290	4.861	68.2	1,144.5	71.2%	0.0%
	Oxide/Mixed Pit (sulfides)	15,941	0.328	4.934	168.0	2,528.7	68.7%	0.0%
	Subtotal Indicated Oxide/Mixed Pit	93,840	0.272	3.837	821.2	11,577.3	73.2%	14.4%
Sulfide Pit	Sulfide	56,544	0.382	4.245	694.2	7,717.5	66.5%	0.0%
	West Wood Sulfide	8,286	0.709	2.342	188.9	624.0	64.2%	0.0%
	Facilities/Office Sulfide	16,184	0.302	3.691	157.0	1,920.5	71.2%	0.0%
	Facilities/Office Mixed	1,556	0.218	2.669	10.9	133.5	71.3%	22.3%
	Facilities/Office Oxide	83	0.186	2.224	0.5	6.0	83.9%	8.1%
	Sleeper Mixed	1,344	0.248	1.948	10.7	84.1	70.0%	15.0%
	Sleeper Oxide	83	0.187	0.500	0.5	1.3	84.5%	9.9%
	West Wood Mixed	757	0.374	2.108	9.1	51.3	65.0%	10.0%
	West Wood Oxide	499	0.413	1.219	6.6	19.6	76.5%	9.0%
	Subtotal Indicated Sulfide Pit	85,336	0.393	3.848	1,078.5	10,557.9	67.4%	0.8%
Total Indicated		179,176	0.330	3.842	1,899.7	22,135.2	70.5%	7.9%



Category	Area	Tonnage (000 t)	Grade (g/t Au)	Grade (g/t Ag)	Contained Metal (000 oz Au)	Contained Metal (000 oz Ag)	Metallurgical Au Recovery (%)	Metallurgical Ag Recovery (%)
Measured + Indicated								
Oxide/Mixed Pit	Facilities/Office Mixed	42,806	0.277	4.341	380.5	5,974.5	71.3%	22.3%
	Facilities/Office Oxide	15,590	0.228	2.640	114.1	1,323.5	83.9%	8.1%
	Sleeper Mixed	17,130	0.260	2.995	143.2	1,649.3	70.0%	15.0%
	Sleeper Oxide	4,376	0.244	2.103	34.4	295.9	84.5%	9.9%
	West Wood Mixed	0	0.000	0.000	0.0	0.0	65.0%	10.0%
	West Wood Oxide	0	0.000	0.000	0.0	0.0	76.5%	9.0%
	Oxide/Mixed Pit (non-sulfides)	79,903	0.262	3.598	672	9,243	74.2%	17.3%
	Sulfide	8,642	0.360	4.993	100.0	1,387.2	66.5%	0.0%
	Facilities/Office Sulfide	7,477	0.290	4.851	69.8	1,166.2	71.2%	0.0%
	Oxide/Mixed Pit (sulfides)	16,119	0.328	4.927	169.8	2,553.4	68.7%	0.0%
	Subtotal Measured + Indicated Oxide/Mixed Pit	96,022	0.273	3.821	841.9	11,796.5	73.3%	14.4%
Sulfide Pit	Sulfide	56,884	0.382	4.234	698.7	7,743.8	66.5%	0.0%
	West Wood Sulfide	9,214	0.759	2.592	224.9	768.0	64.20%	0.00%
	Facilities/Office Sulfide	18,084	0.309	3.649	179.8	2,121.5	71.2%	0.0%
	Facilities/Office Mixed	1,577	0.220	2.667	11.2	135.2	71.3%	22.3%
	Facilities/Office Oxide	83	0.186	2.224	0.5	6.0	83.9%	8.1%
	Sleeper Mixed	1,350	0.248	1.942	10.8	84.3	70.0%	15.0%
	Sleeper Oxide	83	0.187	8.727	0.5	23.4	84.5%	9.9%
	West Wood Mixed	834	0.410	2.119	11.0	56.8	65.0%	10.0%
	West Wood Oxide	573	0.439	1.062	8.1	19.6	76.5%	9.0%
	Subtotal Measured + Indicated Sulfide Pit	88,683	0.402	3.843	1,145.3	10,958.6	67.5%	0.8%
Total Measured + Indicated		184,704	0.335	3.832	1,987.2	22,755.0	70.5%	7.9%



Category	Area	Tonnage (000 t)	Grade (g/t Au)	Grade (g/t Ag)	Contained Metal (000 oz Au)	Contained Metal (000 oz Ag)	Metallurgical Au Recovery (%)	Metallurgical Ag Recovery (%)
Inferred								
Surface	North Dump	23,747	0.364	2.584	277.7	1,972.8	79.0%	40.5%
	South Dump	12,667	0.182	1.612	74.2	656.7	69.8%	43.9%
	West Dump	10,478	0.203	0.883	68.5	297.4	81.4%	54.6%
	Subtotal Inferred Dumps	46,893	0.279	1.941	420.3	2,926.9	77.1%	44.6%
	Heap Leach Pads	31,600	0.301	8.363	306.3	8,496.9	40.0%	0.0%
	TSF	11,165	0.599	6.221	215.2	2,233.2	50.1%	0.0%
	Subtotal Inferred Surface	89,658	0.327	4.738	941.8	13,656.9	60.6%	23.3%
Oxide/Mixed Pit	Facilities/Office Mixed	12,668	0.251	3.233	102.1	1,316.9	71.3%	22.3%
	Facilities/Office Oxide	6,461	0.198	1.800	41.1	373.9	83.9%	8.1%
	Sleeper Mixed	14,851	0.232	2.884	110.6	1,377.2	70.0%	15.0%
	Sleeper Oxide	14,661	0.240	1.403	113.0	661.2	84.5%	9.9%
	West Wood Mixed						65.0%	10.0%
	West Wood Oxide	15	0.136	0.272	0.1	0.1	76.5%	9.0%
	Oxide/Mixed Pit (non-sulfides)	48,656	0.235	2.384	367	3,729	76.6%	14.4%
	Sulfide	2,485	0.302	3.288	24.1	262.6	66.5%	0.0%
	Facilities/Office Sulfide	2,475	0.271	3.800	21.6	302.4	71.2%	0.0%
	Oxide/Mixed Pit (sulfides)	4,960	0.286	3.543	45.7	565.0	68.9%	0.0%
	Subtotal Inferred Oxide/Mix Pit	53,616	0.239	2.491	412.6	4,294.4	75.8%	13.1%
Sulfide Pit	Sulfide	69,108	0.324	2.661	718.8	5,913.4	66.5%	0.0%
	West Wood Sulfide	1,242	0.369	0.987	14.7	39.4	64.2%	0.0%
	Facilities/Office Sulfide	14,602	0.316	3.848	148.3	1,806.5	71.2%	0.0%
	Facilities/Office Mixed	1,728	0.217	2.208	12.1	122.7	71.3%	22.3%
	Facilities/Office Oxide	225	0.190	1.443	1.4	10.5	83.9%	8.1%



Category	Area	Tonnage (000 t)	Grade (g/t Au)	Grade (g/t Ag)	Contained Metal (000 oz Au)	Contained Metal (000 oz Ag)	Metallurgical Au Recovery (%)	Metallurgical Ag Recovery (%)
	Sleeper Mixed	3,348	0.237	1.036	25.5	111.5	70.0%	15.0%
	Sleeper Oxide	2,152	0.183	0.700	12.6	48.4	84.5%	9.9%
	West Wood Mixed	932	0.204	0.616	6.1	18.4	65.0%	10.0%
	West Wood Oxide	1,424	0.193	0.534	8.8	24.4	76.5%	9.0%
	Subtotal Inferred Sulfide Pit	94,761	0.311	2.657	948.3	8,095.3	68.0%	1.4%
Total Inferred		238,035	0.301	3.403	2,302.7	26,046.7	67.0%	12.3%

Notes:

1. The definitions for Mineral Resources in S-K 1300 were followed for Mineral Resources
2. The Mineral Resource estimate is reported on a 100% ownership basis.
3. The point of reference for the Mineral Resource is before the crusher (in situ).
4. Open Pit Mineral Resources are reported at a cut-off grade ranging from 0.074 g/t to 0.217 g/t Au, depending on area and constrained by a preliminary optimized pit shell with a pit slope angle of 45° for rock and 22° for alluvium and a bench height of 10 m.
5. The optimized pit shell and cut-off grades were generated by assuming metallurgical gold recovery ranging from 63.7% to 85.0% and silver recoveries ranging from 0.0% to 54.6%, standard treatment and refining charges, mining costs of US\$2.40/t moved for open pit, processing costs of \$5.51/t oxide/mixed and \$10.44 sulfide processed, and general and administrative costs of \$0.46/t processed
6. Minimal mining width was 60 m for oxide/mixed material and 20 m for sulfide material
7. Mineral Resources are estimated using a long-term gold price of US\$3,100 per ounce
8. Bulk density ranges from 1.5 t/m³ in the tailings storage area to 2.7 t/m³ for in situ material
9. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.
10. Numbers may not add due to rounding.



12.0 Mineral Reserve Estimates

There are no Mineral Reserves defined at the Sleeper Gold Mine at this time.



13.0 Mining Methods

The proposed Base Case mining operations include a conventional open pit truck-shovel operation and rehandling of mineralized material from three existing waste rock dumps. The in situ mining inventory is approximately 128.5 Mt and the rehandled existing waste dump rock material totals approximately 46.9 Mt. The operation is designed to deliver approximately 30,000 tpd of mineralized material to the processing facilities, with a LOM open pit average strip ratio of 1.9:1 (waste tonne: process feed tonne).

In the Alternative Case, only in situ material is mined and processed; no material from the existing waste rock dumps is reclaimed for processing.

13.1 Geotechnical Studies

The current pit slope design is based on preliminary geotechnical assumptions appropriate for an Initial Assessment level of study. In competent bedrock, an overall slope angle of approximately 45° has been applied, as observed in the existing pit walls, reflecting assumed favorable rock mass conditions and stable bench-scale performance. In contrast, alluvial materials are assigned a significantly flatter overall slope angle of approximately 22°, which is also observed in the current pit slopes and is consistent with reduced material strength, potential for raveling, and sensitivity to groundwater and weathering.

Bench-scale geometry is based on 10 m bench heights, which are compatible with production drilling, loading equipment reach, and operational efficiency. In competent rock, bench face angles of 80° and berm widths of approximately 8.24 m have been assumed, while alluvial zones utilize flatter bench face angles of approximately 34° with wider berms of approximately 9.93 m, as shown in Figure 13-3. These parameters are considered reasonable for conceptual planning but will require confirmation through detailed geotechnical investigation, including drilling, laboratory testing, structural analysis, and slope stability modeling in future study phases.

Groundwater conditions have not been explicitly incorporated into slope design at this stage; however, given the pit's depth (approximately 230 m), dewatering and depressurization will be required and will influence the final slope configurations. The current design criteria are considered appropriate for the Initial Assessment but are subject to refinement.

Table 13-1: Geotechnical Design Criteria

Parameter	Competent Rock	Alluvium
Bench height (m)	10	10
Bench face angle (degrees)	80	34
Overall slope angle (degrees)	45	22
Bench berm width (m)	8.24	9.93

13.2 Mine Design

The current pit lake water elevation is 1,255 masl as presented in Figure 13-1. The conceptual open pit design has approximate plan dimensions of 2,650 m (north-south) by 1,860 m (east-west) and a maximum depth of approximately 230 m, with a pit bottom elevation of approximately 1,080 masl, as shown in Figure 13-2. Primary pit access is provided via a south-



side waste haul exit at approximately 1,270 masl and a west-side crusher exit at approximately 1,265 masl, allowing for separation of mineralized material and waste haulage where practical.

The pit design was developed based on pit optimization results at a revenue factor of 1.0 derived using 20 m × 20 m × 20 m blocks. Slope assumptions applied during the optimization were assumed at an overall slope angle of 45° for fresh rock and 22° for alluvial material. Pit Optimization economic parameters and recoveries are provided in Table 11-11, and the mining cost of \$2.40 per tonne mined.



Figure 13-1: Initial Mine Topography

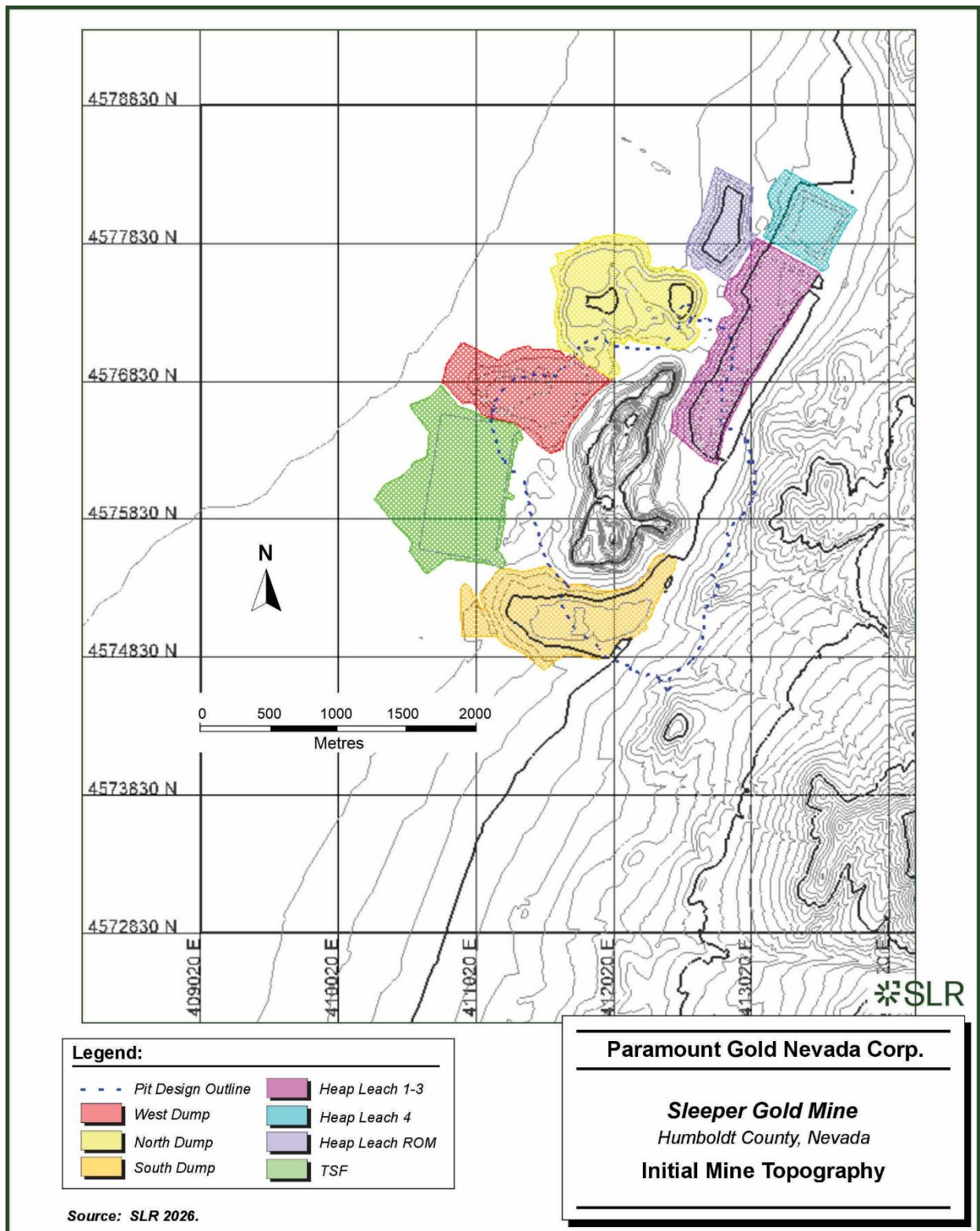
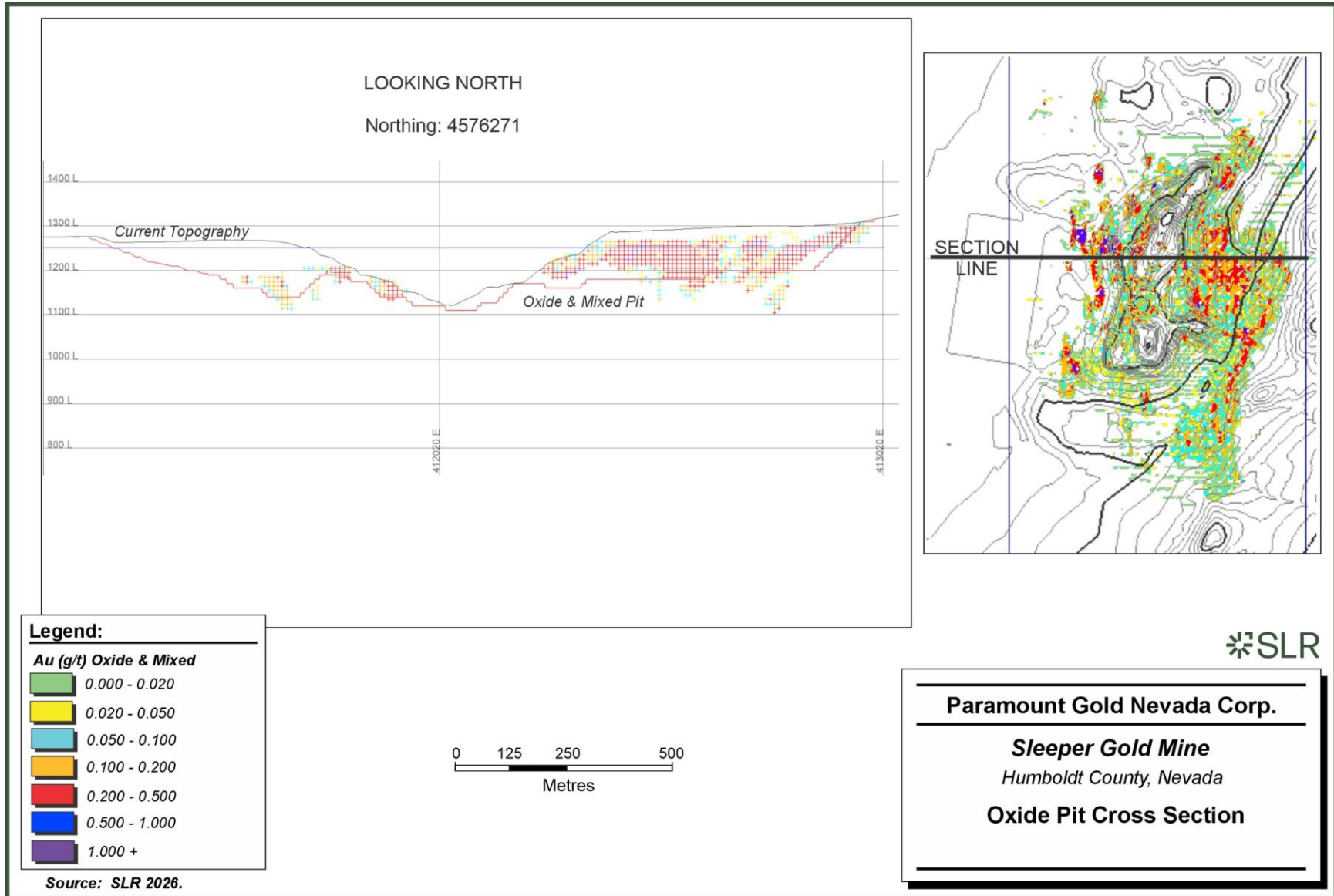


Figure 13-2: Oxide Pit Cross Section 4,576,271 N



Mining will be conducted on 10 m benches with a minimum mining width of 60 m, providing adequate working space for drilling, loading, haulage, and safe operation of large production equipment. Haul road design is based on 150 t class haul trucks, with main ramps constructed at approximately 35 m width and 10% gradient. In the bottom two benches of the pit, where space is constrained, single-lane haulage (supported by traffic management controls and localized passing areas) is proposed.

Ex-pit haul distances to the crusher and waste rock storage facilities are estimated to range from approximately 0.8 km to 2.4 km (0.5 miles to 1.5 miles). Haul cycle times are based on typical industry operating speeds for 150 t haul trucks, accounting for loaded and unloaded travel, ramp grades, and road conditions consistent with a well-maintained Nevada open pit operation.

Material movement assumptions include a swell factor of 35% and a loose density of 1.7 t/m³, resulting in an approximate loose volume of 88 m³ per truck load, equivalent to approximately 65 bank cubic meters (bcm) per load. The SLR QP considers these values to be appropriate for preliminary equipment productivity and haulage calculations.

Operational assumptions include 24-hour continuous operation, utilizing two 12-hour shifts per day across four rotating crews. Effective operating time is assumed to be 53 minutes per hour, reflecting delays for operational inefficiencies, shift changes, and minor interruptions. Equipment performance is further adjusted to 90% mechanical availability utilization, consistent with contractor-operated mining fleets.

Table 13-2: Mine Design Parameters

Parameter	Value
Pit dimensions (N-S)	2,650 m
Pit dimensions (E-W)	1,860 m
Pit depth	230 m
Pit bottom elevation	1,080 masl
Waste exit elevation (south)	1,270 masl
Crusher exit elevation (west)	1,265 masl
Bench height	10 m
Minimum mining width	60 m
Ramp width	35 m
Ramp grade	10%
Bottom benches	Single-lane haulage
Ex-pit haul distance	0.8 km to 2.4 km (0.5–1.5 miles)
Swell Percent	35%
Swell Factor	0.7407
Loose density	1.7 t/m ³



Parameter	Value
Operating schedule	24 hr/day, 2 shifts, 4 crews
Effective time	53 min/hr
Utilization	90% of availability

13.3 Waste Rock Storage Facilities Design

Waste rock generated from open pit mining is planned to be placed in conventional end-dumped waste rock storage facilities (WRSF) located adjacent to the pit. The WRSFs are conceptualized to a maximum height of approximately 150 m and developed in 30 m lifts, consistent with typical large-scale open pit operations in Nevada. Waste material is assumed to have an in situ density of approximately 2.3 t/m³, a swell factor of 35%, and a corresponding loose density of approximately 1.70 t/m³, which forms the basis for volumetric and capacity estimates.

During active operations, waste will be placed by end-dumping over the advancing dump crest in 30 m lift, with the working face developing at an approximate angle of repose of 35°, equivalent to about 1.5H:1V. This geometry reflects the typical behavior of coarse, fragmented rock under gravity placement conditions. For long-term stability and closure, the external slopes of the waste rock dumps are assumed to be regraded to a final 3H:1V slope.

The assumed geometry is appropriate for an IA; however, detailed WRSF design, including slope stability, drainage control, compaction behavior, and closure landform development, will require further geotechnical and hydrological evaluation in future study phases.

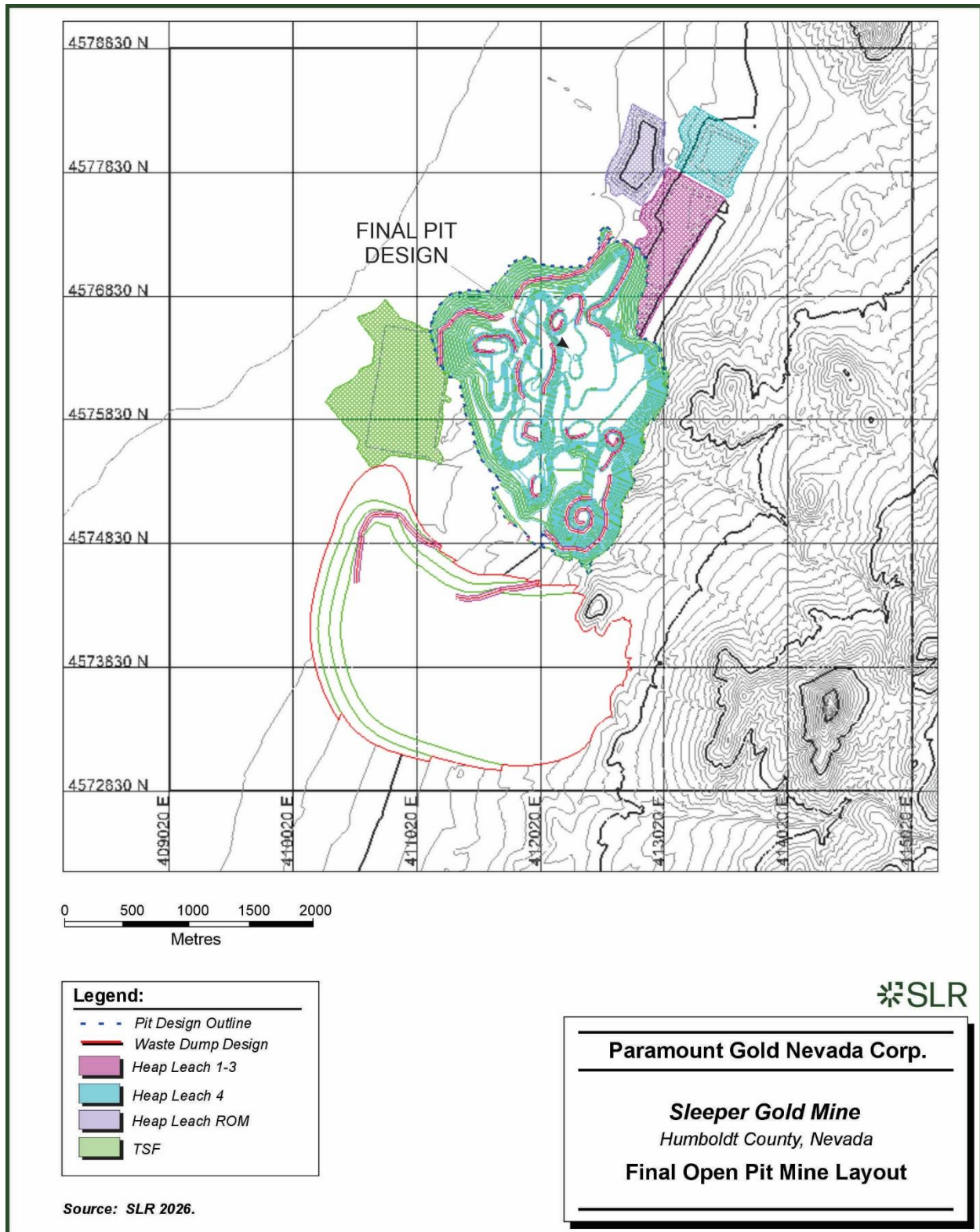
Table 13-3 summarizes the WRSF design parameters. Figure 13-3 presents the Final Pit Design and Waste Rock Storage Facility Design based on the parameters summarized in this section.

Table 13-3: WRSF Design Parameters

Parameter	Value
Maximum dump height	104 m
Lift height	30 m
Number of lifts	3.5
In situ density	2.3 t/m ³
Swell Percent	35%
Loose density	1.70 t/m ³
Active dump slope	35° (~1.5H:1V)
Final reclaimed slope	3H:1V



Figure 13-3: Final Pit Design and Waste Storage Facility Design



13.4 Mining Method

At the stated production rate, the operation will mine approximately 66,300 tpd of waste, resulting in a total material movement of approximately 95,890 tpd. This equates to approximately 10.8 Mtpa of mineralized material, 24.2 Mtpa of waste, and 35.0 Mtpa of total pit movement, assuming continuous operations.

Primary loading is performed using CAT 6060-class hydraulic shovels equipped with 18 m³ to 22 m³ buckets, supplemented by large wheel loaders for operational flexibility, rehandle, and backup loading. The loading configuration is designed around a 4-pass match with 150 t haul trucks, which provides an efficient balance between productivity and truck utilization.

Production drilling is carried out using single-pass diesel rotary drills, such as Pit Viper-class drills, capable of drilling the full 10 m bench height in a single pass. This approach improves drilling efficiency, reduces hole deviation, and supports consistent blast performance. Drill and blast parameters will be refined in future phases based on rock mass characteristics and fragmentation requirements.

Production blasting is assumed to be conducted using conventional rotary blasthole drilling on 10 m bench heights. Blastholes are designed at a nominal diameter of 229 mm and drilled on a 6.5 m burden by 7.5 m spacing pattern, which is considered appropriate for the volcanic and locally silicified rock units present at the Sleeper deposit.

Each blasthole is drilled to include approximately 1.0 m of subdrill to ensure full breakage at the bench floor. Stemming length is assumed to be 4.0 m, resulting in an effective charged length of approximately 7.0 m per hole.

The average in situ rock density is assumed to be 2.3 t/m³, yielding approximately 1,120 t of rock broken per blasthole under the selected pattern geometry.

Given the anticipated groundwater conditions and the requirement for ongoing pit dewatering, wet blasthole conditions are expected to be common. Accordingly, blasting is assumed to utilize bulk emulsion or heavy ANFO–emulsion blends rather than dry ANFO. An average explosive density of approximately 1.15 t/m³ is assumed, resulting in a charge concentration of approximately 47 kg of explosive per metre of loaded hole. This corresponds to approximately 330 kg of explosive per blasthole. Blasting practices are expected to be optimized during operations through field trials to achieve the desired fragmentation for efficient loading, hauling, and downstream crushing or heap leach performance.

Based on these parameters, a powder factor of approximately 0.28 kg of explosive per tonne of rock blasted has been adopted for the mine plan. This value is considered appropriate for preliminary design and cost estimation and is consistent with similar open-pit gold operations in northern Nevada operating under comparable ground and groundwater conditions. Drilling and blasting parameters are summarized in Table 13-4.

Table 13-4: Drilling and Blasting Parameters

Parameter	Unit	Value
Bench height	m	10
Hole diameter	mm	229
Burden	m	6.5
Spacing	m	7.5



Parameter	Unit	Value
Pattern	m × m	6.5 × 7.5
Subdrill	m	1.0
Total hole depth	m	11.0
Stemming length	m	4.0
Charged length	m	7.0
Explosive type	—	Bulk emulsion / heavy ANFO–emulsion
Explosive density	t/m ³	1.15
Explosive per metre	kg/m	47
Explosive per hole	kg	330
Rock density	t/m ³	2.3
Rock broken per hole	t	1,120
Powder factor	kg/t	0.28
Notes:		
<ol style="list-style-type: none"> Parameters reflect production blasting on 10 m benches with 229 mm-diameter blastholes. The 6.5 m × 7.5 m pattern is considered appropriate for the volcanic and locally silicified rock units at Sleeper. Wet blasthole conditions are expected to be common due to groundwater inflows; therefore, bulk emulsion or heavy ANFO–emulsion blends are assumed rather than dry ANFO. The powder factor is derived from the geometry, explosive density, and charge length and is appropriate for preliminary mine planning and cost estimation. 		

Haulage is performed using a fleet of 150 t class rigid frame haul trucks, which transport mineralized material to the crusher and waste to designated storage areas. Based on nominal payload assumptions, the approximate required truckloads per day are listed:

- 200 mineralized material truckloads
- 442 waste truckloads
- 642 total loaded truckloads

Additional haulage demand will be generated by the reclaim of the existing waste rock dump material, depending on the production schedule adopted.

Reclaim of waste rock dumps will be conducted using loaders and/or hydraulic shovels, with material excavated in controlled lifts and hauled directly to the processing facilities. This activity is expected to require limited or no drilling and blasting, depending on material consolidation, and represents a conventional rehandle operation.

Mine support activities include road maintenance using CAT 16H motor graders, along with track dozers, water trucks, and service equipment. Proper road maintenance is critical to maintaining haul truck productivity, extending tire life, minimizing rolling resistance, and ensuring safe operating conditions.

Overall, the selected mining method, comprised of a 10 m bench open pit mining using 150 t haul trucks, CAT 6060-class hydraulic shovels, Pit Viper-class drills, and CAT 16H graders, combined with rehandle of existing waste rock dumps, is considered appropriate for the scale and nature of the Project and consistent with industry practice for Nevada heap leach



operations. A summary of the mining method and proposed equipment fleet is provided in Table 13-5.

Table 13-5: Mining Method and Equipment Summary

Category	Description
Mining method	Conventional open pit truck-shovel plus waste dump reclaim
Process rate	30,000 tpd mineralized material
Strip ratio (W:O)	1.9:1
Waste mined	66,300 tpd
Total movement	95,890 tpd
Haul trucks	150 t class
Hydraulic shovel	CAT 6060 class
Bucket size	18–22 m ³
Loading	4-pass
Drills	Single-pass diesel rotary (Pit Viper class)
Graders	CAT 16H
Waste dump reclaim	46.9 Mt
Truckloads (process feed)	approximately 200/day
Truckloads (waste)	approximately 442/day

13.5 Life of Mine Plan

Base Case production schedule starts by mining the existing waste rock dumps, followed by the in situ oxide and mixed Mineral Resources located around the previous open pit operation.

The total mineralized inventory processed in the Base Case LOM plan is 175.4 Mt at average grades of 0.26 g/t Au and 2.8 g/t Ag. Inferred Resources account for 54.5% of the Base Case production schedule.

Compared to the previous LOM plan (RESPEC 2023), the pit optimization resulted in additional material at lower average gold and silver grades being included in the LOM plan, due to the higher gold price and lower cut-off grades. Cut-off grades by material type, recoveries, and economic parameters used are presented in Table 11-11. Silver is considered a by-product, accounting for less than 4% of the Base Case cash flow on gross revenue average.

There are sufficient Existing Dump Mineral Resources to allow processing for five years, as presented in Table 13-6, totaling Oxide and Mixed Resources of 46.9 Mt at an average gold grade of 0.28 g/t.



Table 13-6: Process Feed from Existing Dumps to the Crusher

Units	Dumps	Grade		Contained		Recovery		Recovered	
	Oxide+ Mixed (Mt)	Gold (g/t)	Silver (g/t)	Gold (koz)	Silver (koz)	Gold (%)	Silver (%)	Gold (koz)	Silver (koz)
Year 1	7.3	0.27	2.2	63.8	510	79.0%	40.5%	50.4	207
Year 2	10.8	0.39	2.7	135.0	930	79.0%	40.5%	106.7	377
Year 3	10.8	0.36	2.1	123.6	724	80.1%	47.2%	99.1	342
Year 4	10.8	0.17	1.4	60.6	496	75.6%	49.2%	45.8	244
Year 5	7.2	0.16	1.2	37.6	268	69.8%	43.9%	26.3	118
Totals	46.9	0.28	1.9	420.6	2,929	78.0%	43.9%	328.2	1,287

Table 13-7 shows the In Situ Mineral Resources feeding the crusher starting in year five and continuing for approximately 12.5 years. The In Situ Oxide and Mixed material feed totals 128.5 Mt at an average gold grade of 0.25 g/t.

Table 13-7: Process Feed from Open Pit to the Crusher

Units	Pit	Grade		Contained		Recovery		Recovered	
	In Situ Oxide+Mixed (Mt)	Gold (g/t)	Silver (g/t)	Gold (koz)	Silver (koz)	Gold (%)	Silver (%)	Gold (koz)	Silver (koz)
Year 1									
Year 2									
Year 3									
Year 4									
Year 5	3.6	0.23	3.1	26.2	357	74.1%	32.1%	19.4	115
Year 6	10.8	0.22	4.2	76.8	1,473	76.7%	15.9%	59.0	235
Year 7	10.8	0.25	5.1	85.6	1,765	72.7%	20.5%	62.2	362
Year 8	10.8	0.24	4.8	84.1	1,670	74.7%	19.0%	62.8	317
Year 9	10.8	0.21	2.9	74.1	1,017	79.1%	11.4%	58.6	116
Year 10	10.8	0.20	3.4	68.2	1,180	72.7%	14.2%	49.5	167
Year 11	10.8	0.24	3.6	84.8	1,249	74.2%	15.1%	62.9	188
Year 12	10.8	0.27	2.4	95.3	818	75.0%	18.1%	71.5	148
Year 13	10.8	0.27	2.3	94.8	815	72.6%	20.6%	68.8	168
Year 14	10.8	0.27	3.1	95.5	1,065	71.9%	20.7%	68.6	220
Year 15	10.8	0.26	1.3	91.0	443	78.0%	14.3%	70.9	63
Year 16	10.8	0.29	1.2	99.9	421	77.4%	12.4%	77.4	52
Year 17	6.1	0.31	2.6	62.0	518	71.9%	14.3%	44.6	74
Totals	128.5	0.25	3.1	1,038.2	12,793	74.8%	17.4%	776.2	2,225

Table 13-8 includes all Oxide and Mixed Resources processed during the life of mine, totaling of 175.4 Mt at an average gold grade of 0.26 g/t, as summarized in Table 13-8.



Table 13-8: Mining Inventory Processed by Year

Units	Pit	Grade		Contained		Recovery		Recovered	
	Total Oxide+ Mixed (Mt)	Gold (g/t)	Silver (g/t)	Gold (koz)	Silver (koz)	Gold (%)	Silver (%)	Gold (koz)	Silver (koz)
Year 1	7.3	0.27	2.2	63.8	510.2	79.0%	40.5%	50.4	207
Year 2	10.8	0.39	2.7	135.0	930.4	79.0%	40.5%	106.7	377
Year 3	10.8	0.36	2.1	123.6	724.2	80.1%	47.2%	99.1	342
Year 4	10.8	0.17	1.4	60.6	495.8	75.6%	49.2%	45.8	244
Year 5	10.8	0.18	1.8	63.8	625.3	74.5%	32.2%	47.5	201
Year 6	10.8	0.22	4.2	76.8	1,472.5	76.7%	15.9%	59.0	235
Year 7	10.8	0.25	5.1	85.6	1,764.6	72.7%	20.5%	62.2	362
Year 8	10.8	0.24	4.8	84.1	1,670.4	74.7%	19.0%	62.8	317
Year 9	10.8	0.21	2.9	74.1	1,016.9	79.1%	11.4%	58.6	116
Year 10	10.8	0.20	3.4	68.2	1,180.4	72.7%	14.2%	49.5	167
Year 11	10.8	0.24	3.6	84.8	1,249.5	74.2%	15.1%	62.9	188
Year 12	10.8	0.27	2.4	95.3	818.3	75.0%	18.1%	71.5	148
Year 13	10.8	0.27	2.4	94.8	815.2	72.6%	20.6%	68.8	168
Year 14	10.8	0.27	3.1	95.5	1,065.1	71.9%	20.7%	68.6	220
Year 15	10.8	0.26	1.3	91.0	443.1	78.0%	14.3%	70.9	63
Year 16	10.8	0.29	1.2	99.9	421.2	77.4%	12.4%	77.4	52
Year 17	6.1	0.31	2.6	62.0	518.2	71.9%	14.3%	44.6	74
Totals	175.4	0.26	2.8	1,458.9	15,721.1	75.8%	22.1%	1,106.2	3,481

The LOM plan requires extracting waste along with the mineralized material from the open pit and existing dumps. Table 13-9 summarizes all open pit materials relevant to the Base Case operation cost estimates, excluding existing dump extraction.

Table 13-9: Base Case Open Pit Production Schedule

Units	Total Oxide + Mixed (Mt)	Gold Grade (g/t)	Silver Grade (g/t)	Total Waste Tonnage (Mt)	Total Material Tonnage (Mt)	Strip Ratio (W:O)	Resource Mining Rate (tpd)	Waste Mining Rate (tpd)	Total Mining Rate (tpd)
Year 1	-	-	-	-	-	-	-	-	-
Year 2	-	-	-	-	-	-	-	-	-
Year 3	-	-	-	-	-	-	-	-	-
Year 4	-	-	-	-	-	-	-	-	-
Year 5	3.6	0.23	3.1	13.2	16.8	3.7	9,927	36,155	45,946
Year 6	10.8	0.22	4.2	13.0	23.8	1.2	30,000	35,497	65,086



Units	Total Oxide + Mixed (Mt)	Gold Grade (g/t)	Silver Grade (g/t)	Total Waste Tonnage (Mt)	Total Material Tonnage (Mt)	Strip Ratio (W:O)	Resource Mining Rate (tpd)	Waste Mining Rate (tpd)	Total Mining Rate (tpd)
Year 7	10.8	0.25	5.1	10.3	21.1	1.0	30,000	28,303	57,892
Year 8	10.8	0.24	4.8	24.2	35.0	2.2	30,000	66,301	95,890
Year 9	10.8	0.21	2.9	24.2	35.0	2.2	30,000	66,31	95,890
Year 10	10.8	0.20	3.4	23.8	34.6	2.2	30,000	65,075	94,664
Year 11	10.8	0.24	3.6	19.3	30.1	1.8	30,000	52,931	82,520
Year 12	10.8	0.27	2.4	24.2	35.0	2.2	30,000	66,301	95,890
Year 13	10.8	0.27	2.3	24.2	35.0	2.2	30,000	66,301	95,890
Year 14	10.8	0.27	3.1	16.2	27.0	1.5	30,000	44,436	74,025
Year 15	10.8	0.26	1.3	24.2	35.0	2.2	30,000	66,301	95,890
Year 16	10.8	0.29	1.2	15.9	26.7	1.5	30,000	43,571	73,160
Year 17	6.1	0.31	2.6	9.4	15.6	1.5	17,069	25,778	42,612
Totals	128.5	0.25	3.1	242.1	370.6	1.9			

Note:
Resource mining rates are based on 360 days per year.
Waste and Total mining rates are based on 365 days per year

13.6 Contract Mining Discussion

Mining at the Project is planned to be executed by an experienced third-party mining contractor under a unit-rate contract. This approach has been selected based on the relatively small size of the Company and the desire to minimize initial capital expenditures associated with the purchase, commissioning, and maintenance of a mining fleet. By utilizing a contractor, the Project avoids significant upfront capital outlays and transfers a portion of the operational and maintenance risk to the contractor, while maintaining flexibility to scale operations as required.

13.6.1 Mining Rate and Production Basis

As previously noted, for the Base Case, operations will begin by mining the existing waste rock dumps at 30,000 tpd, followed by mining the in situ material, which will require additional equipment and personnel.

The mine plan contemplates a nominal processing rate of approximately 30,000 tpd of process feed, supported by a LOM strip ratio of approximately 1.9:1 (waste:process feed) when mining in situ material, resulting in a total material movement rate of approximately 95,890 tpd.

Mining activities will include drilling, blasting, loading, and hauling of both process feed and waste materials. Process feed will be transported to the primary crusher and/or ROM stockpiles for downstream processing, while waste material will be hauled to designated waste rock storage facilities.



13.6.2 Contract Structure and Unit Rates

The estimated cost of contract mining is US\$1.04 per banked cubic meter (bcm), equivalent to approximately US\$2.40 per tonne (based on assumed bulk densities).

The unit rate is expected to include all standard open pit mining activities, including drilling and blasting, loading, hauling, equipment operation, maintenance, supervision, and typical consumables required for production. The use of a unit-rate contract provides cost transparency and aligns contractor compensation directly with production volumes.

13.6.3 Out-of-Scope (“Forced Work”) Allowance

In addition to the base unit mining rate, an allowance has been included for out-of-scope or “forced work”, which encompasses activities not explicitly covered under the base mining contract. These may include, but are not limited to, the following:

- Road construction beyond normal maintenance requirements
- Sump excavation and water management support
- Rehandling of material outside planned sequences
- Additional dozer support or cleanup activities
- Standby time or operational inefficiencies outside contractor control
- Owner-directed miscellaneous work

Based on benchmarking and preliminary discussions, a monthly allowance of approximately US\$112,000 has been included for such activities. This represents approximately 10% of the estimated base mining cost and is considered appropriate for an IA level estimate.

13.6.4 Grade Control and Sampling

The contractor will be responsible for the collection of blasthole drill cuttings during production drilling operations. These samples will be used for grade control purposes and will be collected in accordance with procedures established by the Company to ensure representativity and data quality.

Blasthole sampling will support short-term ore control, including mineralized material/waste delineation and routing of material to the appropriate destinations (crusher, stockpile, or waste dump).

A separate contract will be established for dedicated grade control drilling, which will provide a higher-resolution definition of mineralization boundaries and support the conversion of Mineral Resources and reconciliation of production. This work is not included in the mining contractor’s scope or unit rate.

13.6.5 Operational Considerations

The contractor will be expected to supply and operate a fleet of appropriately sized equipment, likely including hydraulic excavators, front-end loaders, and haul trucks in the 150 t class, along with ancillary support equipment such as dozers, graders, water trucks, and service vehicles.

The contractor will be responsible for the following:

- Equipment supply, operation, and maintenance
- Provision of qualified labor and supervision



- Compliance with site safety, environmental, and operational standards
- Execution of the mine plan in accordance with Company specifications

Paramount will retain responsibility for mine planning, scheduling, grade control, and overall operational oversight to ensure that mining activities are conducted in accordance with the Project's technical and economic objectives.

13.6.6 Contract Mining Summary

The use of a contract mining strategy provides a capital-efficient and flexible approach to Project development. The selected unit rate and allowances are considered reasonable for an IA level study and are consistent with similar operations in the region. The inclusion of a defined allowance for out-of-scope work and separation of grade control drilling provides appropriate transparency and conservatism in the cost estimate.

13.7 Mine Infrastructure

The proposed mining operation is a conventional open pit mining operation designed to support a nominal process feed production rate of approximately 30,000 tpd, with an associated waste-to-process feed strip ratio of approximately 1.92:1, resulting in total material movement of approximately 95,890 tpd. The mine infrastructure has been conceptually designed to support continuous, year-round operations in a manner consistent with industry practice for open pit heap leach operations in northern Nevada.

13.7.1 Mine Access and Haul Roads

The open pit will be developed with a series of engineered haul roads and ramps designed to accommodate 150 t-class rear-dump haul trucks. Ramp widths are expected to be approximately 35 m for two-way traffic, including safety berms and drainage features, with maximum sustained grades of approximately 10%, consistent with standard open pit design criteria. Haul roads will be constructed using locally sourced waste rock and maintained by motor graders to ensure appropriate rolling resistance and safety. Internal pit access will be designed to provide flexibility for multiple working faces and phased pushbacks over the mine life.

13.7.2 Material Handling

Material handling will consist of conventional truck-and-shovel/loader operations, with process feed hauled from the pit to a primary crushing facility located adjacent to the heap leach pad. Process feed haul distances are expected to range from approximately 1.5 km to 4.5 km one-way, while waste material will be hauled to designated waste rock storage facilities located approximately 2.5 km from the pit exit. The primary crusher will reduce ROM material to a size suitable for heap leaching, after which the material may be conveyed or trucked to the leach pad for stacking. Agglomeration may be employed depending on final metallurgical test results.

13.7.3 Backfill

No backfilling of the open pit is currently planned during operations. Waste rock will be placed in external waste rock storage facilities designed to ensure geotechnical stability, drainage control, and long-term reclamation. Placement will be managed using track dozers and haul trucks, with lift heights and dump configurations consistent with industry practice. Partial backfilling of the pit may be considered at closure, depending on the final reclamation plan.



13.7.4 Dewatering

Mine dewatering is expected to be a significant component of the operation, with inflows estimated at approximately 53 m³/min (14,000 gpm). Dewatering will be achieved using a staged pumping system installed within the pit, consisting of submersible or vertical turbine pumps located in sumps and on intermediate benches. Water will be pumped to surface pipelines and conveyed to designated storage or discharge areas. Consistent with operational constraints, no electrical infrastructure will be installed within active mining areas beyond the dewatering pump installations. Excess water not required for processing will be discharged, subject to permitting, to rapid infiltration basin(s) or equivalent area located several kilometers from the pit. The dewatering system will be designed to maintain safe and dry working conditions, and it will include redundancy to ensure reliability.

13.7.5 Maintenance Facilities

The Project currently includes an existing four-bay truck shop located within the footprint of the planned ultimate pit and will therefore require relocation. A new maintenance facility will be constructed outside of the pit limits in a location suitable for long-term operations. The replacement facility is expected to include multiple service bays sized for 150-tonne haul trucks, overhead cranes, lubrication systems, tire handling equipment, and supporting infrastructure. The shop will be supported by adjacent maintenance yards, parts storage, and fueling facilities. Additional light-vehicle and support-equipment maintenance will be accommodated within the same complex or in dedicated auxiliary buildings.

13.7.6 Fuel Storage and Distribution

Diesel fuel storage and distribution facilities will be constructed on-site to support the mining fleet and auxiliary equipment. Fuel will be delivered by tanker truck and stored in above-ground tanks with appropriate containment. Mobile fueling units will be used for in-pit refueling of haul trucks and support equipment to minimize downtime. Refer to Table 13-13 for details on fuel storage arrangements.

13.7.7 Power Supply and Distribution

Electrical power distribution at the mine would utilize multiple voltage levels consistent with industry practice. Major mine loads will be the mine dewatering, support facilities, and maintenance infrastructure.

13.7.8 Communications and Control Systems

The mine will be equipped with a comprehensive communications system, including two-way radio networks, cellular or satellite backup systems, and data communication infrastructure to support operational coordination and safety. A dispatch system may be implemented to optimize fleet productivity and monitor equipment performance. Supervisory control and data acquisition (SCADA) systems will be used to monitor and control key process and infrastructure components, including power distribution and dewatering systems.

13.7.9 Water Supply and Management Infrastructure

Water management infrastructure will include pipelines, storage ponds, and pumping systems to manage both process water and dewatering flows. Given the significant dewatering inflows, the site is expected to be a net water producer, with water reused in processing where practical and



excess water discharged in accordance with regulatory requirements. Potable water will be supplied by truck, as no permanent accommodation camp is planned.

13.7.10 Mine Infrastructure Summary

The proposed mine infrastructure for the Sleeper operation is conventional and appropriate for a 30,000 tpd open pit heap leach project. Key infrastructure elements, including haul roads, material handling systems, dewatering, maintenance facilities, power supply, and communications, have been conceptually designed in accordance with industry standards and comparable operations in Nevada. The relocation of the existing truck shop and the development of new surface infrastructure will support efficient and safe mining operations over the LOM.

13.8 Mine Equipment

The proposed open pit operation will be carry out by contractors, extracting approximately 30,000 tpd of process feed and 66,000 tpd waste, for a maximum total daily material movement of approximately 95,890 tpd based on a waste-to-process feed strip ratio of 1.9:1. Given the projected haul distances, with process feed transported 1.5 km to 4.5 km one-way to the crusher and waste hauled approximately 2.5 km one-way to the waste dump, a conventional diesel-powered truck and shovel fleet using 150 t class rear-dump haul trucks is appropriate.

Based on the planned production rate and a weighted-average haul profile, the haulage fleet would consist of approximately 15 trucks of 150 t trucks. This fleet size is expected to provide adequate capacity to meet the required material movement under average conditions, while allowing for normal mechanical downtime, delays, and short-term cycle-time variability.

Primary loading would be carried out by two hydraulic excavators in the 18 m³ to 22 m³ bucket class, which are suitably matched to the 150 t trucks and would typically load each truck in approximately 4 to 6 passes. A large wheel loader in the 16 m³ to 20 m³ class would supplement the excavator fleet and provide flexibility for ore control. Table 13-10 summarizes the anticipated primary mining equipment fleet requirements.

The support fleet would include a conventional complement of ancillary equipment, including production drills, track dozers, graders, water trucks, fuel and lube trucks, service trucks, and a tire handler. A likely configuration would include two production drills, with one active and one shared standby or campaign support unit, two large track dozers for dump maintenance, pit cleanup, and push assistance, one medium dozer for bench and auxiliary work, two motor graders for haul road maintenance, and two water trucks for dust suppression. Mobile maintenance support would be provided by field service units, lubrication trucks, and a tire handler suitable for the selected truck class.

Table 13-10: Primary Fleet Estimate

Equipment	Typical Size / Class	Qty Operating	Qty Standby / Relief	Total Qty	Primary Duty
Hydraulic excavator	18 to 22 m ³ bucket	2	0	2	Primary process feed and waste loading
Front-end wheel loader	16 to 20 m ³ bucket	1	0	1	Backup loading, blending, crusher support, and cleanup
Rear-dump haul trucks	150 t payload	15	2	17	Process feed and waste haulage



Equipment	Typical Size / Class	Qty Operating	Qty Standby / Relief	Total Qty	Primary Duty
Production drill	171 to 229 mm class	1	1 shared/relief	2	Production drilling
Track dozer	Cat D10/D11 class	2	0	2	Dump maintenance, push assist, pit cleanup
Track dozer	Cat D8 class	1	0	1	Bench cleanup, support work
Motor grader	16M/24M class	1	1	2	Haul road maintenance
Water truck	50,000 to 60,000 L	2	0	2	Dust suppression
Fuel/lube truck	service unit	1	0	1	In-pit fueling and lubrication
Service truck	field mechanic unit	1	0	1	Mobile maintenance support
Tire handler	150 t truck class	1	0	1	Tire changes
Crane / utility truck	site support	1	0	1	Field lifting and support

13.8.1 Fuel Consumption

Using the fleet basis from the mining assumptions, the SLR QP estimates that the operation will consume on the order of 72,000 L to 75,000 L per day of diesel, with a practical base case of about 72,500 L/d (about 19,000 to 19,700 US gal/d). That estimate includes the production fleet and the principal support equipment, not just haulage. The haul fleet consists of 150 t class trucks and uses the Cat 785 as a reasonable proxy, since its nominal payload is 147 t and gross power is 1,193 kW (1,600 hp). The shovel selected was a Cat 6060 hydraulic shovel, which has a gross power of about 2,248 to 2,256 kW, Pit Viper 271-class diesel drills at 652 to 708 kW, and Cat 16 graders at 216 kW.

For the mining rate of approximately 87,600 tpd (total material movement), using an operating basis of 24 h/d, 2 shifts, 4 crews, 53 min/h effective time, and 90% utilization of availability, the mine effectively needs enough active equipment to sustain the target rate of about 19.1 effective operating hours per day. On the haul side, using normal loaded and empty truck speeds for an 8% ramp, plus a 0.8 km to 2.4 km (0.5 to 1.5 miles) ex-pit haul distances, the estimated average cycle time is about 23 minutes for process feed and 26.5 minutes for waste. That supports an operating fleet of approximately 13 haul trucks in service at any one time, which would translate into a purchased or contracted fleet of 14 to 15 trucks total to cover float, maintenance, and shift change. This is an engineering estimate, not a vendor guarantee.

13.8.1.1 Estimated Diesel Consumption by Equipment

Table 13-11 shows the estimated daily diesel consumption for the Base Case. The hourly fuel burn rates are engineering assumptions based on machine class, installed power, and a typical mining duty cycle.



Table 13-11: Equipment Diesel Consumption Estimate

Equipment	Assumed Count Operating	Assumed Fuel Burn (L/h each)	Assumed Operating Hours/Day	Estimated L/d
150-t haul trucks	15	190	21.2	60,420
Cat 6060 hydraulic shovel	1	320	21.2	6,784
Large wheel loaders	2	105	21.2	4,452
Pit Viper-class drills	2	100	18.0	3,600
Cat 16H graders	2	38	18.0	1,368
Track dozers	2	50	18.0	1,800
Water truck	1	80	18.0	1,440
Lube truck	1	15	12.0	180
Service truck	1	15	12.0	180
Light vehicles / pickups	6	5	10.0	300
Total				80,524

That base case is about 80.5 m³/d, approximately 29.4 million L/y.

13.8.1.2 Diesel Storage Comparisons

For storage, the SLR QP recommends that there should be enough fuel on-site to account for weather, supplier delays, delivery timing, and maintenance outages. Using the Base Case burn of about 80.5 m³/d, the recommended storage requirements are shown in Table 13-13.

Table 13-12: Diesel Storage Comparisons

Basis	Days of Storage	Required Diesel (m ³)
Base consumption only	7	564
Base consumption + 15% reserve	7	647
Base consumption only	10	805
Base consumption + 15% reserve	10	926
Base consumption only	14	1,127
Base consumption + 15% reserve	14	1,296

For this Project, a practical recommendation would be to install a total of 850 m³ to 1,000 m³ of diesel storage. The arrangements are provided in Table 13-13.



Table 13-13: Recommended Diesel Storage Arrangements

Tank Arrangement	Total Capacity	Comment
2 × 100,000 gal ASTs + 1 × 25,000 gal day tank	850 m ³ (225,000 gal)	Preferred base case (10.6 days)
3 × 75,000 gal ASTs + 1 × 10,000 to 15,000 gal day tank	890- 900 m ³ (235,000 to 240,000 gal)	Good redundancy, smaller units (11-11.3 days)
2 × 120,000 gal ASTs + 1 × 25,000 gal day tank	1,000 m ³ (265,000 gal)	Better if deliveries are less frequent (12.5 days)
AST – Aboveground Storage Tank		

The preferred base case is approximately 850 m³ of total storage, consisting of two 378.5 m³ bulk tanks and one 94.6 m³ day tank, providing approximately 11 to 12 days of base-case storage and just over 10 days including reserve margin. For the current study level, the QP recommends the following parameters for the budget and layout of the fuel system as follows:

- **Diesel consumption:** 80,524L/d base case
- **Annual diesel:** about 80.5 million L/y

13.9 Mine Personnel

The operation is planned to run continuously on a 24-hour-per-day, year-round basis using a conventional four-crew rotation on 12-hour shifts. Mining activities will be carried out by a mining contractor, who will provide the majority of the operational workforce, including equipment operators, maintenance personnel, and mine-related site support.

The total workforce is estimated at approximately 220 personnel. Of these, about 170 personnel will be employed by the contractor and will support mining operations, equipment maintenance, dewatering, and site services. The remaining approximately 50 personnel will be employed by Paramount owner and will provide technical, supervisory, and administrative functions, including geology, mine engineering, technical services, management, and contract administration.



14.0 Processing and Recovery Methods

14.1 Selected Processing Strategy

Based on the metallurgical test work summarized in Section 10.0, the oxide and mixed Mineral Resources and the existing waste rock dumps are amenable to processing via heap leach with Merrill-Crowe processing. The economic analysis presented in this IA considers the processing of these Mineral Resources only.

Sulfide, HLP, and tailings materials are amenable to processing via flotation, with rougher concentrate assumed to be sold or toll treated at an off-site facility. Sulfide processing is not considered in the economic analysis of this IA. The proposed processing for sulfide, HLP, and tailings materials is presented as an opportunity meriting further evaluation.

14.2 Proposed Process Description

The proposed plant for the initial development case is a conventional crush-agglomerate-heap-leach operation with Merrill-Crowe solution processing. Merrill-Crowe processing has been selected because recovered Ag:Au ratios are expected to exceed 4:1. ROM material from oxide pits and selected waste sources would be crushed to a coarse target size consistent with the historical McClelland test programs, approximately P_{80} 19 mm, and agglomerated with cement at approximately 6.2 kg/t and/or lime as required for pH control. Planned crushing throughput is 30,000 tpd and would consist of primary gyratory crushing followed by secondary cone crushing. Agglomerated material would be conveyor stacked on a lined heap leach pad using a series of conveyors and a radial stacker, with heap lifts constructed at approximately 10 m heights.

Dilute sodium cyanide solution would be applied to the stacked mineralized material using drip emitters at an application rate of approximately 7 L/m²/hr to 8 L/m²/hr. The minimum planned leach cycle is 45 days. Barren solution would be applied to the heap leach pad at a nominal flow rate of approximately 500 m³/hr to 510 m³/hr, with a cyanide concentration of approximately 300 ppm to 400 ppm NaCN. As the solution percolates through the heap, cyanide-soluble gold and silver would dissolve into solution. Pregnant leach solution would be collected through the pad drainage system and pumped to the Merrill-Crowe plant for metal recovery.

In the Merrill-Crowe circuit, pregnant solution would be clarified to remove suspended solids, de-aerated to reduce dissolved oxygen, and contacted with zinc dust to precipitate dissolved gold and silver. The precious-metal precipitate would be recovered by filtration, dried, and smelted to produce doré bars. The barren solution would then be recycled back to the heap leach circuit, with cyanide, lime or pH-control reagents, and make-up water added as required. Make-up water demand is currently estimated at approximately 40 m³/hr to 50 m³/hr. Figure 14-1 shows the crushing and agglomeration flowsheet, and Figure 14-2 provides the overall process plant flowsheet.

14.2.1 Defining Sulfides for the Mineral Resources

Although sulfides are not included as part of the Sleeper process recovery in this IA, sulfide material was included in the Mineral Resource estimate, and a process method was selected. Sulfide, HLP, and tailings materials will be considered separately through a conventional flotation circuit, producing a rougher concentrate. For the definition of Mineral Resources in this IA, the flotation concentrate is assumed to be sold or toll treated off-site rather than processed through an on-site oxidation or concentrate leach plant. Operating costs and payable recoveries



for this route, therefore, include a 12% discount to flotation recoveries to reflect toll milling and related downstream charges. Additional test work is required to further refine opportunities for processing the sulfide, HLP, and TSF material.

14.3 Plant Throughput and Design Basis

The available resource base supports evaluation of a nominal 30,000 tpd heap leach operation, equivalent to approximately 11 Mtpa, as a reasonable benchmark for the conceptual heap leach plant and infrastructure basis. Final throughput should be confirmed against mine scheduling, the proportion of metallurgically supported feed, and the reagent and cycle-time implications of the selected domains.

Major equipment for the heap leach case would include crushing facilities, agglomeration equipment, conveying and stacking systems, lined heap leach cells, solution collection ponds, Merrill-Crowe clarification and precipitation equipment, refining and doré handling facilities, reagent storage and addition systems, and associated utilities.

14.4 Energy, Water, Process Materials, and Personnel

Projected requirements for energy, water, and process consumables for the heap leach case are typical of a Nevada gold-silver heap leach operation. Estimated electrical demand for crushing and conveying, heap leach solution pumping, Merrill Crowe processing and refinery circuits is approximately 4.35 MW operating load. Primary water requirements include make-up water for crushing/agglomeration moisture control, heap leach solution inventory, evaporative losses, and process water make-up. Make-up water is assumed to be provided by pit-dewatering. Principal process consumables include 0.34 kg/mt sodium cyanide, 6.26 kg/mt cement and/or lime for agglomeration and pH control, zinc dust, lead nitrate, diatomaceous earth or filter aid, anti-scalant/flocculant as required, and other Merrill Crowe, refinery and laboratory consumables. Personnel requirements would include 42 operators, 10 maintenance/electrical, and 13 supervision and technical support staff.

14.5 Suitability of the Selected Method

Given the oxide and mixed material is consistent with Sleeper's historical oxide processing history and with the most reliable portions of the metallurgical database (namely Facilities oxide and selected oxide, mixed, and waste composites), it is the QP's opinion that the proposed heap leach and Merrill-Crowe route is a suitable processing method. It is a commercially proven extraction method and does not require special justification as a novel process.

The identified deleterious elements are not currently considered prohibitive; however, elevated Hg, As, Sb, and total sulfur in selected material groups warrant additional metallurgical, precipitate-quality, and refinery test work in future study phases.

Initial refinery capital allowances include a mercury retort as an IA-level provision for mercury management during precipitate handling, doré production, and refinery handling. Future test work should confirm mercury behavior, precipitate, and doré quality, and any required mercury-control measures to refine capital and operating cost assumptions. Sulfide, HLP, and tailings materials may be considered at IA level through conventional flotation, followed by sale or toll treatment of rougher concentrate at an off-site facility. This is also a commercially used approach, but the current application remains preliminary because concentrate quality, payable terms, impurity penalties, and toll milling costs have not yet been demonstrated by project-specific commercial arrangements.



Figure 14-1: Crushing & Agglomeration Process Flow Sheet

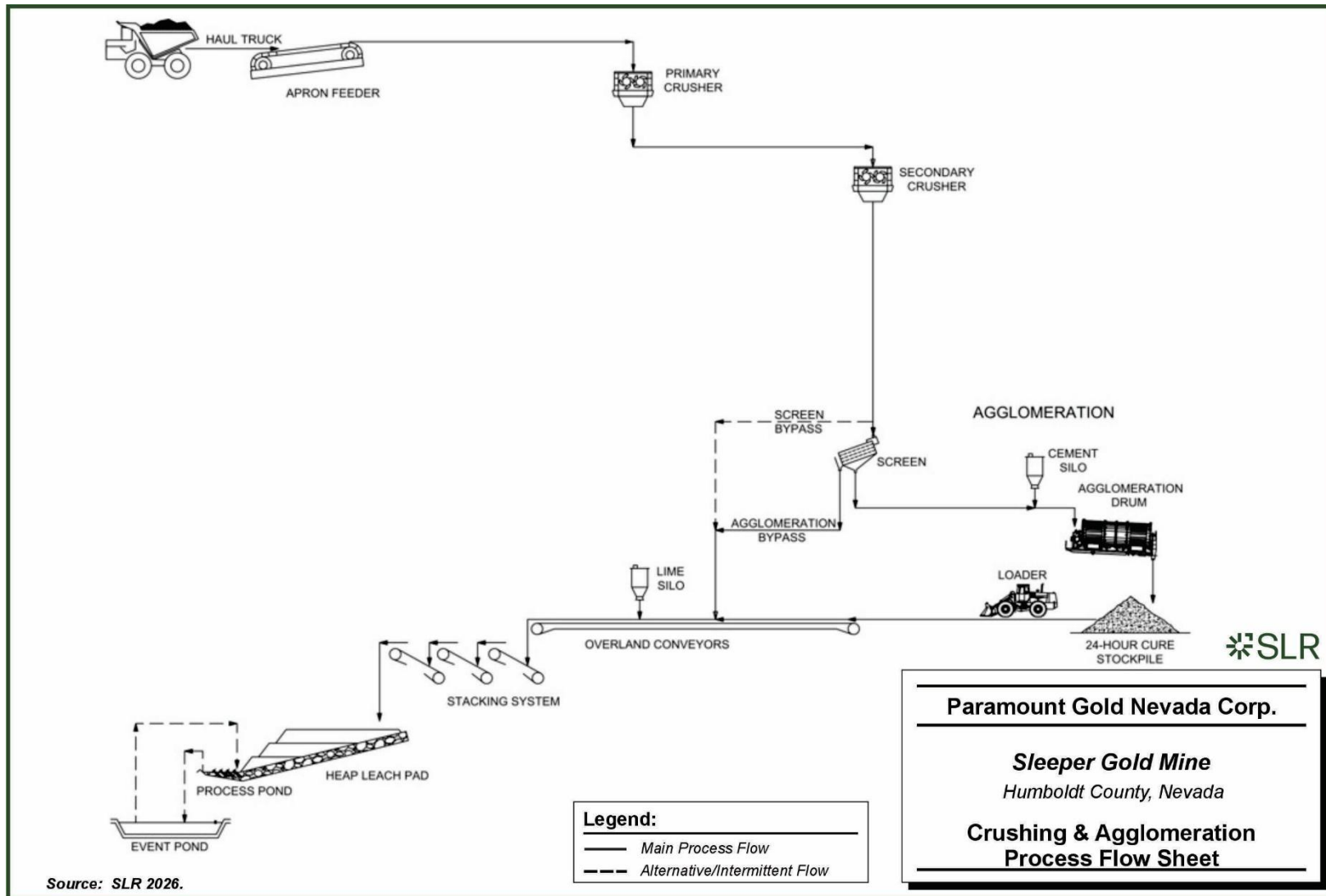
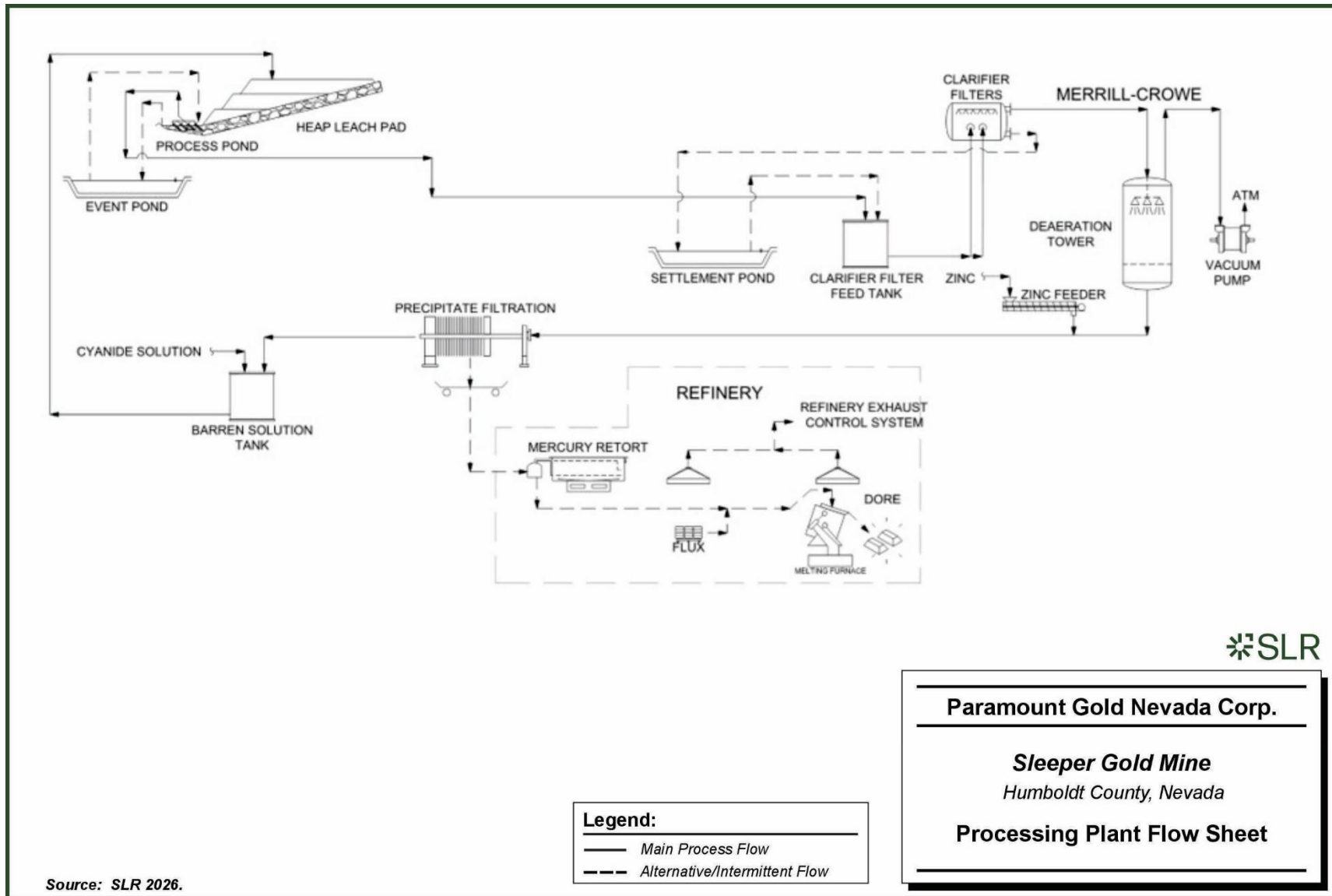


Figure 14-2: Process Plant Flow Sheet



Source: SLR 2026.

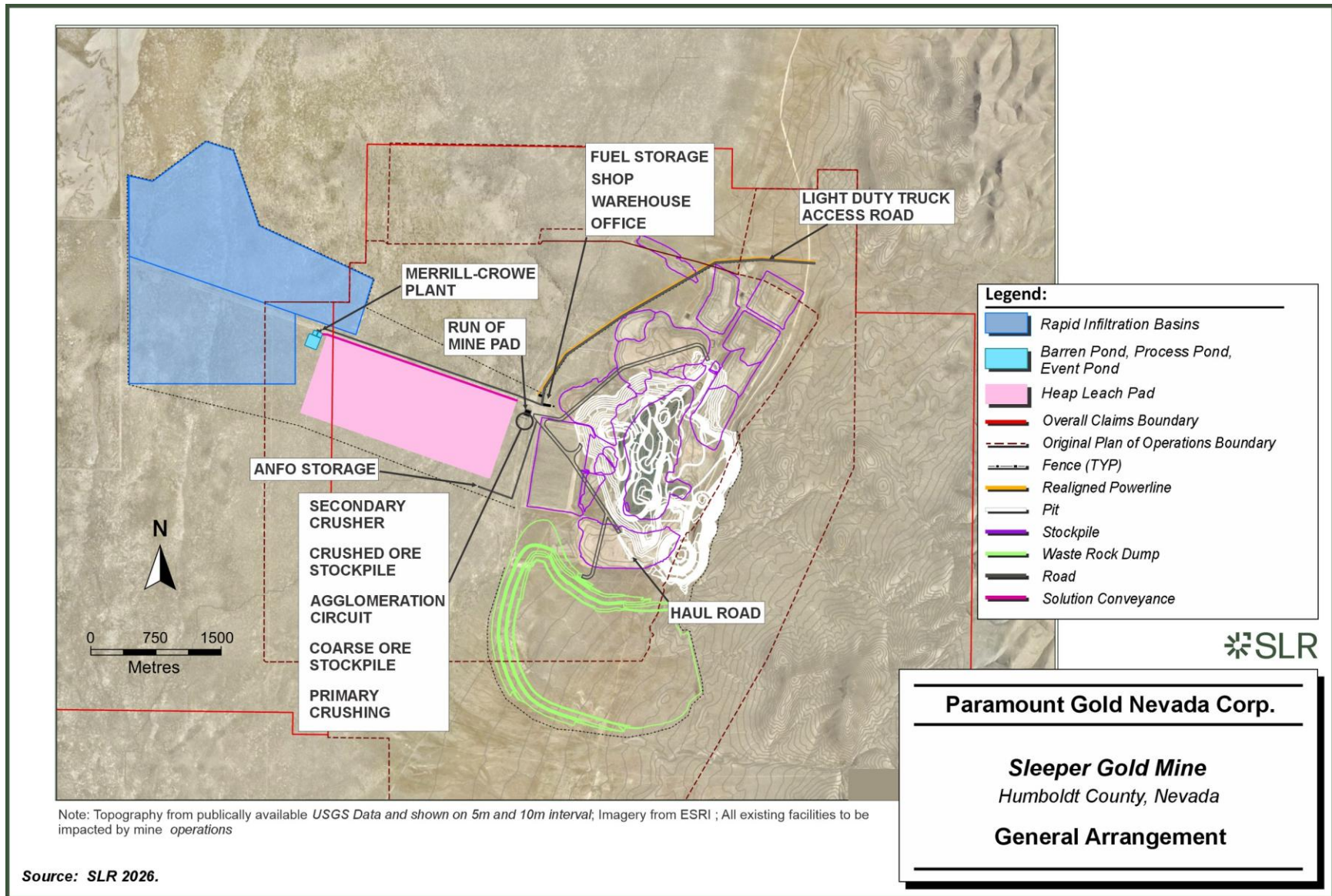


15.0 Infrastructure

The Project infrastructure has been designed to support a large-scale open pit mining and heap leach operation utilizing conventional, well-established technologies commonly employed in northern Nevada. Major infrastructure components include site access and internal mine roads, waste rock storage facilities, ROM and crushed mineralized material stockpiles, a single heap leach pad with associated solution management and storm event ponds, Merrill Crowe Plant for precious metals recovery, electrical power supply and distribution systems, and process and raw water pipelines. The Project benefits from its location within an established mining district with access to existing regional infrastructure, experienced contractors, grid power, and services. Infrastructure development is planned to be staged in alignment with the mine production schedule and designed to meet regulatory, environmental, and operational requirements.



Figure 15-1: Infrastructure Layout



15.1 Access Roads

Existing access to the Project truck shop from Winnemucca, Nevada, is via a combination of paved highway and maintained gravel access roads, with a total one-way distance of approximately 56 km (35 mi). From Winnemucca, proceed north on U.S. Highway 95 for approximately 40 km (25 mi). This segment is fully paved and generally in good condition, providing reliable year-round access. At approximately Milepost 66 to 68 (measured from Winnemucca), turn west onto a graded dirt access road that serves local ranching and mining activities. After leaving U.S. 95, follow the gravel access road for approximately 10 km (6 mi) toward the Sleeper Mine site. This road is typically maintained to accommodate mine-related traffic, although conditions can vary with weather and usage, including sections of wash boarding or minor erosion. The route trends generally west-northwest across gently rolling basin and range terrain. Upon reaching the mine property boundary, continue along internal haul and service roads for an additional 1 to 3 km (1 to 2 miles) to access the main operational area. The current truck shop is located within the central yard complex, adjacent to maintenance bays, fueling stations, and equipment staging areas.

In total, the route comprises approximately 40 km (25 mi) of paved highway driving and approximately 16 km (10 mi) of gravel and site roads, with an estimated travel time of 45 to 60 minutes under normal conditions. Seasonal weather, particularly winter precipitation or spring runoff, may temporarily affect road conditions on the unpaved segments.

15.2 Leach Pad

A synthetically lined Heap Leach Pad (HLP) of approximately 2 Mm² in size will be constructed near the open pit crest to accommodate approximately 175 Mt of mineralized material. The heap will have a total height of 60 m (200 ft), lifts will be placed by radial stacker at a thickness of 10 m (33 ft). The pad footprint of 2 Mm², as shown in Figure 15-1, contains the 175 Mt of heap material at 60 m high and 3H:1V final outslopes at closure.

Mineralized material will be placed on the HLP and irrigated with a cyanide solution. The solution will be recovered from the HLP and stored in the pregnant solution pond (Preg Pond) before being processed and recirculated to the HLP as barren solution. The HLP and External Ponds, collectively referred to as the Heap Leach Facility (HLF), will be synthetically lined so that the solution is in a closed system, with the only net solution loss being to evaporation.

SLR identified a conceptual HLF site within the general area that could be sized to contain the ultimate (175 Mt) HLP capacity, and generally met the following siting constraints:

- Proximity to mining activities
- Gently sloping terrain to maintain positive drainage for solution along the pad liner while remaining geotechnically stable

The leach pad will be synthetically lined with a geomembrane primary liner that is underlain with either a prepared low permeability subgrade or geosynthetic clay liner (GCL). Both applications are acceptable to the State of Nevada. A network of collection system pipelines will be placed over the liner and embedded in a 1-meter-thick lift of granular drain fill (Overliner Drain Fill (ODF)) The pipes will be sized and placed such that the solution application rate over the leached mineralized material will not allow for head to build up on the liner. The particle size distribution of the ODF will allow for free draining of the PLS and will be specified to be two orders of magnitude greater permeability than the barren application rate.



The conceptual HLP layout and capital cost estimate assumed the geotechnical and hydrogeological conditions were suitable. Typical design values were assumed, or values were estimated from previous experience on similar projects, and key criteria were comprised of the following:

- Storage of approximately 175 Mt
- An average annual mineralized material loading rate of 30,000 tpd / 11 million tonnes per annum (Mtpa), resulting in a project life of approximately 16 years (Base Case).
- Mineralized material will be prepared as described in Section 14.0 (crushed and agglomerated) and placed on the HLP using conveyors in 10 m lifts in a retreating manner to limit material compaction. A stability analysis was not performed, and SLR assumed that agglomerated mineralized material will be placed at an overall 3H:1V slope to facilitate closure, a maximum height of approximately 60 m (200 ft), and an average density of 100 pounds per cubic foot (pcf).
- The HLP was designed as a “zero discharge” facility. Containment for the HLP will be provided with a composite lining system, comprised of a Geosynthetic Clay Liner (GCL) overlain by a High-Density Polyethylene (HDPE) geomembrane, over a total area of approximately 200 acres. This liner system is acceptable to the state of Nevada;
- A network of collection system pipelines will be placed over the HDPE geomembrane and embedded in a 2 ft thick lift of granular drain fill (Overliner Drain Fill [ODF]). The pipes will be sized and placed to minimize the risk of head (i.e., pressure) build-up on the liner
- Construction of the HLP was assumed to be over five stages (i.e., approximately three-year increments) to reduce initial capital.

Three external ponds were included in the capital cost estimate, including a pregnant solution pond (Preg Pond), barren solution pond (Barren Pond), and storm event pond (collectively, the Ponds). The HLP will be connected to the pond system via a solution corridor. Typical design values for the external ponds were assumed, or values were estimated from previous experience on similar projects, and key criteria were comprised of the following:

- A water balance was not performed to size the ponds, as pond sizing is based on site specific and operational based criteria, such as dead storage, emergency draindown, operational volume, freeboard, and a design storm event, which is typically the 100-year, 24-hour storm event. For the purpose of the IA, storage of approximately 2.5 million gallons, 2.1 million gallons, and 30.9 million gallons were assumed for the Preg, Barren, and Event Ponds, respectively, based on the QP’s previous experience with similar projects.
- The Ponds were designed as a “zero discharge” facility. Containment for the Ponds will be provided with a double liner system with Leak Collection and Recovery System (LCRS), comprised of a Geosynthetic Clay Liner (GCL) overlain by a HDPE Secondary geomembrane, Geonet drainage layer, and a HDPE Primary geomembrane. This liner has been previously approved by the State of Nevada at similar projects.
- Construction of the Ponds, in their entirety, is assumed to be performed during initial construction.
- The ponds will be double lined with integrated leak collection and recovery systems (LCRS) and will be sized to accommodate:
 - o Freeboard (0.6 m)



- o Operational Volume
- o Emergency Draindown Volume (24-hours of Barren Application Rate)
- o Design Storm Volume
- o Dead Storage for Sedimentation and Pump Priming

The HLP and solution ponds are synthetically lined so that the solution is contained within a closed system, with the only net solution loss due to evaporation, which will be empirically confirmed during pond design using the sitewide water balance.

15.3 Buildings and Facilities

The buildings and facilities described below are in the main plant and offices area, as shown in Figure 15-1:

- Truck shop and mobile maintenance warehouse: The Sleeper truck shop complex will be located near the mine entrance. It is a four-bay shop sized up to 200 t class haul trucks. The shop will contain a tool crib, oil and lubricant bulk storage, multiple offices, locker rooms, a training room, and a warehouse. A covered warehouse storage yard is located adjacent to the admin building complex.
- Process building: The mill building, which is currently not operating, consists of facilities supporting the mineral processing operations, including grinding, gravity separation, flotation, sulfide concentrate filtration and load-out, leach CIP circuit (bypassed), tailings filtration and agglomeration, recovery, and doré casting, and metallurgical laboratory. Adjacent to the mill building is the thickener water storage tank and the remaining CIL tanks from the 1989 flowsheet.
- Crushing plant: The crushing plant will produce P₈₀ 19 mm (0.79-in) material for leaching. Stemming for blastholes, road material, and initial material overliner material for the leach pad which will require additional crushing and screening and will be completed using mobile equipment, not a part of the primary crushing circuit, phased according to construction and development activities.
- Process Recovery: Merrill-Crowe Circuit, zinc precipitation, doré casting, and solution pumping and management. The recovery plant will contain analytical and metallurgical laboratories.
- Wash bay: The wash bay will be located next to the truck shop and consists of one covered bay.
- Administration buildings: The main administration building encompasses most site-support departments.
- Assay laboratory: The assay laboratory will support ongoing mine operations, including grade control and gold solution analysis.
- Motor control center (MCC): The MCC will house controls for the pumps and boosters for the barren and pregnant solution ponds.

15.4 Power Supply and Distribution

Electrical power for the proposed Project is expected to be supplied from the regional electrical grid operated by NV Energy. The project area is situated within a well-established mining district with existing transmission infrastructure, and grid power is considered available within a



reasonable distance of the site. Power would be delivered via a new overhead transmission line, anticipated to be either 69 kilovolt (kV) or 120 kV, depending on final engineering, load growth considerations, and utility interconnection requirements. For the projected peak demand, a 120 kV supply is preferred to provide additional capacity, improved voltage stability, and flexibility for future expansion.

The total connected electrical load for the operation is estimated to be approximately 9 megawatts (MW) to 15 MW, with an average operating demand of 10 MW, based on first principles estimates and benchmarking against comparable heap-leach operations in Nevada. The primary contributors to electrical demand include crushing and conveying, heap leach solution pumping, the Merrill-Crowe recovery plant, pit dewatering, and general site infrastructure, including maintenance facilities, buildings, and lighting. Among these, pit dewatering represents a significant continuous load, reflecting the need to pump approximately 4,542 m³/hr (20,000 gpm) from the open pit.

Electrical power received at the site would be stepped down through a central substation equipped with a primary transformer rated at approximately 25 megavolt-amperes (MVA). The substation would convert transmission voltage (69 kV or 120 kV) to a primary site distribution voltage of 13.8 kV, which would serve as the backbone of the site-wide electrical system. Distribution from the substation would be configured in a radial arrangement with looped circuits for critical infrastructure, including the process plant and dewatering systems, to enhance operational reliability.

Power distribution across the site would utilize multiple voltage levels consistent with industry practice. Major process loads, including crushing, conveying, and high-capacity pumping systems, would operate at 13.8 kV or 4.16 kV, with local step-down transformers where required. The Merrill-Crowe plant, maintenance facilities, warehouse, and ancillary infrastructure would primarily utilize 480-volt (V) systems, while lighting, offices, and control systems would be supplied at 240/120 V. Motor control centers and variable frequency drives would be employed extensively to optimize energy efficiency and process control.

The crushing and conveying circuit are estimated to require approximately 3 MW to 5 MW, supplied at medium voltage, with large motors driving the primary crusher and overland conveyors. Heap leach solution handling systems, including pregnant and barren solution pumps, are estimated to require approximately 0.35 MW to 1 MW. The Merrill-Crowe recovery plant, including clarification, deaeration, zinc precipitation, and refining circuits, is expected to require approximately 1 MW to 2 MW.

Pit dewatering is estimated to require approximately 2 MW to 3.5 MW, depending on final pump configuration, total dynamic head, and system efficiency. The system would consist of staged pumping installations located on pit benches or in sump areas, supplied via medium-voltage distribution. Consistent with operational requirements, no electrical infrastructure would be installed within active mining faces beyond the dewatering pump installations.

Site infrastructure, including the truck shop, maintenance facilities, warehouse, assay laboratory, administrative buildings, and site lighting, is estimated to require approximately 0.5 MW to 1 MW. Additional miscellaneous loads, including reagent handling systems, control systems, and contingency allowances, are estimated at 2 MW to 3 MW.

Emergency and backup power systems would be installed to support critical operations, including process control systems, Merrill-Crowe circuits, and minimum dewatering capacity. These systems would consist of diesel-powered generators with sufficient capacity to maintain safe shutdown and restart conditions. The electrical system would be monitored and controlled



through a supervisory control and data acquisition (SCADA) system integrated with plant operations.

Overall, the proposed electrical power system is conventional for a Nevada-based heap leach operation of this scale and is considered technically feasible. The use of grid power supplied by NV Energy, combined with standard substation and distribution infrastructure, provides a reliable and scalable solution to support the planned mining and processing activities.

Table 15-1: Estimated Power Load by Area

Area	Estimated Load (kW)	Estimated Load (MW)
Crushing and Conveying	3,100	3.10
Heap Leach Solution Pumping	350	0.35
Merrill-Crowe Plant/Recovery/Refining	1250	1.25
Pit Dewatering (20,000 gpm-nominal)	2,400	2.40
Infrastructure, Maintenance & Lab Facilities	1,000	1.00
Miscellaneous and Contingency	2,000	2.00
Total Connected Load	10,100	10.00 – 12.00

15.5 Water

The Project water balance for the proposed 30,000 tpd operation would be dominated by pit dewatering inflows, process solution inventory, heap leach application losses, and evaporation. Mine dewatering, estimated to average approximately 4,542 m³/hr (20,000 gpm), is expected to provide substantially more water than required for crushing, possible agglomeration, heap leaching, and Merrill-Crowe recovery, such that excess water would likely be discharged, subject to permitting and water quality requirements, to engineered rapid infiltration basins (RIBs) located several kilometers and down gradient from the pit.

Process water demand would include dust suppression, ore agglomeration if required, heap leach solution make-up, and plant service water, with solution losses principally associated with heap and pond inventory, evaporation, and residual moisture retained in spent material. No accommodation camp is planned, which materially reduces domestic water demand, and potable water for personnel would be trucked to the site.

Overall, the operation is expected to be a net water producer, with site water management focused primarily on collection, storage, reuse where practical, controlled discharge of surplus dewatering water, and maintenance of adequate operational and environmental water controls.

15.5.1 Current Well Network

As of 2022, four interceptor wells remained operational. All bedrock dewatering wells and the remaining interceptor wells have been decommissioned. In 2005, three of the operational dewatering wells were reported to be completed with line-shaft turbine pumps (WMC 2005a); however, pump reports from 2022 show groundwater discharged from only one of the interceptor wells (New Sleeper Gold 2022). The power lines servicing any on-site line-shaft turbine pumps are expected to remain in place.



As of 2005, four monitoring wells installed adjacent to the tails dam were reported to remain operational. All of the remaining monitoring wells are reported to have been decommissioned (WMC 2005a).

15.5.2 Pit Dewatering Plan

To dewater the Slumber pit lake, infrastructure and service requirements are expected to be as follows:

- One barge-mounted pump operating in the pit lake having a capacity of 631 L/s (10,000 gpm) and an additional barge-mounted pump available on-standby if one of the barge-mounted pumps required maintenance
- Conveyance pipe from the barge pump to the conveyance channel on the west crest of the pit
- Power to the barge-mounted pump
- Submersible camera inspection and rehabilitation of the four interceptor wells remaining from previous dewatering
- A monitoring well network to monitor both groundwater pressures and groundwater quality.
 - Approximately fourteen 50 mm diameter PVC standpipe monitoring wells installed in 200 mm nominal diameter boreholes.
 - Approximately six monitoring wells can be installed to 90 m below grade in the basal gravel aquifer
 - Three monitoring wells installed in the bedrock DFS at 244 m below grade
 - Five monitoring wells in the compartmentalized bedrock PSF assumed to be at 200 m below grade.
 - Total monitoring well drilling would be 2,280 m.
- Twenty 350 mm nominal diameter interceptor wells complete with louvered well screens installed in 450 mm nominal diameter boreholes. As pit lake water level decreases, it is conceivable that as many as 8 additional interceptor wells will be required to lower the head in areas with greater storage capacity.
- Twelve 350 mm nominal diameter bedrock dewatering wells complete with 450 mm nominal diameter surface casings. Since the continuity and interconnectedness of the fracture network is unknown, it is conceivable that as many as four additional bedrock wells will be required. Initially, seven bedrock wells will target the DFS 244 m below grade from the crest of the west wall. Following substantial dewatering of the pit, the remaining bedrock wells will be installed adjacent to compartmentalized zones where groundwater pressures have not been substantially lowered.
- Ten 350 mm nominal diameter wells installed in 450 mm diameter boreholes from the 1,220 m (4,000 ft) elevation in the waste rock piles at the based of the pit. These wells could not be installed until the pit has been dewatered to expose the waste rock and access can be developed for the drill rig.
- Each of the interceptor, bedrock, and waste rock wells completed with a line shaft turbine pump.



- Conveyance pipe from each wellhead to the conveyance channel to the artificial wetland.
- Power to each of the line shaft turbine pumps.
- Excavation of a conveyance channel from the west crest of the pit to the artificial wetland in the middle of the Desert Valley.
- Construction of the impoundment dykes required to develop the artificial wetland.

Generally, installation of functional groundwater dewatering infrastructure is considered to be the critical path that limits the rate at which the pit is dewatered. To maintain pit wall stability groundwater piezometric pressures must be maintained at a level only slightly higher than the level in the pit lake (WMC 2005d).

15.6 Accommodation Camp

An accommodation camp is not required for the Project due to its proximity to the established community of Winnemucca, located approximately 70 km to 80 km (45 to 50 miles) by road from the site. Winnemucca provides sufficient existing infrastructure to support the workforce, including housing, hotels, dining, medical services, and commercial amenities. The Project is accessible via U.S. Highway 95 and maintained access roads, enabling reliable daily commuting for employees.

The operation is expected to utilize a local and regional workforce on a drive-in/drive-out basis, consistent with standard practice for mining operations in north central Nevada. This approach reduces capital and operating costs associated with constructing and maintaining a camp, while also minimizing environmental disturbance and permitting requirements.



16.0 Market Studies and Contracts

16.1 Markets

Gold is the principal commodity at the Sleeper Gold Mine and is freely traded at prices that are widely known, so that prospects for sale of any production are virtually assured. Metal prices for the economic analysis were estimated based on recent consensus industry metal price forecasts and compared with those used in other published studies. The metal prices used for the economic analysis, shown in Table 16-1. These represent the average analyst consensus prices of March 2026.

Table 16-1: Economic Analysis Metal Price Assumptions

Metal Price	Units	Y -1	Y1	Y2	Y3	Y4	Long-Term
Gold	\$/oz	4,370	4,000	3,600	3,600	3,600	3,600
Silver ¹	\$/oz	66.00	59.00	48.00	48.00	48.00	48.00

Note 1: Silver was modeled and evaluated in the cash flow; silver is recovered in the Sleeper recovery facilities.

The doré is securely transported by road freight to a refinery where it is refined into gold bullion. The bullion will be sold by reputable gold trader to banks that specialize in the purchase and sale of gold bullion.

16.2 Contracts

Some of the major contracts that will be negotiated and implemented are discussed below.

- Mining.** Mining operations are expected to be executed by a contract mining firm under a unit-rate agreement, with costs structured primarily on a volumetric basis (US\$/bcm mined) covering drilling, blasting, loading, and haulage activities. The contract would include a schedule of rates for additional “out-of-scope” work, such as road construction, dewatering, and other ancillary services, with provisions for escalation, productivity adjustments, and fuel price variability. Contractor performance would be managed through standard key performance indicators (KPIs), including productivity, dilution control, and safety compliance.
- Diesel Fuel Supply Contract.** Diesel fuel for mining and mobile equipment would be supplied under a term supply agreement with a regional fuel distributor, with pricing typically referenced to published rack or index prices (e.g., OPIS), plus a negotiated differential for delivery, handling, and the supplier's margin. The contract would include provisions for volume commitments, delivery scheduling, on-site storage and inventory management, and adjustments tied to market fuel price fluctuations. Additional terms may address fuel quality specifications, winterization requirements, and contingency supply arrangements to ensure continuity of operations.
- Cyanide Supply Contract.** Sodium cyanide would be procured under a supply agreement with a qualified manufacturer or distributor, with pricing generally based on US\$/tonne delivered and indexed to market conditions and potentially adjusted for freight and energy-related cost drivers. The contract would include provisions for delivery in solid briquette or liquid form, storage and handling requirements, and compliance with applicable safety and environmental regulations (including the International Cyanide



Management Code, where applicable). Supplier support services may include technical assistance, inventory management, and emergency response provisions.

- **Grinding Media Supply Contract.** Grinding media (e.g., steel balls) for the comminution circuit would be supplied under a contract with an established manufacturer, with pricing based on US\$/t delivered and dependent on media specifications, alloy composition, and wear performance guarantees. The agreement would typically include provisions for quality control, delivery schedules, minimum order quantities, and potential price adjustments linked to steel input costs or indices. Supplier performance may be monitored through consumption rates and wear characteristics to optimize operating costs and milling efficiency.
- **Smelting and Refining.** Gold and silver doré produced on site would be sold under standard refining agreements with established precious metal refineries, in which the refineries purchase the doré and pay for the contained metal based on agreed payable percentages. The contract would include typical industry terms for refining charges, treatment fees, assay procedures, and settlement timelines, with deductions for impurities and processing losses as applicable. Final payments are generally based on independently verified assays and prevailing market prices at the time of settlement.
- **Transportation and Handling.** Transportation of doré bullion from site to the refinery would be conducted by a specialized, insured security logistics provider under a contract covering handling, transport, and custody of the material. The agreement would include provisions for secure packaging, chain-of-custody documentation, insurance coverage based on metal value, and defined responsibilities for loss or damage during transit. Logistics arrangements would be coordinated to align with production schedules and refinery delivery requirements.
- **Sales, Hedging, Forward Sales.** The Project may consider implementing a hedging or forward sales strategy for a portion of future gold and silver production to support financing requirements or mitigate commodity price volatility. Any such program would be structured in accordance with standard industry practices and may include instruments such as forward sales, collars, or other price protection mechanisms, subject to market conditions and lender requirements. At this stage, no specific hedging arrangements have been defined.

All contracts described above are expected to be negotiated on commercially reasonable terms consistent with industry norms for comparable Nevada heap leach operations, and no unusual or non-standard contractual provisions are anticipated.



17.0 Environmental Studies, Permitting and Plans, and Social or Community Impact

The Project was developed (mined, milled, and heap leached) by AMAX in the 1980s and 1990s. Operation ceased in 1996. Reclamation has occurred on most of the mine facilities (waste rock dumps, tailing impounds, heap leach pads and ancillary facilities (access and haul roads) and the open pit has been allowed to refill with water. Current activities at the site involve exploration, permit and reclamation maintenance (including e-cells associated with the former heap leach units), and post-closure environmental monitoring.

17.1 Site Environmental Conditions and Monitoring Programs

The summaries of environmental conditions and studies in this section are based on information documented in environmental impact statement (EIS) and environmental assessment (EA) baseline reports as well as the water pollution control permit (WPCP) and regulatory submissions required under the various permits and EIS/EA conditions. A Final Permanent Closure Plan (FPCP) for the Sleeper site was submitted to the Nevada Department of Environmental Protection (NDEP) in 2003 for site-wide closure of the former project. The FPCP included details supporting characterization and stabilization information relative to the various facilities at the site and the stabilization and closure of remaining process facilities.

17.1.1 Physiography

Sleeper is located in northern Nevada in the Great Basin region of the Basin and Range physiographic province. The Project area is situated in a valley on a gently west-sloping alluvial plain at an approximate elevation of 1,300 masl (4,265 fasl).

17.1.2 Geology

The Basin and Range is characterized by a series of generally north-trending, fault-bounded mountain ranges separated by broad alluvium or lake sediment-filled valleys. The Project is at the northwestern flank of the Slumbering Hills within the Desert Valley, which is a typical Basin and Range, fault-bounded valley. The underlying geology is comprised of Mesozoic basement rocks overlain by a sequence of Tertiary volcanic and volcanoclastic units.

17.1.3 Acid Rock Drainage/Metal Leaching Potential

Acid base accounting (ABA) and meteoric water mobility procedures (MWMP) were performed by Hydrotechnica in 1989 to determine acid rock drainage and metal leaching potential in support of the initial WPCP. The results have been used to update the pit lake model, with the latest update in 2021 by Piteau. The MWMP analysis for alluvium indicated that arsenic, iron, mercury, and manganese have the potential for mobility in the alluvial system. In the oxidized volcanic bedrock, analysis conducted to date indicates most metals are immobile; however, the unoxidized volcanic bedrock indicates significant potential exists for mobilizing major cations and anions, as well as trace metals such as manganese and arsenic. The current updated 2016 pit lake model shows that modelled results of these parameters will remain within Profile III reference ranges for the 104-year model simulation, with the possible exception of fluoride (Piteau 2021).

To reduce the impact of acid generation and metal leaching, the open pits on site were partially backfilled with oxidized and unoxidized material and rapid filled through pumping to form a pit lake. Lime slurry was added to the pit lake between July 1996 and November 2001 to increase



the pH of the pit lake water. Consistent monitoring of the pit lake and modeled lake chemistry has shown that most parameters are stable, with a slow increase of alkalinity from alluvial groundwater. The data from monitoring indicates there are no increasing constituent trends and seasonal differences appear to be low. The main control of future water quality is evapoconcentration; however, the rate of evapoconcentration on the site remains low (NDEP 2017).

Oxide and sulfide ore was placed on the existing heap leach pads during operations. The heap leach pads were reclaimed in 2000 in accordance with approved closure plans. Solution from heap leach draindown is monitored semi-annually and quarterly, and indicates the solution is acidic. Draindown solution from the heap leach facilities is managed through passive e-cells. Draindown solution for all pads contain elevated metals and sulfate, with the NROM pad showing consistently higher concentrations of aluminum, arsenic, iron, sulfate, zinc and total dissolved solids.

The existing waste rock dumps consist of alluvial material and both oxidized and unoxidized argillized volcanic tuffs. Acid neutralizing potential (ANP) / acid generating potential (AGP) ratios indicate a net acid generating potential. It is unknown where potentially acid-generating material was placed within the existing waste rock dumps, and no seeps have been observed during quarterly inspections conducted since the completion of reclamation.

17.1.4 Atmospheric Environment

The climate at Sleeper is arid, characterized by warm, dry summers and cold, dry winters. Site-specific data is collected from a meteorological station on the northern side of the site. Site data collected from 2003 to 2025 indicates an average annual temperature of 10°C with a range of -30°C to 36°C, and 153 mm of average annual precipitation with a range of 47 mm to 447 mm.

The air quality in the region of the Project is generally good, due to the limited population and industrial activity. Several mines in the vicinity have the potential to contribute to particulate emissions and industrial pollutants within the Project area. The nearest currently active mine is the Turquoise Ridge-Twin Creeks mine, located approximately 72 km (45 miles) as the crow flies to the east.

17.1.5 Acoustic Environment

Sleeper is in a remote area with limited human activity, and no substantive anthropogenic noise sources within 42 km (29 mi). The nearest town is Winnemucca, Nevada, located approximately 42 km (29 mi) south of the Project area. Ranching activities occur in proximity to the site, which contribute limited noise to the surrounding area. Highway 95 is located approximately 19 km (12 mi) east of the project site, which contributes traffic noise in proximity to the Project area as one of the main travel ways to Idaho and Oregon.

17.1.6 Groundwater and Surface Water

The Project area is located within the Desert Valley (031) groundwater basin. The depth to water in the shallow aquifer before mining activity was approximately 9 m (30 ft) to 12 m (40 ft) below ground surface (bgs). Several hydrologic and hydrochemical models for the site that have been prepared by Water Management Consultants Inc. (WMC) are listed (WMC 1995):

- Sleeper Mine Summary of Groundwater Conditions Beneath the Tailings Dam (1994)
- Preliminary Assessment of Hydrologic and Hydrochemical Conditions in the Final Pit (1994)



- Results of Supplemental Pit Lake Modeling and Closure Plan for the Final Pit (1995)

Additionally, the most recent update to the Sleeper project was completed by Piteau in 2021.

There are three hydrogeologic units identified within the Project area:

- Shallow groundwater zone – lacustrine unit comprised of silty-clay sediments, varying in thickness from near zero to 30 m (100 ft) in the vicinity of the pit area.
 - Basal Gravel Aquifer – this aquifer largely dominates the regional groundwater flow system in the Project area and ranges in thickness from near zero to over 152 m (500 ft) west of the pit.
 - Volcanic bedrock aquifer – groundwater movement in this aquifer is a result of fracture flow, with variable hydraulic conductivity. The thickness ranges from near zero to 52 m (170 ft).
- Because of the abundant fractures within the rocks, the bedrock complex in the Project area, along with the overlying Basal Gravel Aquifer, is the principal source of groundwater. Water chemistry in the shallow groundwater zone is believed to represent background conditions. No baseline data exists on the volcanic bedrock aquifer.

There are no surface waters at or near the mine site, with the exception of the pit lake. Groundwater modeling and pit lake monitoring indicate the pit lake water level has stabilized at an elevation of about 6 m (20 ft) below the pre-mining groundwater level. The latest pit lake model by Piteau in 2021 indicates the pit lake effectively collects groundwater beneath the mine site facilities and will remain a permanent hydrogeologic sink. Contact stormwater is contained on site and non-contact stormwater (stormwater runoff generated from the closed waste rock dumps) discharges off site. The site is considered a zero-discharge facility.

17.1.7 Wildlife

There is limited data available for the Project regarding wildlife and biological resources within the area. Big game species, such as mule deer and pronghorn antelope, small mammals, reptiles, aquatic, and avian species exist within the project area. Several raptor species inhabit the project area, including owls and hawks. It is unknown if golden eagles are present in the project area. No known special status species or threatened or endangered species occur within the project area. There is evidence of aquatic species within the pit lake.

17.1.8 Cultural Resources

A cultural resources survey was conducted for the 1985 EA resulting in the identification of one obsidian flake within the project area. There is no evidence of significant cultural or archaeological sites.

17.2 Waste and Tailings Disposal, Site Monitoring, and Water Management

17.2.1 Tailings Storage Facility

The tailings impoundment was designed as a zero-discharge facility. It was constructed as a native clay-lined facility in accordance with existing standards and was approved by the Nevada Department of Environmental Protection (NDEP). The tailings impoundment was designed to allow for 6.6 million tons of tailings to be deposited over 63 hectares (156 acres). The facility



was constructed in four phases from 1985 through 1994. The final thickness of tailings is about 13.7 m (45 ft) in the southeast corner of the impoundment and about 13.1 m (43 ft) in the northwest corner. The present surface area of the tailings is approximately 45 hectares (113 acres). The tailings facility is closed and released, in accordance with the Closure and Reclamation Plan for the Tailings Impoundment (June 1998) and Final Plan for Permanent Closure (2003), with revegetation remaining as the only remaining activity that has yet to be released. No drain down has been measured since 2009, and the Tailings Seepage Pond was closed in 2017.

17.2.2 Waste Rock Storage Facilities

There are three existing waste rock storage facilities on the site (North, West, and South dumps) that total approximately 171 hectares (423 acres). The waste rock storage facilities on site are reclaimed and revegetated, except for a small laydown area on the South Waste Rock Dump, a non-hazardous solid waste landfill within the West Waste Rock Dump, and a portion of the site access road is located on the North Waste Rock Dump to allow for access to associated collection ponds for processing. Approximately 44.2 metric tons (48.8 million short tons) of oxide and sulfide material was placed onto the heap leach pads during operations. Leaching or recirculation of solution has not occurred since 1997.

17.2.3 Heap Leach Facilities

The heap leach pads were capped and covered in 2000 in accordance with the closure and reclamation plans approved by the NDEP. Pads were graded and revegetated to allow for surface water runoff, which is routed to a long-term stormwater diversion channel that runs along the facility, designed for the 100-year, 24-hour storm event. Process ponds have been closed and in 2023, process ponds for pads 2 (Process Pond #2), 4 (Overflow Pond #4) and NROM (Overflow Pond NROM) were converted to double-lined E-cells with leak detection to passively manage draindown through evaporative disposal. E-cell conversion was completed in 2024 in accordance with approved plans and designs.

The following ponds were closed between 2017 and 2020:

- Overflow Pond #2
- Overflow Pond #3
- Process Pond #4
- South Barren Pond
- Process Pond NROM

The following ponds were closed in 2023:

- Closure of Process Pond #3
- Conversion of Process Pond #2 to E-cell #1
- Conversion of Overflow Pond #4 to E-cell #2
- Conversion of Overflow Pond NROM to E-cell #3

Flows from heap leach pads 1 and 2 are routed via gravity piping to E-Cell 1, flow from heap leach pad 4 is routed via gravity piping to E-Cell 2, and flows from heap leach pads 3 and NROM are routed via gravity piping to E-Cell 3.



17.2.4 Water Management

The project site is considered a zero-discharge facility. All contact stormwater is captured on-site, and facilities have been designed to manage stormwater in diversion channels and features to prevent off-site discharge of contact water. Draindown solution from the heap leach pads is routed to and managed within the E-cells. The pit lake is passively contained.

17.2.5 Monitoring

Routine monitoring is conducted on a quarterly, semi-annual and annual basis as required in the WPCP. Monitoring includes groundwater, pit lake, heap leach pad draindown, erosional stability of closed landforms, and identification of seeps. The site is in compliance with all current permits. There are no known Notices of Violation active at the site; however, some erosion has occurred on the North Waste Rock Dump that is being monitored.

Tailings Storage Facility

The tailings storage facility is reclaimed and released, and monitoring is no longer required.

Waste Rock Dump Facilities

The waste rock dumps are monitored semi-annually for physical stability and presence of seeps.

Heap Leach Facilities

The heap leach pads are monitored for erosion and stability. Process solution is monitored for weekly fluid in the leak detection systems. The draindown solution is monitored on a quarterly basis from each pad, as well as combined E-Cell fluid.

Water Management

Seven groundwater wells are located around the perimeter of the facility to monitor any potential impacts to groundwater on a quarterly basis. The pit lake is monitored continuously for water elevation, quarterly for surface water quality and semi-annually at different depths within the pit. Additionally, meteorological conditions at the site are monitored as required in the WPCP.

17.3 Project Permitting

Current permits for the site exist at the county, state and federal levels, and the Project will be subject to additional permits and amendments to ensure compliance with regulatory requirements and to mitigate potential environmental impacts. Current permits at the site are referenced in Table 17-1 and include the Record of Decision for exploration and closure from the Bureau of Land Management, a WPCP, Reclamation Permit, Surface Area Disturbance Permit, and Class III Solid Landfill Waiver from the NDEP, which may require modification for operations as described within this IA.

The Project is within public lands and is authorized under BLM 43 CFR 3809 mining regulations. Mining activities in accordance with the IA would require an amendment to the current Plan of Operations, which would be submitted to the BLM for *National Environmental Policy Act of 1969* (NEPA) determination. Following their review, the BLM will determine whether an EA or an EIS is required for compliance with NEPA. The EA or EIS would be prepared, and would require additional baseline surveys to be conducted, in accordance with NEPA and BLM guidelines for mining on public lands. Baseline studies and preparation of a new EA or EIS could take 12 to 36 months to complete for an operating site. Baseline studies would be required to assess current conditions for multiple resources including but not limited to groundwater and surface water,



flora and fauna, cultural and social environment, air and wildlife. During the NEPA process, baseline studies will be utilized to facilitate the NEPA process and potential impacts to resources in the EA or EIS. Cultural resources determined to be significant by the Nevada State Historic Preservation Office (SHPO) office will need to be managed through avoidance or approved mitigation during development.

State permits will need to be obtained from NDEP and other state agencies. The primary permit is the WPCP in accordance with NAC 445A.350-445A.447, for any mining operation that has a “mine, waste rock piles, ore piles, beneficiation process components, processed ore disposal sites, and all associated buildings and structures that have the potential to degrade waters of the state”. The Project currently has a WPCP for a closure facility, and a new permit would need to be obtained for mining and processing operations as described in this IA. The Project would also require a new or modified Reclamation Permit in accordance with NAC519A.010-519A.415, “for any exploration, mining, milling, or other beneficiation process activity that proposes to create disturbance of greater than five acres, or remove an excess of 36,500 tons of material from the earth in any calendar year.”

Required or potential permits are included in Table 17-1.

Table 17-1: Required or Potentially Required Permits

Regulatory Agency	Permit Name	Activity	Status
BLM	Record of Decision resulting from NEPA process	Mine Operation, Exploration	Will require modification through NEPA process
EPA	EPA/RCRA ID	Hazardous waste generation and storage	To be initiated
Federal Bureau of Alcohol, Tobacco, and Firearms	Explosives License	Transport, shipment, receiving, or possessing explosive materials	To be initiated
NDEP-BMRR	Water Pollution Control Permit	Protection for Waters of the State	Amended or new permit to be initiated
NDEP-BMRR	Water Pollution Control Permit (RIBS)	Discharge of water produced from the dewatering of the open pits	New permit to be initiated
NDEP-BMRR	Reclamation Permit	Reclamation Plan and Bond	Amended or New permit to be initiated
NDEP- BAPC	Air Quality Permit	Facilities that emit air pollutants	To be initiated
NDEP- BAPC	Surface Area Disturbance Permit	Surface disturbances of more than 5 acres for dust generation	Amended or New permit to be initiated
NDEP- BWPC	Mining Stormwater Permit	Control of stormwater discharges from mining facilities	To be initiated
NDEP- BWPC	Onsite Sewage Disposal Permit	Disposal of sewage	To be initiated



NDEP- BSDW	Potable Water Permit	Providing potable and drinking water	To be initiated
NDEP- BWM	Waste management Permit	Generation of waste and determination	To be initiated, Landfill application amended
NDWR	Permit to Appropriate Public Waters	Water rights for use or production	Amended
NDOW	Industrial Artificial Pond Permit	Protection of wildlife from process solutions	Amended
NDOT	Encroachment Permit	Transportation and use of roads to site	To be initiated
NDOM	Mine Registry Form	Registration of mining projects in Nevada	To be initiated
NDIR	Opening of Mine Notification	Business notification of opening a mine	To be initiated
Nevada State Fire Marshall	Emergency Response Plan	Inventory and response plan for hazardous materials	To be initiated
Humboldt County	Building Permits	Mine operations and facilities	To be initiated
<p>Notes:</p> <p>BAPC Bureau of Air Pollution Control BLM Bureau of Land Management BMRR Bureau of Mining Regulation and Reclamation BSDW Bureau of Safe Drinking Water BWPC Bureau of Water Pollution Control BWM Bureau of Waste Management EPA Environmental Protection Agency NDEP Nevada Division of Environmental Protection NDIR Nevada Division of Industrial Relations NDOM Nevada Division of Minerals NDOT Nevada Department of Transportation NDOW Nevada Department of Wildlife</p>			

17.4 Social or Community Requirements

There are no known social or community issues that would have a material impact to the Project. Identified socioeconomic issues (employment, payroll, services and supply purchases, and State and local tax payments) are anticipated to be positive through the creation of direct and indirect jobs. Hiring practices will include local staff to the extent practicable.

As many new development projects have been identified in the area, community and tribal engagement is a key element to the successful development of a mining project. As the Project progresses beyond IA, Paramount will engage with the local community and tribal entities to allow an understanding of concerns, opportunities, and goals for the Project leading up to, during, and post operation. Engagement at this level has not occurred to date but will occur as part of the mine planning and permitting process.



17.5 Mine Closure Requirements and Summary

The BLM and NDEP-BMRR require a closure plan to be submitted with the submittal of a Plan of Operations, which includes closure and reclamation cost estimate for bonding as well as reclamation and closure plans for facilities and disturbance. A closure cost estimate is required to provide the BLM and/or NDEP surety bonds in the event the operator is unable to fulfill closure requirements to prevent unnecessary or undue degradation of the environment. Closure planning is conceptual at this point, as the mine plan has not been fully developed. All facilities will be closed in accordance with applicable closure regulations. Growth media will be salvaged from existing waste rock dumps and stockpiled for use in reclamation.

The open pit will become a pit lake, and earthen berms will be placed around the perimeter at closure. Depending on water quality analysis and modeling during the Project, inert backfill or lime may be placed within the pit upon closure. This closure approach mirrors the current successful closed condition of the pit lake.

The existing TSF is closed, and no additional closure is expected to occur.

The Heap Leach Pad will be recontoured to a final stable slope, and inert cover material or growth media will be placed on the top and slopes. The area will be revegetated with an approved BLM seed mix. The top will be graded to allow for stormwater runoff. Solution management ponds will be drained and converted to evaporative cells to manage long-term solution. This closure approach mirrors the current successful closed condition of the existing heap leach pads.

Waste rock dumps will be recontoured to a final stable slope and graded to allow for stormwater runoff. Inert cover material or growth media will be placed on top and slopes, and the top and slopes will be revegetated with an approved BLM seed mix.

Buildings and facilities will be demolished and disposed of in accordance with applicable waste regulations, at an on-site non-hazardous landfill. Roads, yards, and other ancillary disturbances will be graded to mirror pre-existing topography and prevent erosion or ponding and revegetated with an approved BLM seed mix.

Reclamation bonding will be prepared using the State Reclamation Cost Estimator (SRCE) model and submitted to the BLM and State agencies to provide financial assurance for the Project. The SRCE model was originally developed as a cooperative effort between the NDEP-BMRR, the U.S. Department of the Interior, BLM, and the Nevada Mining Association (NVMA), to facilitate accuracy, completeness, and consistency in the calculation of costs for mine site closure and reclamation. It is not possible to prepare a SRCE at this stage due to the preliminary nature of the project development. However, based on the size and processing rate described in this IA, a preliminary closure cost estimate ranges between US\$35 million to US\$60 million.

17.6 QP Opinion

The SLR QP is of the opinion that the current plans are adequate to address any issues related to environmental compliance, permitting and local individuals or groups. Plans will be modified as needed to address new issues as they arise.



18.0 Capital and Operating Costs

The capital and operating costs presented in this section include those required to mine and process Mineral Resources from Sleeper Gold Mine. All capital and operating costs in this section are expressed in Q2 2026 US dollars, and unit costs are based on metric tonnes.

SLR's forecast capital and operating cost estimates for the development of Mineral Resources have been prepared using a combination of first principles estimating, benchmarking against comparable projects, and available contractor quotations.

In accordance with the American Association of Cost Engineers (AACE) classification system, the estimates are predominantly Class 5 (scoping-level), indicating a preliminary level of project definition. At this stage, the expected accuracy range is approximately -50% to +50%.

A 25% contingency allowance has been applied to the base capital estimate. This contingency is considered appropriate for a Class 5 estimate and is intended to account for uncertainties associated with limited scope definition, quantities, unit pricing, and execution factors. The contingency does not eliminate the inherent variability in a scoping-level estimate but provides a reasonable allowance for the identified and anticipated risks consistent with the current level of engineering and project development.

18.1 Capital Costs

Life of mine (LOM) capital costs for the Project are estimated at \$596.1 million, and reclamation/closure costs are estimated at \$52.4 million, as summarized in Table 18-1. Initial capital is \$201.1 million and is considered reasonable because (i) the mining fleet will not be purchased as the Base Case assumes contract mining, and (ii) the leach pad will be built in phases.

Costs related to the leach pad are needed to provide additional space for mined process feed. Finishing the Phase 2 construction for the leach pad is estimated to cost approximately \$19 million (year 6), Phase 3 is estimated at \$19 million (year 9), and Phase 4 will cost \$19 million (year 12). These costs have been distributed over time.

As dewatering capital costs will start in year 3, these are considered sustaining capital; the LOM total for dewatering costs is \$139 million (excluding indirect costs).

The Project's economic analysis includes \$52.4 million for Mine Reclamation and Closure, per the updated asset retirement obligation (ARO) estimate and LOM reclamation spend schedule as of 2026. SLR's initial estimate for re-permitting the Project is \$5.5 million.

Table 18-1: LOM Capital Cost Estimate

Capital Area	LOM Total (\$ 000)
Initial Growth and Development Capital	201,085
Sustaining Capital	342,544
Reclamation/Closure Capital	52,432
Total	596,062



Table 18-2: LOM Capital Cost Estimate by Major Area

Capital Area	Initial Growth and Development Capital (\$ 000)	Sustaining Capital (\$ 000)	LOM Total (\$ 000)
	(Year -2 to Year -1)	(Year 1 to Year 17)	(Year -2 to Year 17)
Mining – Mine Equipment (Contract Mining)	-	-	-
Mining – Dewatering	-	138,866	138,866
Processing – Leach Pad / Ponds	40,635	58,132	98,767
Process – Recovery Plant	56,964	2,316	59,280
Infrastructure	23,497	41,007	64,504
Indirects	39,772	33,714	73,486
Contingency	40,217	68,509	108,726
Total Before Closure	201,085	342,544	543,629
Reclamation / Closure Capital		52,432	52,432
Total	201,085	394,977	596,062

18.2 Operating Costs

Table 18-3 presents the average LOM unit operating costs.

Table 18-3: LOM Average Unit Operating Costs

Mining Area	Unit Mining Cost
OP Mining-Base (\$/t mined) – typical year of full production	\$2.40/t
OP Mining-Out of Scope Work (\$ 000/yr) – LOM annual average	\$4,867/yr
Total Mining (\$/t processed)	\$6.37
Total Dewatering (\$/t processed)	\$0.59
Processing (\$/t processed)	\$5.55
G&A (\$/t processed)	\$0.52
Total (\$/t processed)	13.03

18.2.1 Primary Consumable Costs

Power costs are estimated based on NV Energy Northern Nevada tariffs and benchmarked against comparable industrial operations, with an assumed high load factor typical of continuous mining operations. SLR used US\$0.085/kWh for the Base Case.

Diesel fuel costs are based on off-highway (dyed) diesel pricing in northern Nevada, benchmarked against recent retail prices, less applicable federal and state fuel taxes, and adjusted for bulk supply conditions typical of large mining operations. SLR used US\$3.50 per US gallon (\$0.92/L).

Propane costs are based on bulk delivered pricing in northern Nevada, benchmarked against wholesale propane indices and commercial delivery rates. A base case of approximately \$2.25 per US gallon has been assumed.



Sodium cyanide costs are estimated at approximately US\$2,650/t (equivalent to approximately US\$2,400/st) delivered to site.

It has been assumed that high-calcium pebble quicklime (CaO) will be used and slaked on site as needed. Costs for the type of lime are assumed to be US\$375/t.

18.2.2 Workforce

Sleeper will be one of the largest employers in Humboldt County, Nevada, and it will contribute significant tax revenue to the State of Nevada. The average full-time employee count in year 3 of the operation is estimated at 220. PGN anticipates that approximately 75% of the workforce will live in Humboldt County and approximately 12.5% in Elko and Eureka Counties, with the remaining workforce from other areas. A tabulation of the Project’s workforce is presented in Table 18-4. On average, 75% of the workforce is paid hourly.

The proposed operation would employ a conventional four-crew rotation on 12-hour shifts to support continuous 24-hour-per-day, year-round mining and processing activities. The total workforce is estimated at approximately 220 personnel, including both hourly and salaried staff. The hourly workforce, comprising approximately 170 personnel, supports mining, maintenance, processing, and site services, while the remaining 55 personnel consist of supervisory, technical, engineering, geological, and administrative staff.

Mine operations represent the largest component of the workforce, followed by maintenance and processing functions. Staffing levels reflect the use of a 150 t class truck and shovel fleet, which reduces operator requirements relative to smaller truck configurations, as well as the relatively simple processing flowsheet consisting of crushing, heap leaching, and Merrill-Crowe recovery. Additional personnel are allocated to support pit dewatering operations, which represent a significant operational component at the site. The absence of an accommodation camp further reduces total staffing requirements, as all personnel are expected to operate on a drive-in/drive-out basis from nearby communities.

Table 18-4: Sleeper Workforce (Year 3)

Category	Personnel
Mine Operations	80–90
Mine Maintenance	40–50
Processing / Water / Merrill-Crowe	25–35
Geology / Ore Control	8–12
Engineering	8–12
Supervision	12–16
HSE / Environmental	6–10
Warehouse / Admin / Support	20–25
Total	210–220



19.0 Economic Analysis

The economic analysis presented in this IA considers the processing of the in situ oxide and mixed Mineral Resources and the Mineral Resources in the existing waste rock dumps only.

The economic analyses contained in this TRS are preliminary in nature and are based, in part, on Inferred Mineral Resources that are considered too speculative geologically to have modifying factors applied to them that would enable them to be categorized as Mineral Reserves. It is important to note that, unlike Mineral Reserves, Mineral Resources do not have demonstrated economic viability, and there is no certainty that the economic projections presented in this IA will be realized.

Taxes and revenues are assumed. Discounted cash flow analyses are based on assumed production rates and revenues from available Mineral Resources.

SLR notes that the economic analysis presented in this section is based on revenue from gold and silver only. After-tax cash flow projections have been generated from the Base Case and the Alternative Case LOM production schedules and capital and operating cost estimates, as summarized in the sub-sections that follow.

19.1 Base Case

The Project's Base Case is based on a production plan with a mine life of 17 years and includes a mineralized material inventory of approximately:

- Approximately 47 million tonnes (Mt) of waste rock dump material, classified as Inferred Mineral Resources, grading approximately 0.28 g/t gold (Au)
- In situ oxide and mixed Mineral Resources, including approximately 2 Mt Measured Resources grading 0.29 g/t Au, 78 Mt Indicated Resources grading 0.26 g/t Au, and 49 Mt Inferred Resources grading 0.24 g/t Au.

The Base Case mineralized material inventory includes approximately 95.6 Mt of Inferred Mineral Resources containing 788 koz of gold and 6,484 koz of silver, representing approximately:

- 55% of the total Base Case tonnage.
- 54% of the total Base Case gold ounces.
- 41% of the total Base Case silver ounces.

The remaining material in the mined inventory is from Measured and Indicated Mineral Resources. A summary of the Base Case criteria is provided below.

19.1.1 Economic Criteria

19.1.1.1 Revenue

- Mine life: 17 years.
- LOM production and processing plans as summarized in Table 13-9 and Table 13-8, respectively.
- 30,000 tpd mineralized material stacked (approximately 10.8 Mt per year), average stacked grade of 0.26 g/t Au and silver grade of 2.79 g/t Ag (ROM, crushed, and stockpile mine plan).



- Mine life averages 65,000 ounces per year of gold recovered and 205,000 ounces per year of silver recovered from the mine plan, with LOM stacked process gold recovery averaging 75.8% and silver recovery averaging 22.1%.
- Total 1.11 Moz of gold recovered, and 3.5 Moz of silver recovered over the LOM operation.
- The summary of the physicals in the financial model is listed in Table 19-1. It has been estimated that 420 koz of gold and 2,952 koz of silver are in waste rock dumps and are accounted for in the financial model over the first five years of Leach Pad operations.
- Gold and silver payable at the refinery are assumed at 99.95% Au payable and 97.0% Ag payable
- Gold and silver prices are based on analyst consensus price forecasts from the end of March 2026. For the economic analysis it was assumed:
 - o Y1: US\$4,000/oz Au and US\$59.00/oz Ag
 - o Y2 to Y17: US\$3,600/oz Au and US\$48.00/oz Ag
 - o Resulting in LOM net realized prices of:US\$3,618/oz Au and US\$48.70/oz Ag
- Net Smelter Return (NSR) includes doré refining, transport, and insurance costs.
- NSR royalty assumed at 3%. The property is subject to different royalties between 0.5% and 3%, and for modeling purposes was assumed at an overall 3%
- Revenue is recognized at the time of gold and silver production.
- Non-cash inventory adjustments are not included in the SLR cash flow model.
- LOM net revenue is US\$4,014 million (after royalty, transportation, and refining charges)

Table 19-1: Sleeper Base Case Production Physicals Summary

Physicals	Value
Total Mineralized Material Stacked (kt)	175,445
Max Process Rate (tpd)	30,000
Au Head Grade (g/t)	0.26
Ag Head Grade (g/t)	2.79
Contained Au (koz)	1,459
Contained Ag (koz)	15,721
Average Recovery, Au	75.8%
Average Recovery, Ag	22.1%
Recovered Au (koz)	1,106
Recovered Ag (koz)	3,481
Payable Au (koz)	1,101
Payable Ag (koz)	3,376
Avg Annual Au - LOM (koz / yr)	65
Avg Annual Ag Sales - LOM (koz / yr)	199



19.1.1.2 Costs

- Pre-production period assumes 24 months (Year -1 to Year -2).
- Initial (Growth) and development capital costs total US\$201 million
- Mine life sustaining capital totals US\$343 million
- Final reclamation costs from after year 17 total US\$52.4 million.
- Mine life capital totals US\$596 million.
- Average LOM operating cost is US\$13.03 per tonne stacked.
 - o Open pit operating costs of US\$2.53 per tonne mined (US\$6.37 per tonne stacked). Includes out-of-scope mining operations.
 - o Dewatering operating costs of US\$0.59 per tonne stacked.
 - o Processing operating costs of US\$5.55 per tonne stacked.
 - o Site services & general and administrative (G&A) costs of US\$5.6 million per year for years of full production (LOM average of US\$0.52 per tonne stacked).
- Life of Mine production plan as summarized in Table 13-9.

19.1.1.3 Taxation and Royalties

The federal and state income taxes are summarized in Table 19-2.

Table 19-2: Federal and State Tax Summary

Tax Type	Rate
Federal Corporate Income Tax	21.0%
Nevada Corporate Income Tax	5.0% of federal taxable income
Royalties and Severance Fees	Based on ore extracted (state-regulated).

A total of five NSR royalties apply to future mineral production from portions of the Project. These royalties are summarized in Table 19-3.

Table 19-3: Royalties Summary

Royalty Holder	Royalty Terms
Snyder Syndicate	1% NSR on the 1,044 Sleeper Gold Mine claims (All claims, EXCEPT for ALL MIMI, ALL SP, AL SS, AND ALL BLUE.)
Franco-Nevada U.S. Corporation	2% NSR on minerals produced from all 2,474 claims
Evolving Gold / Quinton Hennigh	2% NSR royalty on all SS and all SP claims.
Dry Lake Placer Association	3% NSR on Dry Lake Placer claims
ICN Resources Ltd.	0.5% NSR on all SS and all SP claims; 1.5% NSR on all Blue claims

For the economic analysis and financial modeling purposes, an overall 3% NSR royalty rate was assumed over the LOM.



19.1.2 Cash Flow Analysis

SLR has prepared its own unlevered after-tax LOM cash flow model based on the information contained in this TRS to confirm the physical and economic parameters of the Project.

The Project’s Base Case economics have been evaluated using the discounted cash flow method, considering annual processed tonnages and the associated gold and silver grades. The process gold and silver recoveries, gold and silver price forecasts, operating costs, refining and transportation charges, royalties, and initial and sustaining capital expenditures were also considered.

The Project, as currently designed, has variations in the mining and processing amounts over its planned 17-year life. These variations are shown in Figure 19-1, Figure 19-2, and Figure 19-3.

Figure 19-1: Mine Production Profile by Material Movement – Base Case

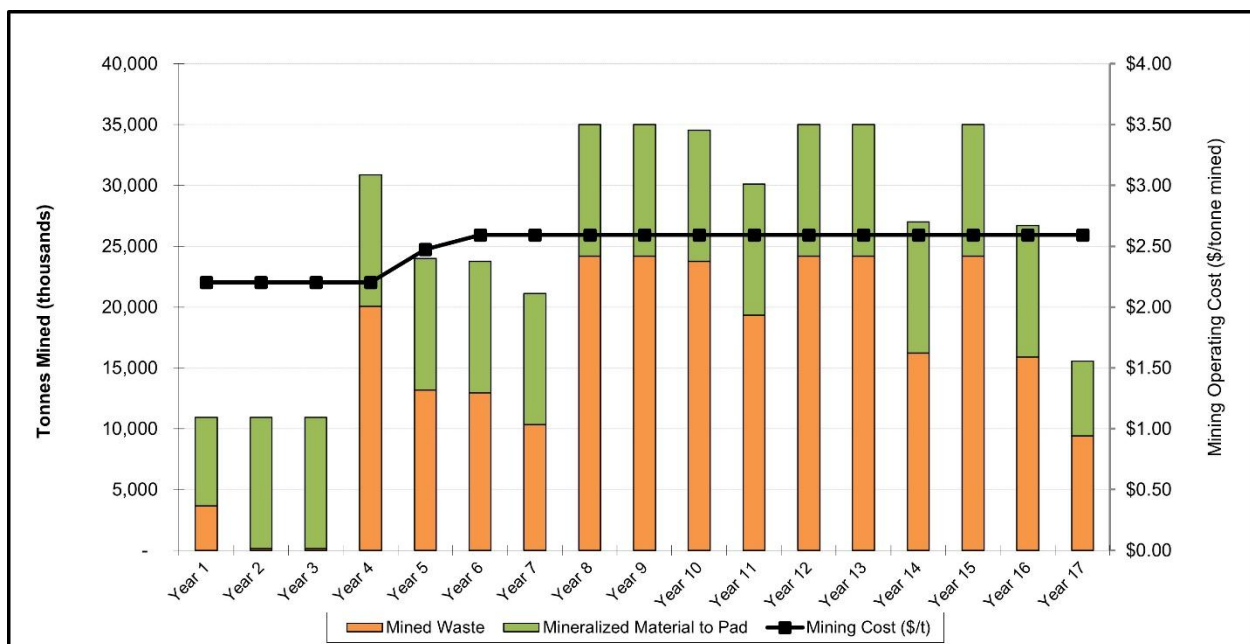


Figure 19-2: Process Production Profile and Head Grade – Base Case

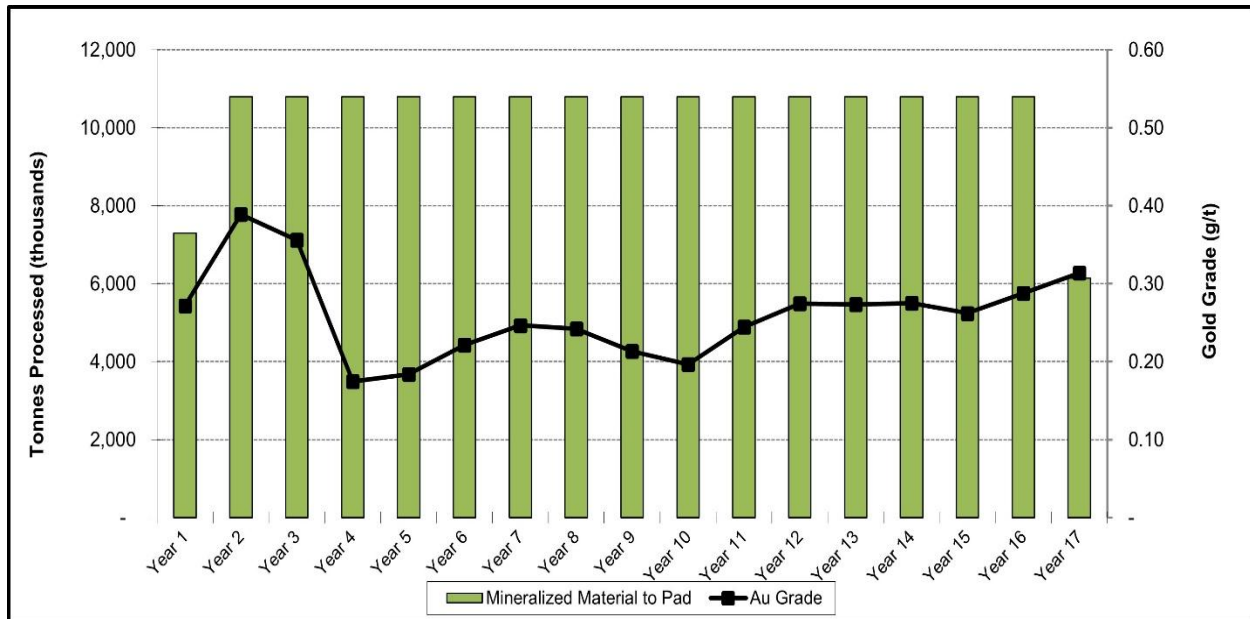
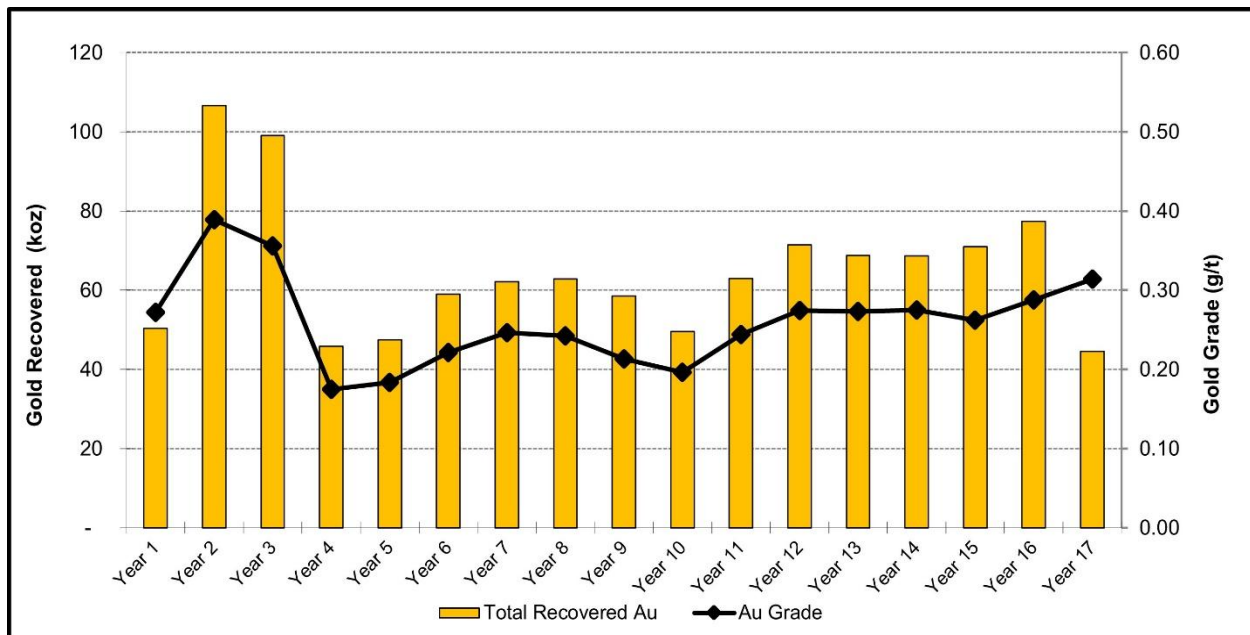


Figure 19-3: Annual Processing Gold Production and Head Grade Profile – Base Case



The economic analysis demonstrates that the Project’s Mineral Resources have reasonable prospects for economic extraction at the LOM net average realized prices of US\$3,618/oz Au and US\$48.70/oz Ag, and with long-term prices of US\$3,600/oz Au and US\$48.00/oz Ag, and that further advancement of Project studies is warranted.

A base discount rate of 8% has been applied in this TRS for the Project. This rate is considered reasonable for evaluating a precious metals project at a preliminary level of project definition, such as Sleeper. Discounted present values of annual cash flows are summed to arrive at the Mine’s Base Case NPV.



Considering the Project’s Base Case on a stand-alone basis, the Project’s pre-tax NPV at an 8% discount rate is approximately US\$505 million, and the pre-tax internal rate of return (IRR) is approximately 51.3%. The Project’s after-tax NPV at an 8% discount is approximately US\$402 million, the after-tax IRR is approximately 44.5%, and the payback period is approximately 1.4 years from the start of production.

The LOM undiscounted pre-tax cash flow totals approximately US\$1,132 million, and the LOM undiscounted after-tax cash flow totals approximately US\$918 million.

SLR has also run a stand-alone economic analysis for the Project using flat resource metal prices of US\$3,100/oz Au and US\$34/oz Ag, and the analysis demonstrates that the Project’s Mineral Resources also have reasonable prospects for economic extraction at these prices.

The Project’s after-tax free cash flow profile and gold payable metal per year are presented in Figure 19-4.

Figure 19-4: Base Case Project After-Tax Metrics Summary

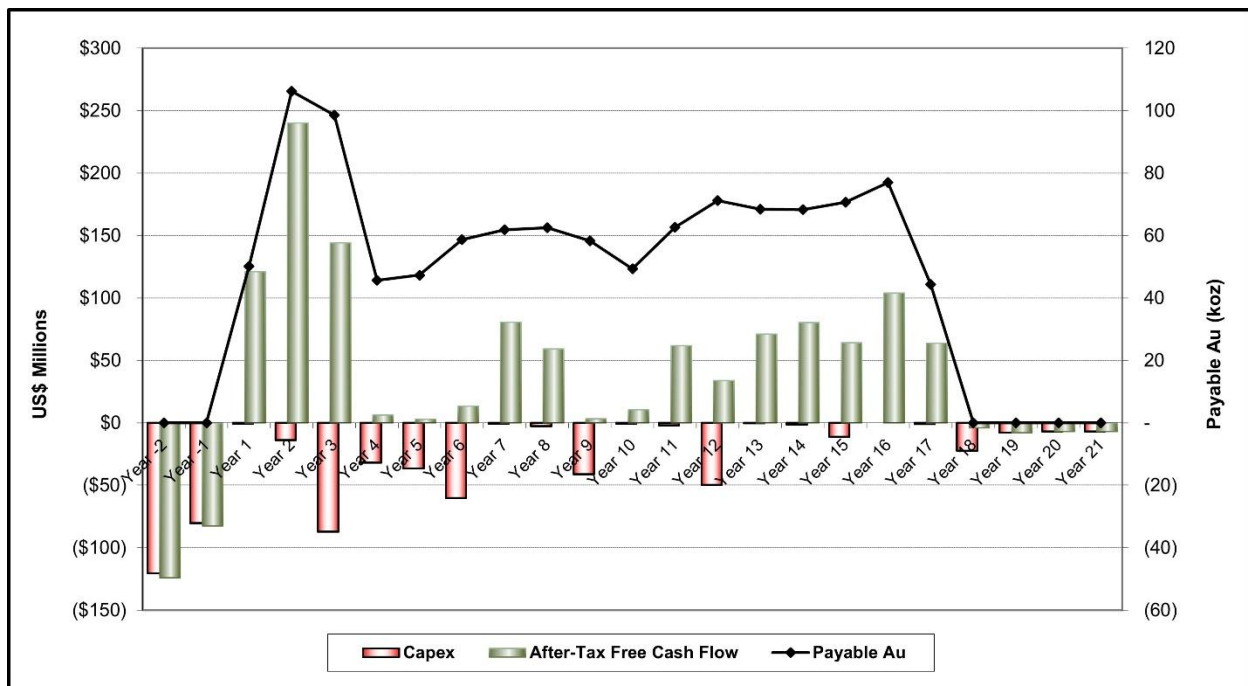


Table 19-4 shows the LOM total metrics for the Sleeper mine as currently designed. Due to the length of the mine life, the full annual cash flow model is presented in Appendix 2 Cash Flow Summaries.

Table 19-4: Total Life of Mine Metrics – Base Case

Item	Units	Base Case Values
Realized Market Prices		
Au Price	US\$/oz	\$3,618
Ag Price	US\$/oz	\$48.70
Payable Gold	koz	1,101
Payable Silver	koz	3,376



Item	Units	Base Case Values
Total Gross Revenue	US\$ million	4,147
Mining Cost	US\$ million	(1,117)
Dewatering Costs	US\$ million	(104)
Process Cost	US\$ million	(974)
G & A Cost	US\$ million	(92)
Refining/Freight	US\$ million	(8)
Royalties	US\$ million	(124)
Total Operating Costs	US\$ million	(2,418)
Operating Margin (EBITDA)	US\$ million	1,728
Federal Income Tax	US\$ million	(134)
State Tax - Nevada Mining Tax	US\$ million	(80)
Working Capital	US\$ million	0
Operating Cash Flow	US\$ million	1,514
Development (Initial) Capital	US\$ million	(201)
Sustaining Capital	US\$ million	(343)
Closure/Reclamation Capital	US\$ million	(52)
Total Capital	US\$ million	(596)
Pre-tax Free Cash Flow	US\$ million	1,132
Pre-tax NPV @ 5%	US\$ million	670
Pre-tax NPV @ 8%	US\$ million	505
Pre-Tax IRR	%	51.3%
Pre-Tax Payback	years	1.3
After-tax Free Cash Flow	US\$ million	918
After-tax NPV @ 5%	US\$ million	539
After-tax NPV @ 8%	US\$ million	402
After-Tax IRR	%	44.5%
After-Tax Payback	years	1.4

Note: Numbers may not add due to rounding.

The Project's World Gold Council Adjusted Operating Cost (AOC) net of Ag by-product credits is US\$2,048/oz Au payable. The mine life sustaining capital costs are US\$359/oz Au payable, for an All-in Sustaining Cost (AISC) net of Ag by-products credits of US\$2,407/oz Au payable.

The average annual gold sales during operations are approximately 64,746 payable ounces. Table 19-5 shows the AISC build-up.



Table 19-5: Base Case All-in Sustaining Costs Composition

Item	Total LOM (\$ million)	Unit Cost (\$/oz Au)
Mining	1,117	1,015
Dewatering	104	94
Process	974	885
Site G&A	92	83
Subtotal Site Costs	2,286	2,077
Refining/Freight	8	8
Mining Royalties	124	113
Total Cash Costs before by-product credits	2,418	2,197
Ag By-Product Credit	(164)	(149)
Total Cash Costs net of by-product credits	2,254	2,048
Sustaining Capital Cost	343	311
Closure/Reclamation Costs	52	48
Total Sustaining Costs	395	359
Total All-in Sustaining Costs	2,649	2,407

Note: Numbers may not add due to rounding.

The AISC calculated in the cash flow analysis reflects the benefit of low-cost ounces already stacked on the heap leach pads, compared to AISC estimated in a steady-state model that assumes current input costs. Much of Sleeper's near-term production comes from material mined and placed in prior years, when gold prices, fuel, and consumable costs were lower. These ounces require minimal additional spending to recover, resulting in lower realized cash costs. As these legacy ounces are depleted and replaced with newly mined material, unit costs are expected to gradually normalize toward long-term levels.

19.1.3 Sensitivity Analysis

The Project's Base Case risks can be identified in both economic and non-economic terms. Key economic risks were examined by running cash flow sensitivities:

- Metal prices
- Head grade
- Metallurgical Recovery
- Operating costs
- Pre-production and sustaining capital costs

Where possible, the after-tax NPV 8% sensitivities relative to the Base Case have been calculated for -20% to +20% variations in head grade and recovery, and -20% to +30% in metal prices. Operating and capital cost sensitivities have been calculated at -15% to +35% variations. The sensitivities are shown in Table 19-6 and Figure 19-5

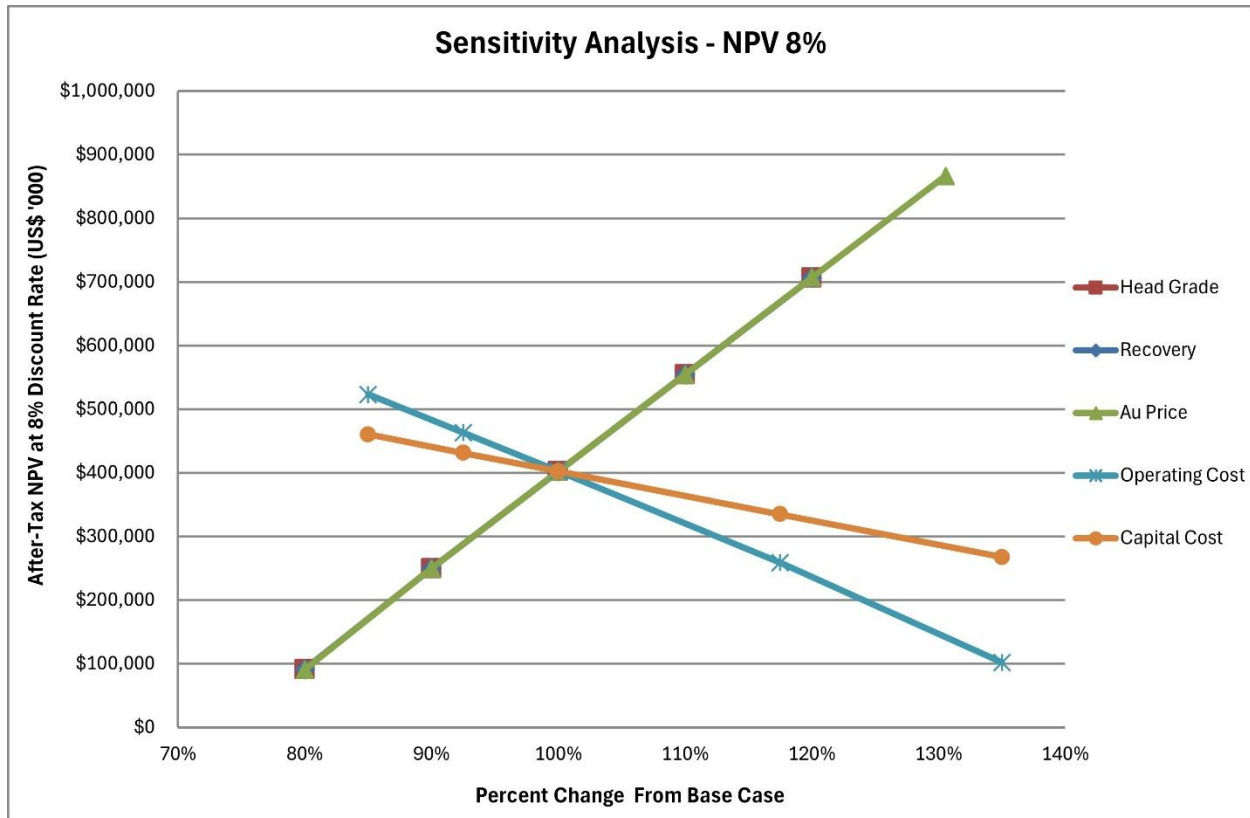


Table 19-6: Base Case After-Tax Sensitivity Analyses

Variance	Head Grade (g/t Au)	NPV at 8% (US\$ 000)
80%	0.21	91,329
90%	0.23	249,814
100%	0.26	402,353
110%	0.28	554,310
120%	0.31	706,171
Variance	Recovery (% Au)	NPV at 8% (US\$ 000)
80%	60.7%	91,329
90%	68.2%	249,814
100%	75.8%	402,353
110%	83.4%	554,310
120%	91.0%	706,171
Variance	Metal Prices (US\$/oz Au)	NPV at 8% (US\$ 000)
80%	\$2,880	90,637
90%	\$3,240	249,505
100%	\$3,600	402,353
110%	\$3,960	554,614
131%	\$4,700	866,553
Variance	Operating Costs (US\$/t)	NPV at 8% (US\$ 000)
85%	\$11.07	523,205
93%	\$12.05	462,780
100%	\$13.03	402,353
118%	\$15.31	259,020
135%	\$17.59	102,091
Variance	Capital Costs (US\$ 000)	NPV at 8% (US\$ 000)
85%	\$506,652	460,155
93%	\$551,357	431,254
100%	\$596,062	402,353
118%	\$700,372	334,916
135%	\$804,683	267,480



Figure 19-5: Base Case After-Tax Sensitivity Analysis



19.2 Alternative Case - Measured and Indicated Only

19.2.1 Economic Criteria

The Alternative Case assumes a production schedule based exclusively on Measured and Indicated Mineral Resources, resulting in a mineralized material inventory of 62.4 Mt and a projected mine life of seven years. A summary of the Measured and Indicated Only Case criteria is provided below.

19.2.1.1 Revenue

- Mine life: 7 years.
- 30,000 tpd mineralized material stacked (approximately 10.8 Mt per year), average stacked grade of 0.27 g/t Au and silver grade of 3.83 g/t Ag (ROM, crushed, and stockpile mine plan).
- Mine life averages 58,500 ounces per year of gold recovered and 200,000 ounces per year of silver recovered from the mine plan, with LOM stacked process gold recovery averaging 74.3% and silver recovery averaging 18.1%.
- Total 410 koz of gold recovered, and 1,396 koz of silver recovered over the LOM operation.
- Gold and silver payable at the refinery are assumed at 99.95% Au payable and 97% Ag payable



- Gold and silver prices are based on analyst consensus price forecasts from the end of March 2026. For the economic analysis was assumed:
 - o Y1: US\$4,000/oz Au and US\$59.00/oz Ag
 - o Y2 to Y7: US\$3,600/oz Au and US\$48.00/oz Ag
 - o Resulting in LOM net realized prices of:US\$3,622/oz Au and US\$48.00/oz Ag
- Net Smelter Return (NSR) includes doré refining, transport, and insurance costs.
- NSR royalty assumed at 3%. The property is subject to different royalties between 0.5% and 3%, and for modeling purposes was assumed at an overall 3%
- Revenue is recognized at the time of gold and silver production.
- Non-cash inventory adjustments are not included in the SLR cash flow model.
- LOM net revenue is US\$1,493 million (after royalty, and transportation, and refining charges).

Table 19-7: Sleeper Alternative Case Production Physicals Summary

Physicals	Value
Total Mineralized Material Stacked (kt)	62,447
Max Process Rate (tpd)	30,000
Au Head Grade (g/t)	0.27
Ag Head Grade (g/t)	3.83
Contained Au (koz)	552
Contained Ag (koz)	7,697
Average Recovery, Au	74.3%
Average Recovery, Ag	18.1%
Recovered Au (koz)	410
Recovered Ag (koz)	1,396
Payable Au (koz)	408
Payable Ag (koz)	1,354
Avg Annual Au Sales - LOM (koz / yr) – full production	64
Avg Annual Ag Sales - LOM (koz / yr) – Full production	218

19.2.1.2 Costs

- Pre-production period assumes at 24 months (Year -1 to Year -2).
- Initial (Growth) and development capital costs total US\$335 million.²
- Mine life sustaining capital totals US\$120 million
- Final reclamation costs from after year 7 total US\$18.7 million.

² Note that, in the Alternative Case, only in situ Measured and Indicated Mineral Resources are included in the mining inventory. The existing waste dumps are not included in the LOM plan for the Alternative Case because they are currently classified as Inferred Mineral Resources. As dewatering of the in situ Mineral Resources must start before mining, the rapid infiltration basins cost and the dewatering costs are Initial Capital Costs for the Alternative Case rather than Sustaining Capital as in the Base Case.



- Mine life capital totals US\$473 million.
- Average LOM operating cost is US\$11.87 per tonne stacked.
 - Open pit operating costs of US\$2.59 per tonne mined (US\$5.03 per tonne stacked). Includes out-of-scope mining operations.
 - Dewatering operating costs of US\$0.73 per tonne stacked.
 - Processing operating costs of US\$5.55 per tonne stacked.
 - Site services & general and administrative (G&A) costs of US\$5.6 million per year for years of full production (LOM average of US\$0.56 per tonne stacked).

19.2.1.3 Taxation and Royalties

The federal and state income taxes are summarized in Table 19-8

Table 19-8: Federal and State Tax Summary

Tax Type	Rate
Federal Corporate Income Tax	21.0%
Nevada Corporate Income Tax	5.0% of federal taxable income
Royalties and Severance Fees	Based on ore extracted (state-regulated).

A total of five NSR royalties apply to future mineral production from portions of the Project. These royalties are summarized in Table 19-9.

Table 19-9: Royalties Summary

Royalty Holder	Royalty Terms
Snyder Syndicate	1% NSR on the 1,044 Sleeper Gold Mine claims (All claims, EXCEPT for ALL MIMI, ALL SP, AL SS, AND ALL BLUE.)
Franco-Nevada U.S. Corporation	2% NSR on minerals produced from all 2,474 claims
Evolving Gold / Quinton Hennigh	2% NSR royalty on all SS and all SP claims.
Dry Lake Placer Association	3% NSR on Dry Lake Placer claims
ICN Resources Ltd.	0.5% NSR on all SS and all SP claims; 1.5% NSR on all Blue claims

For the economic analysis and financial modeling purposes, an overall 3% NSR royalty rate was assumed over the LOM.

19.2.2 Cash Flow Analysis

SLR has prepared its own unlevered after-tax LOM cash flow model based on the information contained in this TRS to confirm the physical and economic parameters of the Project.

The Project's Alternative Case economics have been evaluated using the discounted cash flow method, considering annual processed tonnages and the associated gold and silver grades. The process gold and silver recoveries, gold and silver price forecasts, operating costs, refining and transportation charges, royalties, and initial and sustaining capital expenditures were also considered.



The Project, as currently designed, has variations in the mining and processing amounts over its planned 7-year life. These variations are shown in Figure 19-6, Figure 19-7, and Figure 19-8.

Figure 19-6: Mine Production Profile by Material Movement – Alternative Case

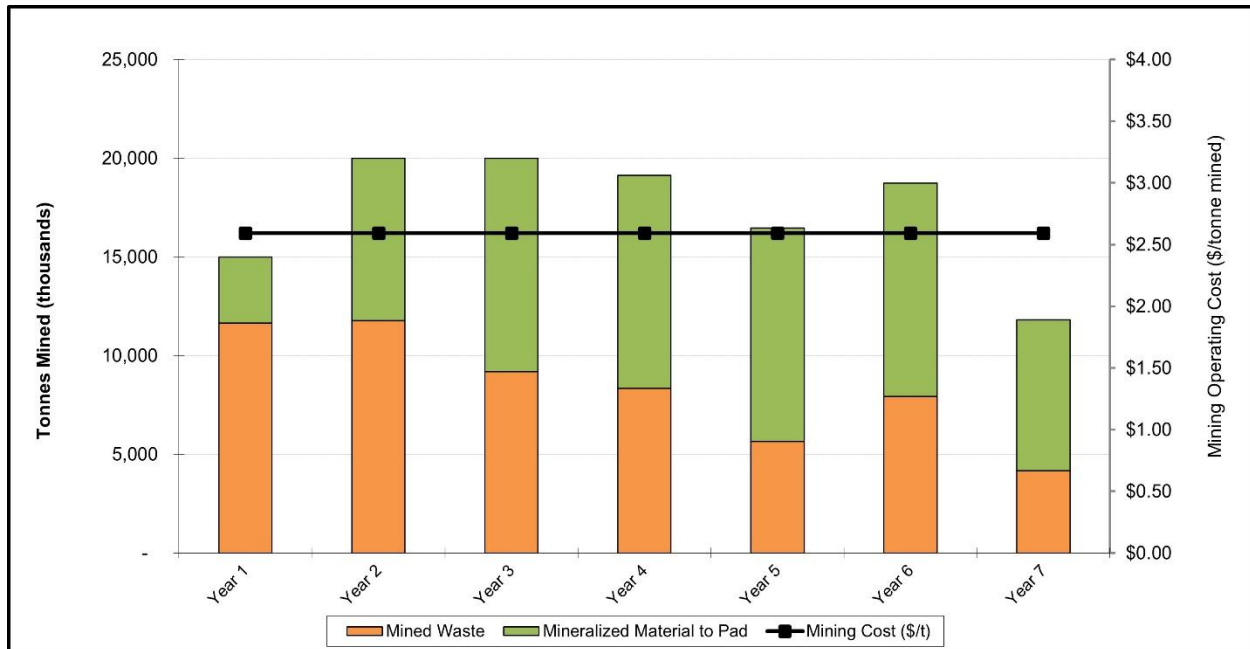


Figure 19-7: Process Production Profile and Head Grade – Alternative Case

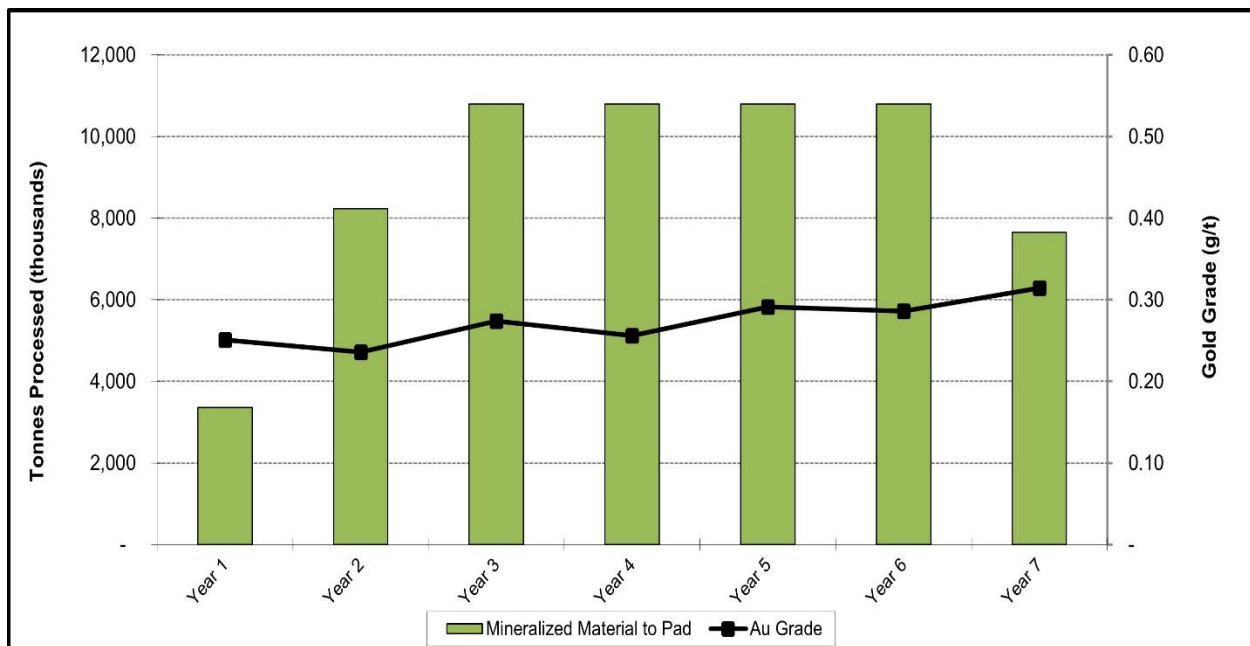
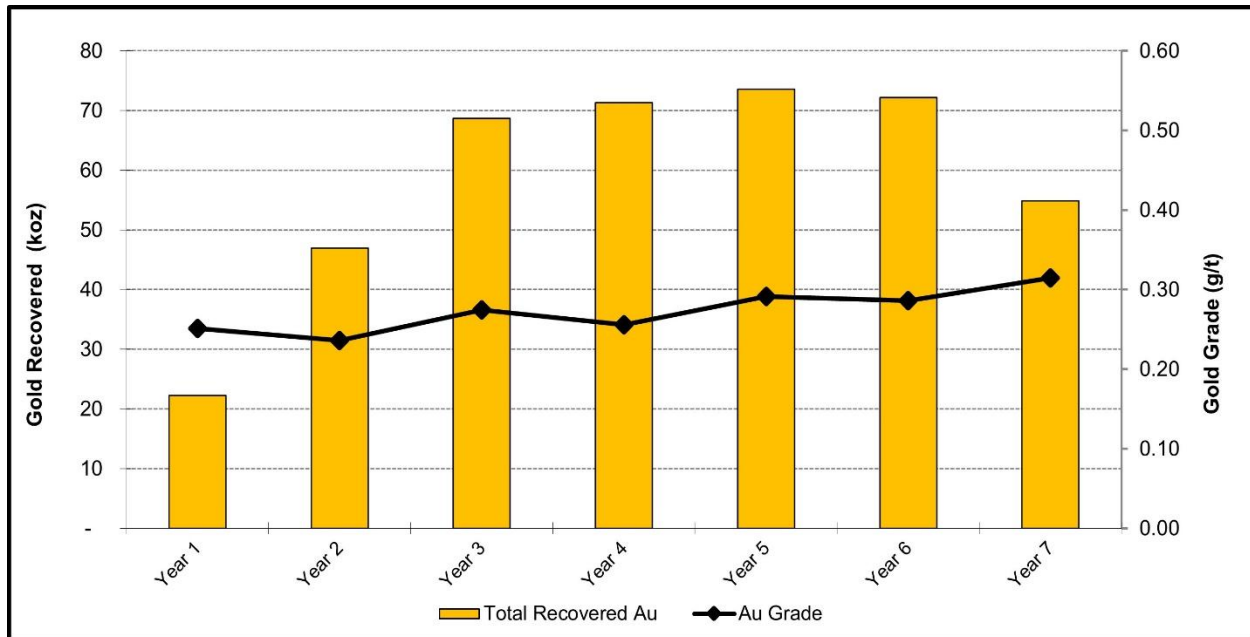


Figure 19-8: Annual Processing Gold Production and Head Grade Profile



The economic analysis demonstrates that the Project’s Mineral Resources have reasonable prospects for economic extraction, at the LOM net average realized prices of US\$3,622/oz Au and US\$48.40/oz Ag, with long-term prices of US\$3,600/oz Au and US\$48.00/oz Ag, and that further advancement of Project studies is warranted.

A base discount rate of 8% has been applied in this TRS for the Project. This rate is considered reasonable for evaluating a precious metals project at a preliminary level of project definition, such as Sleeper. Discounted present values of annual cash flows are summed to arrive at the Mine’s Base Case NPV.

Considering the Project’s Alternative Case on a stand-alone basis, the Project’s pre-tax NPV at an 8% discount rate is approximately US\$59 million, and the pre-tax internal rate of return (IRR) is approximately 11.5%. The Project’s after-tax NPV at an 8% discount is approximately US\$31 million, the after-tax IRR is approximately 9.9%, and the payback period is approximately 4.9 years from the start of production.

The LOM undiscounted pre-tax cash flow totals approximately US\$279 million, and the LOM undiscounted after-tax cash flow totals approximately US\$232 million.

The Project’s after-tax free cash flow profile and gold payable metal per year are presented in Figure 19-9.



Figure 19-9: Alternative Case Project After-Tax Metrics Summary

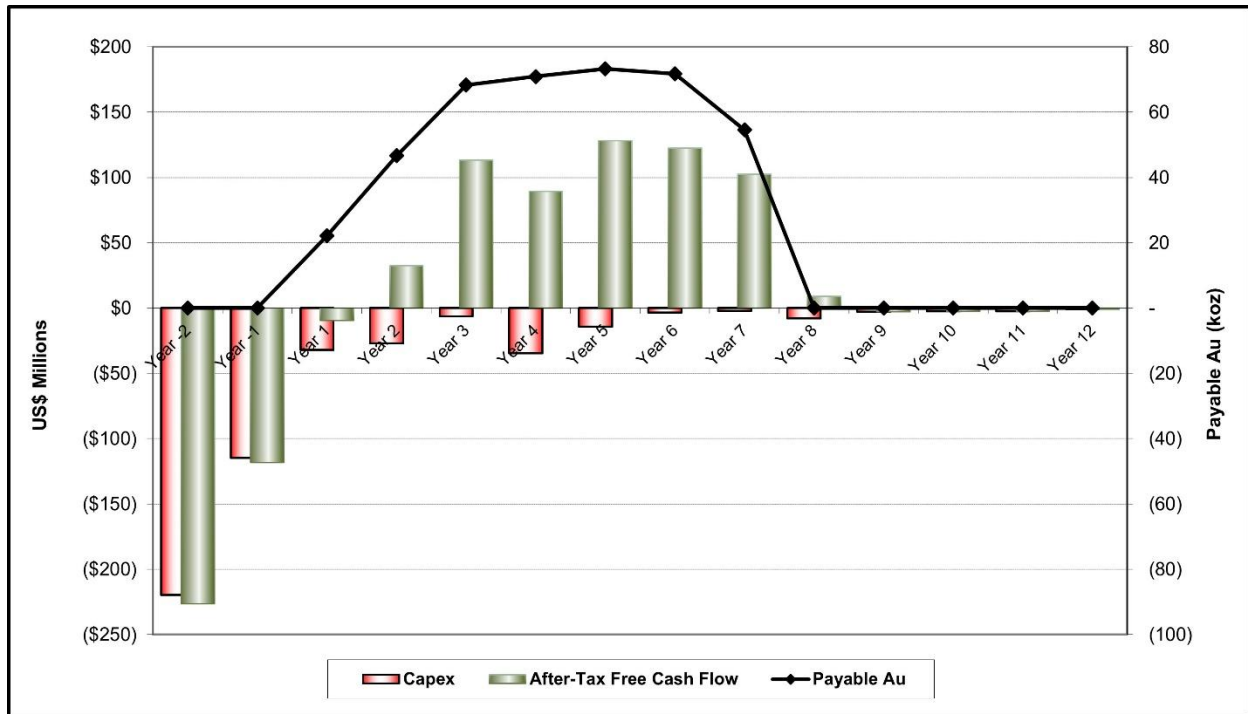


Table 19-10 shows the LOM total metrics for the Project’s Alternative Case. The full annual cash flow model is presented in Appendix 2 Cash Flow Summaries.

Table 19-10: Total Life of Mine Metrics – Alternative Case (Measured and Indicated Only)

Item	Units	Base Case Values
Realized Market Prices		
Au Price	US\$/oz	\$3,622
Ag Price	US\$/oz	\$48.40
Payable Gold	koz	408
Payable Silver	koz	1,354
Total Gross Revenue	US\$ million	1,542
Mining Cost	US\$ million	(314)
Dewatering Costs	US\$ million	(45)
Process Cost	US\$ million	(347)
G & A Cost	US\$ million	(35)
Refining/Freight	US\$ million	(3)
Royalties	US\$ million	(46)
Total Operating Costs	US\$ million	(790)
Operating Margin (EBITDA)	US\$ million	752
Federal Income Tax	US\$ million	(12)



Item	Units	Base Case Values
State Tax - Nevada Mining Tax	US\$ million	(34)
Working Capital	US\$ million	0
Operating Cash Flow	US\$ million	705
Development (Initial) Capital	US\$ million	(335)
Sustaining Capital	US\$ million	(120)
Closure/Reclamation Capital	US\$ million	(19)
Total Capital	US\$ million	(473)
Pre-tax Free Cash Flow	US\$ million	279
Pre-tax NPV @ 5%	US\$ million	124
Pre-tax NPV @ 8%	US\$ million	59
Pre-Tax IRR	%	11.5%
Pre-Tax Payback	years	4.7
After-tax Free Cash Flow	US\$ million	232
After-tax NPV @ 5%	US\$ million	91
After-tax NPV @ 8%	US\$ million	31
After-Tax IRR	%	9.9%
After-Tax Payback	years	4.9
Note:	Numbers may not add due to rounding.	

The Project's World Gold Council Adjusted Operating Cost (AOC) net of Ag by-product credits is US\$1,778/oz Au payable. The mine life sustaining capital costs are US\$339/oz Au payable, for an All-in Sustaining Cost (AISC) net of Ag by-products credits of US\$2,117/oz Au payable.

The average annual gold sales during operations are approximately 64,267 payable ounces.

Table 19-11 shows the AISC build-up.

Table 19-11: Alternative Case All-in Sustaining Costs Composition

Item	Total LOM (\$ million)	Unit Cost (\$/oz Au)
Mining	314	770
Dewatering	45	111
Process	347	850
Site G&A	35	86
Subtotal Site Costs	741	1,817



Item	Total LOM (\$ million)	Unit Cost (\$/oz Au)
Refining/Freight	3	8
Mining Royalties	46	113
Total Cash Costs before by-product credits	790	1,938
Ag By-Product Credit	(65)	(161)
Total Cash Costs net of by-product credits	725	1,778
Sustaining Capital Cost	120	293
Closure/Reclamation Costs	19	46
Total Sustaining Costs	138	339
Total All-in Sustaining Costs	863	2,117

Note: Numbers may not add due to rounding.

19.2.3 Sensitivity Analysis

The project's Alternative Case risks can be identified in both economic and non-economic terms. Key economic risks were examined by running cash flow sensitivities:

- Metal prices
- Head grade
- Metallurgical Recovery
- Operating costs
- Pre-production and sustaining capital costs

Where possible, the after-tax NPV 8% sensitivities relative to the Alternative Case have been calculated for -20% to +20% variations in head grade and recovery, and -20% to +30% in metal prices. Operating and capital cost sensitivities have been calculated at -15% to +35% variations. The sensitivities are shown in Table 19-12 and Figure 19-10.

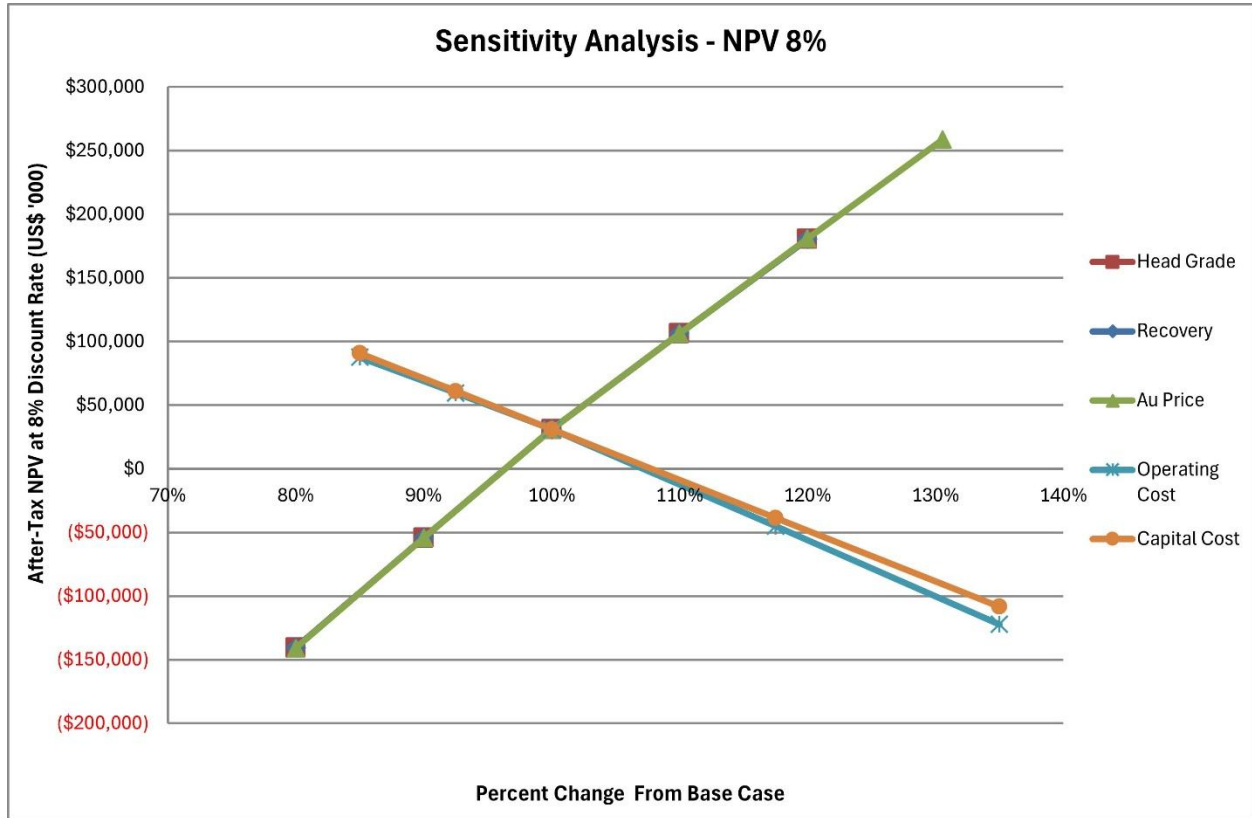


Table 19-12: Alternative Case After-Tax Sensitivity Analyses

Variance	Head Grade (g/t Au)	NPV at 8% (US\$000)
80%	0.22	(140,512)
90%	0.25	(54,187)
100%	0.27	31,106
110%	0.30	106,275
120%	0.33	180,559
Variance	Recovery (% Au)	NPV at 8% (US\$000)
80%	59.4%	(140,512)
90%	66.9%	(54,187)
100%	74.3%	31,106
110%	81.7%	106,275
120%	89.2%	180,559
Variance	Metal Prices (US\$/oz Au)	NPV at 8% (US\$000)
80%	\$2,880	(140,868)
90%	\$3,240	(54,363)
100%	\$3,600	31,106
110%	\$3,960	106,424
131%	\$4,700	258,552
Variance	Operating Costs (US\$/t)	NPV at 8% (US\$000)
85%	\$10.09	87,662
93%	\$10.98	59,481
100%	\$11.87	31,106
118%	\$13.94	(44,879)
135%	\$16.02	(122,212)
Variance	Capital Costs (US\$000)	NPV at 8% (US\$000)
85%	\$401,924	90,847
93%	\$437,387	60,977
100%	\$472,851	31,106
118%	\$555,600	(38,591)
135%	\$638,349	(108,288)



Figure 19-10: Alternative Case After-Tax Sensitivity Analysis



20.0 Adjacent Properties

The Project is located within the Sleeper Mining District of Humboldt County, Nevada, an area that hosts several past-producing precious-metal deposits and active exploration properties.

Several exploration properties occur within a 10 km radius of the Project, targeting similar epithermal mineralization hosted in Miocene volcanic rocks. Historical exploration programs in the district have included geologic mapping, geochemical sampling, geophysical surveys, and drilling.

Publicly available information indicates that these adjacent properties host epithermal gold-silver mineralization genetically related to regional volcanic and structural systems.

The SLR QP has not independently verified this information, and this information is not necessarily indicative of the mineralization at the Sleeper Gold Project.



21.0 Other Relevant Data and Information

21.1 Sleeper PFS - Project Overview and Execution Philosophy

The Project Execution Plan (PEP) defines the strategy for advancing the Project from the current S-K 1300 IA stage through Pre-Feasibility Study (PFS), permitting, construction, and into operations. The development scenario evaluated in the IA consists of a 30,000 tpd open pit mining operation feeding a probable processing scenario comprising a crush–agglomerate–heap-leach process with Merrill-Crowe recovery.

The scope of the IA, and therefore this PEP, is limited to the reprocessing of waste dump material and the mining of in situ oxide and mixed mineralization. Processing will occur on a single-use heap leach pad designed in accordance with Nevada regulatory requirements.

The execution philosophy is based on a practical and capital-efficient restart strategy, incorporating the following principles:

- Low initial capital intensity with contractor mining and modular process infrastructure. This approach minimizes upfront fleet purchases and reduces financing requirements during early project development.
- Immediate advancement to a PFS, with overlapping technical, environmental, and permitting workstreams to accelerate the overall project schedule.
- Maximizing the use of existing disturbed areas, including waste rock dumps and previously impacted process areas, to streamline permitting and reduce environmental footprint.
- Parallel advancement of engineering, metallurgical test work, and environmental baseline programs to avoid sequential delays.
- Maintaining optionality for future expansion, including potential treatment of sulfide material under a separate development scenario.

21.2 Project Development Strategy

21.2.1 Development Pathway

The Project will advance through a structured, but overlapping, series of development phases designed to minimize schedule duration while maintaining technical rigor:

- PFS Phase (Immediate Initiation): Comprehensive technical evaluation, including updated mine planning, metallurgical test work, cost estimation, and trade-off studies.
- Permitting and Baseline Study Advancement: Collection of environmental baseline data and preparation of regulatory submissions. This phase represents the Project's critical path.
- Definitive Engineering: Advancement of engineering design to a level sufficient to support construction, procurement, and cost certainty.
- Early Works and Site Preparation: Initial site activities, including relocation of existing infrastructure, earthworks, and utility installation.
- Construction and Commissioning: Development of process facilities, heap leach pad, ponds, and supporting infrastructure, followed by commissioning.



- Ramp-up to Steady-State Operations: Progressive increase to the design throughput of approximately 30,000 tpd.

The Company intends to initiate the PFS immediately and pursue an execution strategy targeting first production approximately 24 months from initiation, subject to permitting timelines and technical outcomes.

21.3 Workstreams and Scope of Activities

21.3.1 Geological, Resource, and Drilling Programs

A comprehensive drilling and sampling program will be implemented to support resource confidence, metallurgical characterization, and engineering design. The program is designed to address both waste dump material and in situ oxide and mixed mineralization.

Key programs are listed:

- Sonic and reverse circulation (RC) drilling of waste dumps, TSF, and heap leach pads to characterize grade distribution, material variability, and bulk density.
- RC drilling of in situ oxide and mixed material to support resource classification upgrades and mine planning.
- Twin drilling and QA/QC validation to confirm historical data reliability and ensure compliance with reporting standards.
- Bulk sampling to provide representative material for metallurgical test work and variability analysis of waste dumps, heap leach pads and TSF.

The outputs of these programs will support updates to the Mineral Resource Estimate, development of a geometallurgical model, and refinement of mine planning inputs for the PFS.

21.3.2 Metallurgical Test Work

Metallurgical test work is a critical component of technical risk reduction, particularly given the presence of mixed oxides and transition materials, as well as reprocessed waste rock dumps.

The metallurgical program will include the following:

- Bottle roll testing across all defined material domains to establish baseline recoveries and reagent consumption.
- Column leach testing at multiple crush sizes to evaluate heap leach performance and optimize particle size distribution.
- Agglomeration optimization to improve permeability and leach kinetics for fine-grained or clay-rich materials.
- Permeability testing to assess heap stability and solution flow characteristics.
- Cyanide consumption and reagent optimization to define operating cost inputs.
- Gold and silver recovery variability testing to establish recovery models by domain.
- Evaluation of gravity recovery potential, where applicable.

Deliverables will include recovery models by domain, heap leach design criteria, reagent consumption forecasts, and inputs for operating cost estimation.



21.3.3 Mining and Production Planning

Mining operations will be executed by a contractor to minimize initial capital requirements and provide operational flexibility during the early years of production.

Key components of the mining plan include:

- Open pit optimization and shell selection based on updated economic and metallurgical inputs.
- Mine sequencing to prioritize oxide and mixed material and optimize cash flow.
- Waste dump reclaim sequencing integrated with in situ mining operations.
- Haulage design, including process feed haul distances of approximately 1.5 km to 4.5 km and waste haul distances of approximately 2.5 km.
- Development of a production schedule supporting approximately 30,000 tpd of material processing.

The mining contractor is expected to supply and operate a fleet comprising 150 t to 200 t class haul trucks, hydraulic excavators, loaders, and support equipment. The Owner's team will provide oversight, grade control, and reconciliation.

21.3.4 Process Design and Infrastructure

The process flowsheet is based on conventional and well-established technologies suitable for oxide and mixed gold mineralization.

Process plant components include:

- Primary crushing to achieve the target particle size for heap leaching.
- Agglomeration, if required, to improve heap permeability and recovery.
- Heap leach stacking using conveyor or truck stacking systems.
- Solution management systems, including pregnant and barren solution circuits.
- Merrill-Crowe recovery plant for gold and silver extraction.
- Refining facilities for doré production.

Infrastructure components include:

- Single-use heap leach pad designed with double-liner systems consistent with Nevada regulatory requirements.
- Solution ponds, including pregnant, barren, and stormwater ponds.
- Recovery/Merrill-Crowe processing facilities.
- Power supply infrastructure, which may include grid connection or hybrid systems.
- Water supply and distribution systems.
- Maintenance facilities, including relocation of the existing truck shop affected by pit expansion.
- Site access roads, haul roads, and support infrastructure.



21.3.5 Water Management and Dewatering

SLR considers water management to be a key operational and permitting consideration for the Project. A comprehensive program will be implemented to define water availability, manage process water, and ensure compliance with regulatory requirements.

Key components include:

- Groundwater baseline data collection and pump testing to define aquifer characteristics.
- Development of a groundwater model to support dewatering design and water balance calculations.
- Evaluation of pit dewatering and discharge requirements.
- Preparation of a detailed process water balance.
- Design of heap leach solution management systems, including containment and recycling.
- Stormwater management systems to control runoff and protect water quality.

Water supply is expected to be sourced from a combination of groundwater and recycled process water, subject to permitting and availability.

21.3.6 Environmental Baseline and Permitting

Permitting represents the critical path for Project development and will be advanced in parallel with technical studies.

The anticipated environmental baseline studies that will be required are listed:

- Surface water quality and hydrology.
- Groundwater quality and levels.
- Air quality and emissions.
- Flora and fauna surveys.
- Cultural and archaeological resource assessments.
- Geochemical characterization, including acid rock drainage and metal leaching potential.
- Meteorological data collection.

The permitting strategy includes the following steps.

- Submission of a Notice of Intent (NOI) to the BLM.
- Advancement through the EA process, or EIS process if required.
- Modification of existing Plans of Operations and permits.
- Coordination with relevant agencies, including the BLM, NDEP, and Nevada Division of Water Resources.

A key advantage of the Project is that existing disturbance areas, including waste rock dumps, heap leach pads, and tailings storage facilities, remain bonded and permitted. This condition is expected to facilitate a brownfields redevelopment pathway and reduce permitting complexity.



21.3.7 Project Organization and Execution Model

21.3.7.1 Execution Model

The Project will be executed using a combination of Owner's team oversight, contractor execution, and specialist consulting support.

- Owner's Team: Responsible for overall project management, technical oversight, permitting coordination, and stakeholder engagement.
- EPCM/EPC Contractor: Responsible for engineering, procurement, and construction management or execution.
- Mining Contractor: Responsible for all mining operations, including drilling, blasting, loading, and hauling.
- Specialist Consultants: Provide expertise in metallurgy, geotechnical engineering, environmental studies, and hydrogeology.

21.3.7.2 Staffing Philosophy

The staffing approach will be scaled to the project phase:

- Lean Owner's team during PFS and early development.
- Increased staffing during construction and commissioning.
- Transition to steady-state operational staffing levels during production.

No on-site camp is required, as the Project will utilize a local or regional workforce.

21.4 Schedule and Critical Path

21.4.1 Overall Timeline

The Project schedule is structured to allow overlapping activities and accelerated development:

- PFS initiation: Immediate.
- Permitting and baseline data collection: Approximately 12 to 36 months.
- Engineering and procurement: Approximately 12 to 18 months, overlapping with permitting.
- Construction: Approximately 9 to 12 months.
- Commissioning and ramp-up: Several months following construction completion.

The target for first gold production is approximately 24 months from project initiation, subject to permitting approvals and technical validation.

21.4.2 Critical Path Elements

The primary critical path elements include:

- Completion of environmental baseline data collection.
- Progression through the BLM permitting process, including NOI submission, EA/EIS preparation, and Record of Decision.



- Water rights acquisition and discharge permitting.
- Resolution of metallurgical variability and confirmation of recovery assumptions.

21.5 Procurement and Contracting Strategy

21.5.1 Mining

Mining will be conducted by a contractor under a unit-rate contract, typically expressed in US dollars per cubic meter of mined material. Contracts will include provisions for standard mining activities and rate schedules for out-of-scope work.

21.5.2 Process and Infrastructure

Major process equipment and infrastructure components will be procured through competitive bidding processes. Key items include crushers, Merrill-Crowe plant components, pumps, and piping systems.

Anticipated bulk consumables and services contracts and agreements are listed:

- Diesel fuel supply contracts
- Cyanide supply agreements
- Lime and other reagents
- Grinding media, if required

21.5.3 Refining and Sales

Gold and silver doré will be transported to third-party refineries under standard industry contracts. Transportation, security, and refining arrangements will be structured to align with industry norms. The potential use of hedging or forward sales will be evaluated during the PFS.

21.6 Sulfide Mineralization – Future Work Programs

Although sulfide mineralization is included within the Mineral Resource inventory, it is explicitly excluded from the economic analysis presented in this Initial Assessment. The sulfide material represents a potential future development opportunity; however, additional technical studies, test work, and engineering are required to determine an appropriate processing pathway and economic viability. Sulfides have been identified in the heap leach pads, the TSF, and are found in the in situ material.

The following work programs are recommended to advance understanding of sulfide mineralization and support future evaluation:

21.6.1 Geological and Resource Definition

Additional drilling and geological modeling will be required to improve confidence in the sulfide Mineral Resources and support potential conversion to higher confidence categories. Key activities include:

- Infill drilling to improve spatial continuity and grade confidence within sulfide domains.
- Extension drilling to evaluate down-dip and along-strike mineralization potential.



- Detailed geological modeling to refine lithological, structural, and alteration controls on sulfide mineralization.
- Density measurements and validation to support tonnage estimates.

These efforts will support a future Mineral Resource update and will be instrumental in the conversion to Mineral Reserves and provide a foundation for mine planning studies specific to sulfide material.

21.6.2 Metallurgical Test Work

Sulfide mineralization at Sleeper is not amenable to conventional heap leaching and will require alternative processing methods. A staged metallurgical program is required to evaluate viable treatment options.

Recommended test work includes:

- Mineralogical and deportment studies to define gold association (e.g., refractory vs. free milling components).
- Gravity concentration studies.
- Flotation testing to evaluate concentrate grade, recovery, and mass pull.
- Diagnostic leach testing to assess gold liberation characteristics.
- Evaluation of oxidation processes, including pressure oxidation (POX), bio-oxidation, or roasting, where applicable.
- Cyanidation testing of flotation concentrates and/or oxidized products.

The objective of this program is to identify a technically viable and economically competitive flowsheet for sulfide processing.

21.6.3 Process and Infrastructure Trade-Off Studies

Development of sulfide mineralization will require significant additional infrastructure compared to the oxide heap-leach scenario. Trade-off studies should evaluate:

- Standalone sulfide processing facility versus integration with existing oxide infrastructure.
- Processing options, gravity concentration circuit, including flotation with concentrate sale, flotation with on-site oxidation, or whole ore processing.
- Consideration of POX Toll Mill for flotation concentrate
- Capital and operating cost implications of each processing route.
- Power requirements and supply options for high-energy processing circuits.
- Water demand and additional permitting requirements.

These studies will define the preferred development pathway and associated capital intensity.

21.7 Risk Management

21.7.1 Key Risks

Key project risks are listed:



- Metallurgical variability, particularly within transition material
- Permitting delays or regulatory challenges
- Water availability and water management (dewatering) constraints
- Contractor performance and productivity
- Cost escalation for fuel, reagents, and construction materials

21.7.2 Mitigation Measures

Risk mitigation strategies include the following:

- Early and comprehensive metallurgical testing across all material types
- Parallel advancement of permitting and engineering activities
- Use of conservative design assumptions and contingency allowances
- Engagement of experienced contractors with Nevada operating experience
- Inclusion of appropriate contingency in capital and operating cost estimates

21.7.3 Capital Efficiency Strategy

The Project has been designed to minimize initial capital requirements while maintaining operational flexibility. Key elements of this strategy are listed:

- Use of contractor mining to eliminate the need for owner-purchased mining fleet.
- Development within existing disturbed areas to reduce earthworks and permitting requirements.
- Modular process plant design to allow phased expansion.
- Deferral of major capital expenditures associated with sulfide processing.

21.7.4 Transition to Pre-Feasibility Study (PFS)

The PFS will build upon the IA and refine all technical and economic assumptions. The study will upgrade cost estimates to an AACE Class 4 level, with an expected accuracy range of approximately minus 25 percent to plus 25 percent.

Key PFS deliverables will include the following:

- Development and geotechnical drilling, assaying, and metallurgical test work.
- Updated mine plan and production schedule.
- Refined metallurgical recovery models.
- Detailed capital and operating cost estimates.
- Permitting plan and status updates.
- Comprehensive set of trade off studies, yet to be defined.
- Economic analysis, including net present value and internal rate of return.



21.7.5 Mining and Scheduling Considerations

Future development of sulfide material will require integration into the overall mine plan. Key considerations include:

- Sequencing oxide and sulfide material to optimize project economics.
- Potential stockpiling strategies for sulfide material during oxide operations.
- Evaluation of cut-off grades specific to sulfide processing costs and recoveries.
- Impact on strip ratio and overall mine life.

These factors will be incorporated into future mine planning studies.

21.7.6 Environmental and Permitting Requirements

Processing of sulfide mineralization will likely introduce additional environmental considerations and permitting requirements, including:

- Expanded process facilities and tailings storage requirements.
- Increased water usage and potential discharge considerations.
- Additional air quality permitting, particularly for oxidation processes.
- Enhanced geochemical characterization to assess acid rock drainage and metal leaching potential.

Early engagement with regulatory agencies is recommended to define permitting pathways and timelines for sulfide development.

21.7.7 Future Sulfide Study Pathway

Advancement of sulfide mineralization is expected to follow a staged study approach, including:

- Scoping-level evaluation of processing options and economics.
- Pre-Feasibility Study (PFS) specific to sulfide development, if warranted.
- Feasibility Study (FS) and detailed engineering following confirmation of economic viability.

The sulfide resource represents a longer-term opportunity that could materially extend mine life and increase total metal production; however, it is associated with higher capital intensity and greater technical complexity than the oxide heap leach operation.

21.8 Conclusion

The Project PEP outlines a practical and efficient pathway to develop the Project through the reprocessing of waste rock dumps and the mining of oxide and mixed material using heap-leach technology. The strategy leverages existing site conditions, proven processing methods, and contractor-based mining to reduce capital intensity and accelerate development.

Permitting remains the critical path, supported by environmental baseline programs and regulatory engagement. With immediate initiation of the PFS and execution of parallel workstreams, the Project has the potential to achieve first production within approximately two years, subject to permitting timelines and successful completion of technical programs.



22.0 Interpretation and Conclusions

22.1 Geology and Mineral Resources

- The geological interpretation and deposit model are appropriate, internally consistent, and aligned with a low-sulfidation epithermal system, with mineralization strongly controlled by fault architecture and lithological contrasts.
- Mineralization exhibits high spatial variability, with discontinuous high-grade veins embedded within a laterally and vertically continuous low-grade stockwork domain, which comprises most of the tonnage.
- The Mineral Resource estimate has been prepared in accordance with S-K 1300 and CIM (2019) Best Practice Guidelines, supported by appropriate domain modeling, compositing, grade capping, interpolation, and validation workflows.
- The estimate is constrained within optimized open-pit shells demonstrating Reasonable Prospects for Economic Extraction (RPEE,) based on reasonable mining, processing, and economic assumptions, including a long-term gold price of US\$3,100/oz.
- The drilling database is large and generally adequate (approximately 4,300+ drill holes); however, gaps in historical metadata, incomplete records, and exclusion of unverifiable data introduce uncertainty, which is appropriately reflected in classification.
- Historical drilling is predominantly vertical RC, which adequately defines bulk-tonnage mineralization but limits confidence in true geometry and continuity of steeply dipping high-grade structures.
- The QA/QC and sampling protocols, while variable in early historical programs, are considered sufficient overall due to:
 - o Exclusion of unreliable or unsupported data from the Mineral Resource Estimate (MRE)
 - o Validation of assay datasets through statistical analysis, capping, compositing, and multi-method estimation checks
 - o Use of industry-standard QA/QC review and data screening prior to estimation. Accordingly, the QP considers the analytical dataset valid and appropriate to support the MRE, with remaining uncertainties reflected in classification.
- The oxidation model has been reviewed and corrected for inconsistencies and is considered appropriate for current estimation; however, localized coding issues indicate moderate residual uncertainty where metallurgical assumptions are sensitive.
- Exploration datasets (geophysical, geochemical, geological) are well integrated and effective for targeting, defining structural corridors, and mineralized trends extending beyond historically mined areas.
- Mineralization remains open along strike, at depth, and beneath cover, with identified targets considered conceptual but supported by integrated datasets.
- Compared to the 2023 estimate, the 2026 MRE shows a material increase in tonnage and contained metal, driven by:
 - o Inclusion and delineation of surface materials (existing waste rock dumps, heap leach pads, and tailings storage facility);



- o Expanded pit shells under higher gold price assumptions (US\$3,100/oz versus approximately US\$1,800/oz); and
- o Updated geological interpretation and database validation.
- This increase in tonnage is accompanied by a moderate reduction in average grade, consistent with inclusion of marginal material and not indicative of estimation bias.

22.2 Mining and Mineral Reserves

- There is no current geotechnical information for the pit slopes. Current pit slope assumptions may be optimized once geotechnical information has been collected and incorporated into the pit design.
- The current Base Case life of mine (LOM) plan includes a significant proportion of Inferred Mineral Resources (approximately 55%). The next stage of the Project will require converting Inferred Resources to Indicated Resources to reduce the project risk.
- Pit slope design assumes dry (i.e., dewatered) walls. Pit dewatering needs to start early enough for the open-pit mining operation to begin.
- There is potential to extend the mine life with the addition of a sulfide pit. To include the sulfide pit in the LOM plan, additional metallurgical test work and block modeling will be required.

22.3 Mineral Processing

- Metallurgical test work supports heap leaching with Merrill-Crowe recovery for oxide, mixed, and selected waste-rock materials, and flotation with off-site toll treatment or concentrate sale for sulfide, existing heap leach pad (HLP), and existing tailings material.
- The Base Case economic analysis is restricted to the heap-leach scenario, which is supported by the most complete, representative, and internally consistent metallurgical dataset.
- The proposed Base Case processing facility is a 30,000 tpd conventional crush–agglomerate–heap-leach operation employing Merrill-Crowe recovery. Design parameters include crushing to approximately P₈₀ 19 mm and agglomeration using cement and/or lime.
- Facilities oxide material demonstrates the strongest metallurgical response to heap leaching, with additional oxide, mixed, and selected waste-dump composites also supporting inclusion in the heap-leach feed blend.
- Gold and silver recovery assumptions for the heap-leach case are derived primarily from column leach testing, with conservative assumptions applied where only bottle-roll or limited test data exist.
- Sulfide, HLP, and tailings materials represent future processing opportunities via flotation. Recoveries have been reduced by 12% to account for toll-milling deductions and downstream treatment charges.
- No silver recovery is currently attributed to the flotation scenario; silver is treated as upside potential pending further metallurgical test work and commercial assessment.



- The heap leach flowsheet is a commercially proven, low-risk processing route appropriate for IA-level planning.
- Preliminary test work of the flotation option as a processing method for the sulfide material and existing HLP and TSF material is sufficient for the declaration of Mineral Resources; however, additional variability testing, concentrate characterization, and commercial evaluation are required to advance this option.

22.4 Infrastructure

- Access to the mine site is reliable via frequently traveled and maintained public infrastructure from Winnemucca, Nevada.
- Access and haul roads constructed on site will be designed and constructed in a manner sufficient to facilitate required on-site vehicular movement
- The proposed heap leach pad has been sited based on terrain, environmental, and operational bases and has been adequately sized to accommodate 175 Mt of agglomerated mineralized material.
- The pregnant solution and barren solution ponds have been located in proximity to the leach pad to take advantage to native slopes and have been sized to accommodate operational solution flow rates.
- The storm event pond has been located adjacent to the process ponds and has been sized to accommodate the 100-year 24-hour storm volume.
- Rapid infiltration basins have been designed to accommodate infiltration from pit dewatering efforts at an average rate of 4,542 m³/hr (20,000 US gallons per minute [gpm]).
- No accommodation camp has been included in the proposed infrastructure as the town of Winnemucca is within commuting distance and hosts a knowledgeable mining industry labor force.

22.5 Environment

- There are no known significant environmental issues at the site, and the former mine is in an advanced state of closure with post-closure monitoring and minor operational and maintenance activities being conducted.
- The regulatory environment is well developed, and the environmental permitting path forward for the mine plan presented in this TRS is generally well understood.

22.6 Capital and Operating Costs

- Preliminary capital and operating cost estimates have been prepared for the proposed mining operation based on a conceptual processing rate of approximately 30,000 tpd.
- For the Base Case, initial capital costs required to restart mining operations are estimated to be approximately US\$201 million, with sustaining capital estimated at approximately US\$342 million over the life of mine.
- Life-of-mine operating costs for the Base Case are estimated to average approximately US\$13.03 per tonne processed, resulting in an estimated all-in sustaining cost of approximately US\$2,407 per ounce of gold produced.



22.7 Risks

- The economic analysis presented in the Base Case as part of this TRS includes a material proportion of Inferred Mineral Resources within the mine plan and associated cash flow. The Inferred Mineral Resources are included at the beginning of the life-of-mine plan by mining existing dumps in the economic analysis, which introduces significant uncertainty.



23.0 Recommendations

The SLR QPs offer the following recommendations by discipline:

23.1 Geology and Mineral Resources

- 1 Conduct the following drilling and exploration programs:
 - a) Infill drilling to support conversion of Inferred to Indicated Mineral Resources (in situ and surface materials) by conducting systematic infill drilling within pit-constrained in situ domains and within surface material domains (dumps, heap leach pads, and TSF) to increase data density and improve confidence in grade continuity, tonnage, and material variability, consistent with S-K 1300 classification criteria.
 - b) Targeted infill drilling within established mineralization domains to increase drill density within defined grade domains to better constrain grade variability and continuity, particularly in areas where current spacing limits classification.
 - c) Additional drilling and geological logging to improve confidence in oxide, mixed, and sulfide boundaries, which directly influence metallurgical assumptions applied in the MRE.
- 2 Geology and Mineral Resource Estimate
 - a) Maintain domain-controlled drilling and sampling protocols to ensure all new data collection aligns with the current geological, mineralization, and estimation domain framework to support direct integration into future MRE updates.
 - b) Incorporate new data into updated geological interpretations and block models to support iterative improvement of the Mineral Resource estimate in accordance with S-K 1300 reporting requirements.
 - c) Acquire additional bulk density measurements across in situ and surface material domains where current density assignments are based on limited data, to improve tonnage estimates.
 - d) Focus drilling within the existing Mineral Resource footprint by prioritizing data acquisition in areas where incremental drilling is most likely to materially improve classification, rather than expanding the resource footprint at this stage.
- 3 Quality Assurance and Quality Control
 - a) Implement consistent QA/QC protocols for future work. Apply standardized QA/QC procedures (sampling, insertion rates, documentation) to ensure all new data meets S-K 1300 and CIM (2019) requirements and supports classification upgrades.
 - b) Recommend investigation of incomplete database information and update the database through investigation of historic files

To advance the Project, the QP recommends that Paramount Gold undertake a two-phase exploration and data validation program totaling \$8.52 million, as summarized in Table 23-1.

The goal is to support upgrading Inferred Mineral Resources to the Indicated category, validate key project assumptions regarding density and metallurgy, and continue delineation in underexplored areas.

This budget reflects a disciplined yet robust investment to de-risk the MRE, validate key technical assumptions (density, metallurgical recovery), and support a potential future



Preliminary Feasibility Study (PFS). The recommended work is expected to materially enhance the geological understanding and economic viability of the Sleeper Project.

The two phases of the work program are independent of each other.

Table 23-1: Proposed Sleeper 2026-2027 Exploration Budget

Activity	Details	Estimated Cost (US\$ 000)
Phase 1 – Surface and In Situ Resource Definition, QA/QC Implementation, and Metallurgical Studies		
ESG Permitting	Exploration and Environmental Permits for Phase 1 drilling	25
Sonic Drilling	Up to 30 holes (4000 ft) of sonic drilling at \$90/ft focused on obtaining metallurgical samples from Waste dumps, TSF and HL pads	360
RC Drilling	Up to 500 holes (50,000 ft) of RC drilling in Waste dumps, HL pads at \$50/ft	2,500
Core drilling	Confirmation core drilling of up to 10,000 ft at \$120/ft (HQ/NQ core)	1,200
Bulk Density Sampling	Collection and testing of up to 200 core and/or pit samples across all domains	12
Geochemical Assays	Assaying of approximately 15,000 samples incl. duplicates, standards, blanks	750
QA/QC Program Implementation	Establish certified sample control and auditing protocols	100
Metallurgical Testing	Leach testing of mineralized core for recovery studies	750
Technical Staff & Supervision	Field geologist, QA/QC lead, database tech	300
Total Phase 1		5,997
Phase 2 – Project Development Scoping		
ESG Permitting	Exploration and Environmental Permits for Phase 2 Geotech	25
Ground Support Geotechnical Testing	Geotech and analysis studies for Ground Support	250
Heap Leach Pad Geotechnical Testing and Design	Geotech and design engineering studies for Heap Leach Pad	600
Mining and Process Design & Engineering Analysis	Process design and engineering cost analysis and modeling	400
Environmental Baseline Studies	Hydrogeology, cultural, flora/fauna baseline for mine permitting	600
Stakeholder Engagement & Permitting Prep	Initial outreach, permitting roadmap	100
Technical Oversight & Contingency (10%)	Includes legal, overhead, permitting scope prep	198



Activity	Details	Estimated Cost (US\$ 000)
Reporting and Independent Review	S-K 1300 PFS update and QP sign-off	350
Total Phase 2		2,523
Grand Total		8,520

23.2 Mining and Mineral Reserves

- 1 Collect geotechnical information and develop geotechnical studies to support the pit design slopes for the next stage of the project.
- 2 Ensure the open-pit mining sequence is closely coordinated with the open-pit dewatering plan.
- 3 Continue the analysis of the sulfide pit as an opportunity after the oxide pit mining.

23.3 Mineral Processing

1. Complete additional variability column leach testing on oxide, mixed, and waste rock dump domains to confirm recovery, leach kinetics, and reagent consumption across the planned heap leach feed range.
2. Confirm provisional recovery assumptions for Sleeper oxide, Sleeper mixed, and West Wood mixed material with representative column leach test work.
3. Refine crush-size and agglomeration test work to confirm the selected coarse-crush heap leach design basis and optimize cement and lime addition by material type.
4. Expand reagent-consumption testing to better define sodium cyanide, lime, and cement demand for oxide, mixed, and waste rock dump materials, particularly where existing results indicate variable or elevated consumable requirements.
5. Complete additional column leach testing on selected waste rock dump materials to refine recovery assumptions by dump area and improve confidence in domain-based economic modeling.
6. Complete additional deleterious-element and precipitate-quality testing for Hg, As, Sb, and sulfur to confirm mercury management requirements and refine refinery and operating cost assumptions.
7. Complete flotation variability, optimization, and locked-cycle test work on representative sulfide, HLP and tailings composites to confirm recovery, consumable requirements, concentrate quality, and the suitability of an off-site toll-treatment or concentrate-sale route.

23.4 Infrastructure

- 1 Evaluate site-wide water balance and discharge requirements.
- 2 Perform a hydrogeological evaluation to support PFS level engineering of the rapid infiltration basin.
- 3 Confirm power requirements and supply availability.



- 4 Develop site-specific design criteria for the HLP and perform field investigations and laboratory testing to support advancing the HLP design.
- 5 Develop a PFS level HLP design that incorporates site specific data into the engineering calculations and analysis for such items as grading plan, slope stability analysis, water balance, settlement, and closure.

23.5 Environment

1. Complete updated baseline studies in accordance with National Environmental Policy Act of 1969 (NEPA) and applicable guidelines.
2. Engage early with local stakeholders and tribes and develop a stakeholder outreach plan.
3. Develop a permitting strategy and timeline.

23.6 Capital and Operating Costs

- 1 Move the dewatering from an “Allowance” to a full ‘Engineered System’, e.g., calibrated groundwater model; staged dewatering sequencing; pumping lift curves by pit phase; transient inflow modeling; wellfield spacing and drawdown analysis; contingency pumping scenarios; and power demand modeling for peak pumping periods.
- 2 Re-evaluate the crushing/agglomeration trade-off, e.g., variability column testing; permeability testing; compaction testing; fines migration testing; cement consumption optimization; lift-height testing; and irrigation optimization.
- 3 Tighten the heap leach pad phasing strategy, e.g., minimizing initial lined acreage; maximizing early vertical expansion; deferring later phases; reducing early pond construction; and sequencing underdrain installation.
- 4 Lock down power infrastructure requirements early, e.g., actual condition of transmission line; substation rebuild requirements; transformer replacement needs; utility interconnect requirements; and backup generation philosophy.
- 5 Validate the contractor mining strategy, i.e., obtain budgetary contractor bids; benchmark Nevada owner-mining versus contractor-mining; validate bank cubic meter (bcm) assumptions; stress-test diesel escalation; and stress-test productivity losses from wet conditions.
- 6 Refine the estimate by:
 - a) Improving mine haulage and re-handle modeling.
 - b) Tightening reagent consumption assumptions.
 - c) Adding more detailed closure escalation and water management costs.



24.0 References

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25.0 Reliance on Information Provided by the Registrant

This TRS has been prepared by SLR for PGN. The information, conclusions, opinions, and estimates contained herein are based on:

- Information available to SLR at the time of preparation of this TRS.
- Assumptions, conditions, and qualifications as set forth in this TRS.
- Data, reports, and other information supplied by PGN and other third-party sources.

For the purpose of this TRS, SLR has relied on current ownership information provided by PGN in a Title Report from PGN's Owner Representative dated December 1, 2023, entitled "2023 Update of Title Report on Sleeper Project, Humboldt County, Nevada." SLR has not researched property title or mineral rights for the Property as we consider it reasonable to rely on PGN's legal counsel, who is responsible for maintaining this information.

SLR has relied on PGN for guidance on applicable taxes, royalties, and other government levies or interests, applicable to revenue or income from the Property in the Executive Summary and Sections 4 and 19.

The SLR QP have taken all appropriate steps, in their professional opinion, to ensure that the above information from PGN is sound.

Except as specifically provided by applicable laws, any use of this TRS by any third party is at that party's sole risk.



26.0 Date and Signature Page

This report titled “S-K 1300 Technical Report Summary, Sleeper Gold Mine, Humboldt County, Nevada” with an effective date of April 29, 2026, was prepared and signed by:

(Signed) *SLR International Corporation*

Dated at Lakewood, CO
June 17, 2026

SLR International Corporation



27.0 Appendix 1 List of Claims

Table 27-1: Sleeper List of Claims

Claim Group	Claim Name	BLM Serial No.
SLEEPER	SLEEPER# 1	NMC250715
SLEEPER	SLEEPER# 2	NMC250716
SLEEPER	SLEEPER# 3	NMC250717
SLEEPER	SLEEPER# 4	NMC250718
SLEEPER	SLEEPER# 5	NMC250719
SLEEPER	SLEEPER# 6	NMC250720
SLEEPER	SLEEPER# 7	NMC250721
SLEEPER	SLEEPER# 8	NMC250722
SLEEPER	SLEEPER# 9	NMC250723
SLEEPER	SLEEPER# 10	NMC250724
SLEEPER	SLEEPER # 1 1	NMC250725
SLEEPER	SLEEPER# 12	NMC250726
SLEEPER	SLEEPER# 13	NMC250727
SLEEPER	SLEEPER# 14	NMC250728
SLEEPER	SLEEPER# 15	NMC250729
SLEEPER	SLEEPER# 16	NMC250730
SLEEPER	SLEEPER # 17	NMC250731
SLEEPER	SLEEPER # 18	NMC250732
SLEEPER	SLEEPER# 19	NMC250733
SLEEPER	SLEEPER # 20	NMC250734
SLEEPER	SLEEPER #21	NMC250735
SLEEPER	SLEEPER # 22	NMC250736
SLEEPER	SLEEPER # 23	NMC250737
SLEEPER	SLEEPER # 24	NMC250738
SLEEPER	SLEEPER # 25	NMC250739
SLEEPER	SLEEPER # 26	NMC250740
SLEEPER	SLEEPER # 27	NMC250741
SLEEPER	SLEEPER # 28	NMC250742
SLEEPER	SLEEPER # 29	NMC250743
SLEEPER	SLEEPER #30	NMC250744
SLEEPER	SLEEPER# 31	NMC250745
SLEEPER	SLEEPER # 32	NMC250746
SLEEPER	SLEEPER# 33	NMC250747
SLEEPER	SLEEPER # 34	NMC250748
SLEEPER	SLEEPER #35	NMC250749
SLEEPER	SLEEPER# 36	NMC250750

Claim Group	Claim Name	BLM Serial No.
MIMI	MIMI 371	NMC1072951
MIMI	MIMI 372	NMC1 072952
MIMI	MIMI 373	NMC1072953
MIMI	MIMI 374	NMC1072954
MIMI	MIMI 375	NMC1072955
MIMI	MIMI 376	NMC1072956
MIMI	MIMI 377	NMC1072957
MIMI	MIMI 378	NMC1072958
MIMI	MIMI 379	NMC1072959
MIMI	MIMI 380	NMC1 072960
MIMI	MIMI 381	NMC1072961
MIMI	MIMI 382	NMC1072962
MIMI	MIMI 383	NMC1072963
MIMI	MIMI 384	NMC1072964
MIMI	MIMI 385	NMC1072965
MIMI	MIMI 386	NMC1072966
MIMI	MIMI 387	NMC1072967
MIMI	MIMI 388	NMC1072968
MIMI	MIMI 389	NMC1072969
MIMI	MIMI 390	NMC1072970
MIMI	MIMI 391	NMC1072971
MIMI	MIMI 392	NMC1072972
MIMI	MIMI 393	NMC1072973
MIMI	MIMI 394	NMC1072974
MIMI	MIMI 395	NMC1072975
MIMI	MIMI 396	NMC1072976
MIMI	MIMI 397	NMC1072977
MIMI	MIMI 398	NMC1072978
MIMI	MIMI 399	NMC1072979
MIMI	MIMI 400	NMC1072980
MIMI	MIMI 401	NMC1072981
MIMI	MIMI 402	NMC1072982
MIMI	MIMI 403	NMC1 072983
MIMI	MIMI 404	NMC1072984
MIMI	MIMI 405	NMC1072985
MIMI	MIMI 406	NMC1072986



SLEEPER	SLEEPER# 37	NMC250751
SLEEPER	SLEEPER# 38	NMC250752
SLEEPER	SLEEPER # 39	NMC250753
SLEEPER	SLEEPER # 40	NMC250754
SLEEPER	SLEEPER# 41	NMC250755
SLEEPER	SLEEPER # 42	NMC250756
SLEEPER	SLEEPER # 43	NMC250757
SLEEPER	SLEEPER # 44	NMC250758
SLEEPER	SLEEPER # 45	NMC250759
SLEEPER	SLEEPER # 46	NMC250760
SLEEPER	SLEEPER # 47	NMC250761
SLEEPER	SLEEPER # 48	NMC250762
SLEEPER	SLEEPER # 49	NMC250763
SLEEPER	SLEEPER # 50	NMC250764
SLEEPER	SLEEPER# 51	NMC250765
SLEEPER	SLEEPER # 52	NMC250766
SLEEPER	SLEEPER # 53	NMC250767
SLEEPER	SLEEPER # 54	NMC250768
SLEEPER	SLEEPER# 55	NMC250769
SLEEPER	SLEEPER # 56	NMC250770
SLEEPER	SLEEPER# 57	NMC250771
SLEEPER	SLEEPER# 58	NMC250772
SLEEPER	SLEEPER # 59	NMC250773
SLEEPER	SLEEPER # 60	NMC250774
SLEEPER	SLEEPER# 61	NMC250775
SLEEPER	SLEEPER # 62	NMC250776
SLEEPER	SLEEPER # 63	NMC250777
SLEEPER	SLEEPER # 64	NMC250778
SLEEPER	SLEEPER # 65	NMC250779
SLEEPER	SLEEPER # 66	NMC250780
SLEEPER	SLEEPER # 67	NMC250781
SLEEPER	SLEEPER # 68	NMC250782
SLEEPER	SLEEPER # 69	NMC250783
SLEEPER	SLEEPER # 70	NMC250784
SLEEPER	SLEEPER #71	NMC250785
SLEEPER	SLEEPER # 72	NMC250786
SLEEPER	SLEEPER # 73	NMC250787
SLEEPER	SLEEPER # 74	NMC250788
SLEEPER	SLEEPER # 75	NMC250789
SLEEPER	SLEEPER # 76	NMC250790

MIMI	MIMI 407	NMC1072987
MIMI	MIMI 408	NMC1072988
MIMI	MIMI 409	NMC1072989
MIMI	MIMI 410	NMC1072990
MIMI	MIMI 411	NMC1072991
MIMI	MIMI 412	NMC1072992
MIMI	MIMI 413	NMC1072993
MIMI	MIMI 414	NMC1072994
MIMI	MIMI 415	NMC1072995
MIMI	MIMI 416	NMC1072996
MIMI	MIMI 417	NMC1072997
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NA	NA #47	NMC250848
NA	NA #48	NMC250849
NA	NA #49	NMC250850
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NA	NA #55	NMC250856
NA	NA# 56	NMC250857
NA	NA #57	NMC250858
NA	NA# 58	NMC250859
NA	NA# 59	NMC250860
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NA	NA# 61	NMC250862
NA	NA #62	NMC250863
DRYLAKE	DRYLAKE# 4	NMC251345
DRYLAKE	DRYLAKE# 15	NMC251346
DRYLAKE	DRYLAKE# 17	NMC251347
DRYLAKE	DRYLAKE# 18	NMC251348
DRYLAKE	DRYLAKE # 20	NMC251350
DRYLAKE	DRYLAKE# 21	NMC251351
DRYLAKE	DRYLAKE # 25	NMC251352
DRYLAKE	DRYLAKE # 28	NMC251353
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NA	NA #106	NMC321795
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MIMI	MIMI 535	NMC1073115
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SLEEPER	SLEEPER #91	NMC322020
SLEEPER	SLEEPER # 92	NMC322021
SLEEPER	SLEEPER # 93	NMC322022
SLEEPER	SLEEPER # 94	NMC322023
SLEEPER	SLEEPER # 95	NMC322024
SLEEPER	SLEEPER # 96	NMC322025
SLEEPER	SLEEPER # 97	NMC322026
SLEEPER	SLEEPER # 98	NMC322027
SLEEPER	SLEEPER # 99	NMC322028
SLEEPER	SLEEPER #100	NMC322029
SLEEPER	SLEEPER #101	NMC322030
SLEEPER	SLEEPER #102	NMC322031
SLEEPER	SLEEPER #103	NMC322032
SLEEPER	SLEEPER #104	NMC322033
SLEEPER	SLEEPER #105	NMC322034
SLEEPER	SLEEPER #106	NMC322035
SLEEPER	SLEEPER #107	NMC322036

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MIMI	MIMI 686	NMC1073266



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SLEEPER	SLEEPER #109	NMC322038
SLEEPER	SLEEPER #110	NMC322039
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SLEEPER	SLEEPER #112	NMC322041
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SLEEPER	SLEEPER #114	NMC322043
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SLEEPER	SLEEPER #11 8	NMC322047
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SLEEPER	SLEEPER #126	NMC322055
SLEEPER	SLEEPER #127	NMC322056
SLEEPER	SLEEPER #128	NMC322057
SLEEPER	SLEEPER #129	NMC322058
SLEEPER	SLEEPER #130	NMC322059
SLEEPER	SLEEPER #131	NMC322060
SLEEPER	SLEEPER #132	NMC322061
SLEEPER	SLEEPER #133	NMC322062
SLEEPER	SLEEPER #134	NMC322063
SLEEPER	SLEEPER #135	NMC322064
SLEEPER	SLEEPER #136	NMC322065
SLEEPER	SLEEPER #137	NMC322066
SLEEPER	SLEEPER #138	NMC322067
SLEEPER	SLEEPER #139	NMC322068
SLEEPER	SLEEPER #140	NMC322069
SLEEPER	SLEEPER #141	NMC322070
SLEEPER	SLEEPER #142	NMC322071
SLEEPER	SLEEPER #143	NMC322072
SLEEPER	SLEEPER #144	NMC322073
SLEEPER	SLEEPER #145	NMC322074
SLEEPER	SLEEPER #146	NMC322075
SLEEPER	SLEEPER #147	NMC322076

MIMI	MIMI 687	NMC1 073267
MIMI	MIMI 688	NMC1073268
MIMI	MIMI 689	NMC1073269
MIMI	MIMI 690	NMC1073270
MIMI	MIMI 691	NMC1073271
MIMI	MIMI 692	NMC1 073272
MIMI	MIMI 693	NMC1073273
MIMI	MIMI 694	NMC1073274
MIMI	MIMI 695	NMC1 073275
MIMI	MIMI 696	NMC1 073276
MIMI	MIMI 697	NMC1 073277
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MIMI	MIMI 699	NMC1 073279
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MIMI	MIMI 701	NMC1073281
MIMI	MIMI 702	NMC1073282
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MIMI	MIMI 704	NMC1 073284
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MIMI	MIMI 709	NMC1073289
MIMI	MIMI 710	NMC1 073290
MIMI	MIMI 711	NMC1073291
MIMI	MIMI 712	NMC1073292
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MIMI	MIMI 714	NMC1073294
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MIMI	MIMI 716	NMC1073296
MIMI	MIMI 717	NMC1073297
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MIMI	MIMI 722	NMC1073302
MIMI	MIMI 723	NMC1073303
MIMI	MIMI 724	NMC1073304
MIMI	MIMI 725	NMC1073305
MIMI	MIMI 726	NMC1073306



SLEEPER	SLEEPER #148	NMC322077
SLEEPER	SLEEPER #149	NMC322078
SLEEPER	SLEEPER #150	NMC322079
SLEEPER	SLEEPER #151	NMC322080
SLEEPER	SLEEPER #152	NMC322081
SLEEPER	SLEEPER #153	NMC322082
SLEEPER	SLEEPER #154	NMC322083
SLEEPER	SLEEPER #155	NMC322084
SLEEPER	SLEEPER #156	NMC322085
SLEEPER	SLEEPER #157	NMC322086
SLEEPER	SLEEPER #158	NMC322087
SLEEPER	SLEEPER #159	NMC322088
SLEEPER	SLEEPER #160	NMC322089
SLEEPER	SLEEPER #161	NMC322090
SLEEPER	SLEEPER #162	NMC322091
SLEEPER	SLEEPER #163	NMC322092
SLEEPER	SLEEPER #164	NMC322093
SLEEPER	SLEEPER #165	NMC322094
SLEEPER	SLEEPER #166	NMC322095
SLEEPER	SLEEPER #167	NMC322096
SLEEPER	SLEEPER #168	NMC322097
SLEEPER	SLEEPER #169	NMC322098
SLEEPER	SLEEPER #170	NMC322099
SLEEPER	SLEEPER #171	NMC322100
SLEEPER	SLEEPER #172	NMC322101
SLEEPER	SLEEPER #173	NMC322102
SLEEPER	SLEEPER #174	NMC322103
SLEEPER	SLEEPER #175	NMC322104
SLEEPER	SLEEPER #176	NMC322105
SLEEPER	SLEEPER #177	NMC322106
SLEEPER	SLEEPER #178	NMC322107
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SLEEPER	SLEEPER #183	NMC322112
SLEEPER	SLEEPER #184	NMC322113
SLEEPER	SLEEPER #185	NMC322114
SLEEPER	SLEEPER #186	NMC322115
SLEEPER	SLEEPER #187	NMC322116

MIMI	MIMI 727	NMC1073307
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MIMI	MIMI 729	NMC1073309
MIMI	MIMI 730	NMC1073310
MIMI	MIMI 731	NMC1073311
MIMI	MIMI 732	NMC1073312
MIMI	MIMI 733	NMC1073313
MIMI	MIMI 734	NMC1073314
MIMI	MIMI 735	NMC1073315
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MIMI	MIMI 737	NMC1073317
MIMI	MIMI 738	NMC1073318
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MIMI	MIMI 741	NMC1073321
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MIMI	MIMI 743	NMC1073323
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MIMI	MIMI 749	NMC1073329
MIMI	MIMI 750	NMC1073330
MIMI	MIMI 751	NMC1073331
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MIMI	MIMI 753	NMC1073333
MIMI	MIMI 754	NMC1073334
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MIMI	MIMI 756	NMC1073336
MIMI	MIMI 757	NMC1073337
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MIMI	MIMI 760	NMC1073340
MIMI	MIMI 761	NMC1073341
MIMI	MIMI 762	NMC1 073342
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MIMI	MIMI 764	NMC1073344
MIMI	MIMI 765	NMC1073345
MIMI	MIMI 766	NMC1073346



SLEEPER	SLEEPER #188	NMC322117
SLEEPER	SLEEPER #189	NMC322118
SLEEPER	SLEEPER #190	NMC322119
SLEEPER	SLEEPER #191	NMC322120
SLEEPER	SLEEPER #192	NMC322121
SLEEPER	SLEEPER #193	NMC322122
SLEEPER	SLEEPER #194	NMC322123
SLEEPER	SLEEPER #195	NMC322124
SLEEPER	SLEEPER #196	NMC322125
SLEEPER	SLEEPER #197	NMC322126
SLEEPER	SLEEPER #198	NMC322127
SLEEPER	SLEEPER #199	NMC322128
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SLEEPER	SLEEPER #209	NMC322138
SLEEPER	SLEEPER #210	NMC322139
SLEEPER	SLEEPER #312	NMC405562
SLEEPER	SLEEPER #317	NMC405567
SLEEPER	SLEEPER #318	NMC405568
SLEEPER	SLEEPER #319	NMC405569
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SLEEPER	SLEEPER #321	NMC405571
SLEEPER	SLEEPER #326	NMC405576
SLEEPER	SLEEPER #327	NMC405577
SLEEPER	SLEEPER #328	NMC405578
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SLEEPER	SLEEPER #330	NMC405580
SLEEPER	SLEEPER #335	NMC405585
SLEEPER	SLEEPER #336	NMC405586
SLEEPER	SLEEPER #337	NMC405587
SLEEPER	SLEEPER #338	NMC405588
SLEEPER	SLEEPER #339	NMC405589
SLEEPER	SLEEPER #343	NMC405593

MIMI	MIMI 767	NMC1 073347
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MIMI	MIMI 772	NMC1073352
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MIMI	MIMI 776	NMC1073356
MIMI	MIMI 777	NMC1073357
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MIMI	MIMI 779	NMC1073359
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MIMI	MIMI 786	NMC1073361
MIMI	MIMI 787	NMC1073362
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MIMI	MIMI 792	NMC1073367
MIMI	MIMI 793	NMC1073368
MIMI	MIMI 794	NMC1073369
MIMI	MIMI 795	NMC1073370
MIMI	MIMI 796	NMC1073371
MIMI	MIMI 797	NMC1 073372
MIMI	MIMI 798	NMC1073373
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MIMI	MIMI 800	NMC1073375
MIMI	MIMI 801	NMC1073376
MIMI	MIMI 802	NMC1073377
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MIMI	MIMI 811	NMC1073386



SLEEPER	SLEEPER #344	NMC405594
SLEEPER	SLEEPER #345	NMC405595
SLEEPER	SLEEPER #346	NMC405596
SLEEPER	SLEEPER #347	NMC405597
SLEEPER	SLEEPER #348	NMC405598
SLEEPER	SLEEPER #349	NMC405599
SLEEPER	SLEEPER #350	NMC405600
SLEEPER	SLEEPER #351	NMC405601
SLEEPER	SLEEPER #352	NMC405602
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SLEEPER	SLEEPER #358	NMC405608
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SLEEPER	SLEEPER #360	NMC405610
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SLEEPER	SLEEPER #364	NMC405614
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SLEEPER	SLEEPER #372	NMC405622
SLEEPER	SLEEPER #373	NMC405623
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SLEEPER	SLEEPER #375	NMC405625
SLEEPER	SLEEPER #376	NMC405626
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MIMI	MIMI 812	NMC1073387
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MIMI	MIMI 815	NMC1 073390
MIMI	MIMI 816	NMC1073391
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MIMI	MIMI 820	NMC1073395
MIMI	MIMI 821	NMC1073396
MIMI	MIMI 822	NMC1073397
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MIMI	MIMI 826	NMC1073401
MIMI	MIMI 827	NMC1073402
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MIMI	MIMI 833	NMC1073408
MIMI	MIMI 834	NMC1 073409
MIMI	MIMI 835	NMC1073410
MIMI	MIMI 836	NMC1073411
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MIMI	MIMI 870	NMC1 073445
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PDSLPL	PDSLPL 104	NMC778341

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MIMI	MIMI 895	NMC1073470
MIMI	MIMI 896	NMC1073471
MIMI	MIMI 897	NMC1073472
MIMI	MIMI 898	NMC1073473
MIMI	MIMI 899	NMC1073474
MIMI	MIMI 900	NMC1073475
MIMI	MIMI 901	NMC1073476
MIMI	MIMI 902	NMC 1073477
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MIMI	MIMI 909	NMC1073484
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MIMI	MIMI 954	NMC1080376
ELECTRUM	ELECTRUM # 11	NMC235675
ELECTRUM	ELECTRUM# 12	NMC235676
ELECTRUM	ELECTRUM# 13	NMC235677
ELECTRUM	ELECTRUM #21	NMC239887
ELECTRUM	ELECTRUM # 23	NMC239889



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FREE GOLD	FREE GOLD# 1	NMC252825
FREE GOLD	FREE GOLD# 2	NMC252826
FREE GOLD	FREE GOLD# 3	NMC252827
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FREE GOLD	FREE GOLD# 6	NMC252830
FREE GOLD	FREE GOLD# 7	NMC252831
FREE GOLD	FREE GOLD# 8	NMC252832
FREE GOLD	FREE GOLD# 9	NMC252833
FREE GOLD	FREE GOLD# 10	NMC252834
DAY	DAYLIGHT FRACTION	NMC269681
RR	RR#2	NMC340619
RR	RR#13	NMC340630
RR	RR#24	NMC340641
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RR	RR#37	NMC340654
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RR	RR#39	NMC340656
RR	RR#40	NMC340657
ELECTRUM	ELECTRUM# 1	NMC371654
ELECTRUM	ELECTRUM# 2	NMC371655
ELECTRUM	ELECTRUM# 3	NMC371656
LLY	LLY 1	NMC683286
LLY	LLY2	NMC683287
LLY	LLY 3	NMC683288
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DAY	DAY 16	NMC701011
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DAY	DAY 57	NMC713678



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NEW ALMA	NEW ALMA	NMC75273
VIRGINIA	VIRGINIA	NMC75274
MORNING	MORNING	NMC75275
MORNING STAR	MORNING STAR	NMC75276
NEW EVENING	NEW EVENING	NMC75277
NEW SNOWSTORM	NEW SNOWSTORM	NMC75278
LAM	LAM 76	NMC771939
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YORK	YORK#1	NMC787346
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YORK	YORK #3	NMC787348
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YORK	YORK #5	NMC787350
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MIMI	MIMI 293	NMC1 072885
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MIMI	MIMI 296	NMC1072888
MIMI	MIMI 297	NMC1072889
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MIMI	MIMI 304	NMC1072893
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MIMI	MIMI 323	NMC1072903
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MIMI	MIMI 325	NMC1072905
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SP	SP 627	NMC956095
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SS	SS67	NMC985082
SS	SS68	NMC985083
SS	SS 69	NMC985084
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SS	SS 72	NMC985087
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SS	SS 75	NMC985090
SS	SS76	NMC985091
SS	SS 77	NMC985092
SS	SS 78	NMC985093
SS	SS 79	NMC985094
SS	SS 80	NMC985095
SS	SS 81	NMC985096
SS	SS 82	NMC985097
SS	SS 83	NMC985098
SS	SS 84	NMC985099



MIMI	MIMI 328	NMC1072908
MIMI	MIMI 329	NMC1072909
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MIMI	MIMI 331	NMC1072911
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MIMI	MIMI 342	NMC1072922
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MIMI	MIMI 353	NMC1072933
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MIMI	MIMI 356	NMC1 072936
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MIMI	MIMI 359	NMC1072939
MIMI	MIMI 360	NMC1 072940
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MIMI	MIMI 362	NMC1072942
MIMI	MIMI 363	NMC1072943
MIMI	MIMI 364	NMC1072944
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MIMI	MIMI 367	NMC1072947

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SS	SS 87	NMC985102
SS	SS 88	NMC985103
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SS	SS 92	NMC985107
SS	SS 93	NMC985108
SS	SS 94	NMC985109
SS	SS 95	NMC985110
SS	SS 96	NMC9851 11
SS	SS 97	NMC985112
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LAM	LAM 0207	NMC833026
LAM	LAM 0208	NMC833027
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LAM	LAM 0210	NMC833029
CR	CR 1	NMC945647
CR	CR2	NMC945648
CR	CR3	NMC945649
CR	CR4	NMC945650
CR	CR5	NMC945651
CR	CR6	NMC945652
CR	CR7	NMC945653
CR	CR8	NMC945654
CR	CR9	NMC945655
CR	CR 10	NMC945656




MIMI	MIMI 368	NMC1072948
MIMI	MIMI 369	NMC1072949
MIMI	MIMI 370	NMC1 072950




28.0 Appendix 2 Cash Flow Summaries


Table 28-1: Base Case Cash Flow Summary

Economic Model Annual Summary														
		Company Name: Paramount Gold Nevada Corp Project Name: Sleeper Gold & Silver OP Project Scenario Name: Base Case - Measured, Indicated, and Inferred Resources Analysis Type: IA & SK-1300												
		Year -2 Pre-Prod. 22	Year -1 Pre-Prod. 21	Year 1 Ops 20	Year 2 Ops 19	Year 3 Ops 18	Year 4 Ops 17	Year 5 Ops 16	Year 6 Ops 15	Year 7 Ops 14	Year 8 Ops 13	Year 9 Ops 12	Year 10 Ops 11	Year 11 Ops 10
Calendar Year Project Stage Time Until Closure In Years	US\$ & Metric Units	LoM Avg / Total												
Market Prices														
Gold, Forecast	US\$/oz	\$3,618	-	4,370	4,000	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600
Silver, Forecast	US\$/oz	\$48.70	-	66.00	59.00	49.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00
Physicals														
Measured & Indicated Material Mined	45% kt	79,825	-	-	-	-	-	-	2,001	7,790	8,343	7,161	6,716	5,883
Inferred Material Mined	55% kt	66,620	-	-	7,300	10,800	10,800	10,800	8,799	3,070	2,454	3,639	4,084	5,112
Total Mineralized Material Mined	100% kt	175,445	-	-	7,300	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800
Total Waste Mined	kt	266,098	-	-	3,650	150	150	20,061	13,197	12,956	10,331	24,200	24,200	23,752
Total Material Mined	kt	441,542	-	-	10,950	10,950	10,950	30,861	23,997	23,756	21,131	35,000	35,000	34,552
Stripping Ratio	W/O	1.52	-	-	0.50	0.01	0.01	1.86	1.22	1.20	0.98	2.24	2.20	2.20
Total Mineralized Material Processed	kt	175,445	-	-	7,300	10,300	10,300	10,300	10,300	10,300	10,300	10,300	10,300	10,300
Gold Grade, Processed	g/t	0.26	-	-	0.27	0.39	0.36	0.17	0.18	0.22	0.25	0.24	0.21	0.20
Silver Grade, Processed	g/t	2.79	-	-	2.17	2.68	2.09	1.43	1.80	4.24	5.08	4.81	2.93	3.40
Contained Gold, Processed	koz	1,459	-	-	64	135	124	61	64	77	86	84	74	68
Contained Silver, Processed	koz	15,721	-	-	510	930	724	496	625	1,473	1,765	1,670	1,017	1,180
Average Recovery, Gold	%	75.8%	-	-	79.0%	79.0%	80.1%	76.8%	74.7%	74.7%	72.7%	74.7%	79.1%	72.7%
Average Recovery, Silver	%	22.1%	-	-	40.5%	40.5%	47.2%	49.2%	32.2%	15.6%	20.5%	19.0%	11.4%	14.2%
Recovered Gold, Processed	koz	1,106	-	-	50	107	99	46	48	59	62	63	59	50
Recovered Silver, Processed	koz	3,481	-	-	207	377	342	244	201	235	302	317	116	167
Payable Gold, Total	koz	1,101	-	-	50	106	99	46	47	59	62	62	58	49
Payable Silver, Total	koz	3,376	-	-	200	360	332	237	195	228	351	308	112	162
Cash Flow														
Gold Gross Revenue	66.0% \$000s	3,982,504	-	-	200,612	382,040	354,811	164,043	170,174	211,259	222,693	224,951	209,788	177,362
Silver Gross Revenue	4.0% \$000s	104,273	-	-	11,825	17,545	15,917	11,360	9,363	10,920	16,835	14,773	5,398	7,780
Gross Revenue Before By-Product Credits	100.0% \$000s	4,146,777	-	-	212,438	399,584	370,727	175,403	179,537	222,179	239,529	239,723	215,186	185,142
Gold Gross Revenue	\$000s	3,982,504	-	-	200,612	382,040	354,811	164,043	170,174	211,259	222,693	224,951	209,788	177,362
Silver Gross Revenue	\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Gross Revenue After By-Product Credit	\$000s	3,982,504	-	-	200,612	382,040	354,811	164,043	170,174	211,259	222,693	224,951	209,788	177,362
Mining Cost	\$000s	(1,116,897)	-	-	(24,125)	(24,125)	(24,125)	(67,992)	(59,390)	(61,577)	(54,771)	(90,720)	(90,720)	(89,560)
Dewatering Costs	\$000s	(103,595)	-	-	(1,882)	(3,064)	(2,587)	(5,694)	(6,153)	(6,999)	(11,519)	(9,237)	(5,526)	(11,676)
Process Cost	\$000s	(973,608)	-	-	(40,510)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)
G&A Cost	\$000s	(91,735)	-	-	(3,817)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)
Refining and Freight Cost	\$000s	(8,378)	-	-	(408)	(628)	(765)	(397)	(398)	(471)	(554)	(636)	(409)	(381)
Royalties	\$000s	(124,152)	-	-	(8,381)	(11,953)	(11,099)	(5,250)	(5,375)	(6,651)	(7,169)	(7,176)	(6,443)	(5,543)
Subtotal Cash Costs Before By-Product Credits	\$000s	(2,418,365)	-	-	(76,901)	(105,560)	(104,156)	(144,904)	(136,853)	(141,278)	(139,593)	(169,246)	(168,679)	(172,740)
By-Product Credits	\$000s	164,273	-	-	11,825	17,545	15,917	11,360	9,363	10,920	16,835	14,773	5,398	7,780
Total Cash Costs After By-Product Credits	\$000s	(2,254,093)	-	-	(65,075)	(88,015)	(88,240)	(133,544)	(127,520)	(130,358)	(122,758)	(154,476)	(163,281)	(164,960)
Operating Margin	42% \$000s	1,728,412	-	-	135,537	294,025	266,571	30,499	42,654	80,900	99,936	70,475	46,507	12,402
Other Admin Expenses	\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-
EBITDA	\$000s	1,728,412	-	-	135,537	294,025	266,571	30,499	42,654	80,900	99,936	70,475	46,507	12,402
Depreciation Allowance	\$000s	(543,029)	(120,651)	(80,434)	(715)	(13,948)	(87,238)	(31,927)	(36,781)	(60,255)	(715)	(2,691)	(41,132)	(715)
Depletion Allowance	\$000s	(485,279)	-	-	(30,911)	(58,143)	(53,944)	-	(2,936)	(10,323)	(34,854)	(33,892)	(2,888)	(5,944)
Earnings Before Taxes	\$000s	719,503	(120,651)	(80,434)	103,911	221,933	125,389	(1,428)	2,936	10,323	64,367	33,892	2,688	5,844
Federal Income Tax & State Tax	\$000s	(214,344)	-	-	(9,782)	(33,541)	(33,973)	(1,254)	(1,359)	(3,733)	(17,608)	(10,000)	(1,944)	(2,534)
Net Income	\$000s	505,159	(120,651)	(80,434)	94,129	188,393	91,416	(2,882)	1,578	6,590	46,759	23,888	744	3,310
Non-Cash Add Back - Depreciation	\$000s	543,029	120,651	80,434	715	13,948	87,238	31,927	36,781	60,255	715	2,691	41,132	715
Non-Cash Add Back - Depletion	\$000s	485,279	-	-	30,911	58,143	53,944	-	2,936	10,323	34,854	33,892	2,888	5,944
Working Capital	\$000s	0	(3,620)	(2,413)	(4,150)	(6,328)	(1,436)	8,722	(1,604)	(3,469)	(989)	(236)	1,166	(2,515)
Operating Cash Flow	\$000s	1,514,067	(3,620)	(2,413)	121,605	254,156	231,162	37,966	39,851	73,838	81,335	61,758	44,327	11,035
Initial Capital	\$000s	(201,685)	(120,651)	(80,434)	-	-	-	-	-	-	-	-	-	-
Sustaining Capital	\$000s	(342,544)	-	-	(715)	(13,948)	(87,238)	(31,927)	(36,781)	(60,255)	(715)	(2,691)	(41,132)	(715)
Closure/Reclamation/Monitoring Costs	\$000s	(52,432)	-	-	-	-	-	-	-	-	-	-	-	-
Total Capital	\$000s	(596,662)	(120,651)	(80,434)	(715)	(13,948)	(87,238)	(31,927)	(36,781)	(60,255)	(715)	(2,691)	(41,132)	(715)
Cash Flow Adj./Reimbursements	\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-



Economic Model Annual Summary																
		Company: Paramount Gold Nevada Corp Project Name: Sleeper Gold & Silver OP Project Scenario Name: Base Case - Measured, Indicated, and Inferred Resources Analysis Type: IA & SK-1300														
		Year -2 Pre-Prod. 22	Year -1 Pre-Prod. 21	Year 1 Ops 20	Year 2 Ops 19	Year 3 Ops 18	Year 4 Ops 17	Year 5 Ops 16	Year 6 Ops 15	Year 7 Ops 14	Year 8 Ops 13	Year 9 Ops 12	Year 10 Ops 11	Year 11 Ops 10		
Calendar Year	Project Stage	US\$ & Metric Units	LoM Avg / total													
Market Prices																
Gold, Forecast		US\$/oz	\$3,618	-	4,370	4,000	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	
Silver, Forecast		US\$/oz	\$48.70	-	66.00	59.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	
Physicals																
Measured & Indicated Material Mined	45%	kt	79,825	-	-	-	-	-	-	2,001	7,790	8,348	7,161	6,716	5,883	5,841
Inferred Material Mined	55%	kt	96,620	-	-	7,300	10,800	10,800	10,800	8,799	3,070	2,454	3,639	4,084	5,112	4,953
Total Mineralized Material Mined	100%	kt	175,445	-	-	7,300	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800
Total Waste Mined		kt	266,098	-	-	3,650	150	150	20,081	13,197	12,956	10,331	24,200	24,200	23,752	19,320
Total Material Mined		kt	441,542	-	-	10,950	10,950	10,950	30,981	23,997	23,756	21,131	35,000	35,000	34,552	30,120
Stripping Ratio		W/O	1.52	-	-	0.50	0.01	0.01	1.86	1.22	1.20	0.98	2.24	2.24	2.20	1.79
Total Mineralized Material Processed		kt	175,445	-	-	7,300	10,300	10,300	10,300	10,300	10,300	10,300	10,300	10,300	10,300	10,300
Gold Grade, Processed		g/t	0.26	-	-	0.27	0.39	0.36	0.17	0.18	0.22	0.25	0.24	0.21	0.20	0.24
Silver Grade, Processed		g/t	2.79	-	-	2.17	2.68	2.09	1.43	1.80	4.24	5.08	4.81	2.93	3.40	3.60
Contained Gold, Processed		koz	1,459	-	-	64	135	124	61	64	77	86	84	74	68	85
Contained Silver, Processed		koz	15,721	-	-	510	930	724	496	625	1,473	1,765	1,670	1,017	1,180	1,249
Average Recovery, Gold		%	75.8%	-	-	79.0%	79.0%	80.1%	75.8%	74.5%	74.7%	72.7%	74.7%	79.1%	72.7%	74.2%
Average Recovery, Silver		%	22.1%	-	-	40.5%	40.5%	47.2%	49.2%	32.2%	15.9%	20.5%	19.0%	11.4%	14.2%	15.1%
Recovered Gold, Processed		koz	1,106	-	-	50	107	99	46	48	59	82	63	59	50	63
Recovered Silver, Processed		koz	3,481	-	-	207	377	342	244	201	235	362	317	116	167	188
Payable Gold, Total		koz	1,101	-	-	50	106	99	46	47	59	82	62	58	49	63
Payable Silver, Total		koz	3,376	-	-	200	360	332	237	195	228	351	308	112	162	183
Cash Flow																
Gold Gross Revenue	95.0%	\$000s	3,982,504	-	-	200,612	382,040	354,811	164,043	170,174	211,259	222,893	224,951	209,788	177,362	225,450
Silver Gross Revenue	4.0%	\$000s	104,273	-	-	11,825	17,545	15,917	11,360	9,363	10,920	16,835	14,773	5,398	7,780	8,762
Gross Revenue Before By-Product Credits	100.0%	\$000s	4,146,777	-	-	212,438	399,584	370,727	175,403	179,537	222,179	239,728	239,724	215,186	185,142	234,212
Gold Gross Revenue		\$000s	3,982,504	-	-	200,612	382,040	354,811	164,043	170,174	211,259	222,893	224,951	209,788	177,362	225,450
Silver Gross Revenue		\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Gross Revenue After By-Product Credit		\$000s	3,982,504	-	-	200,612	382,040	354,811	164,043	170,174	211,259	222,893	224,951	209,788	177,362	225,450
Mining Cost		\$000s	(1,116,897)	-	-	(24,125)	(24,125)	(24,125)	(67,992)	(59,390)	(61,577)	(54,771)	(90,720)	(90,720)	(89,590)	(78,070)
Dewatering Costs		\$000s	(1,103,595)	-	-	(1,882)	(3,064)	(2,587)	(5,694)	(6,153)	(6,999)	(11,519)	(5,237)	(5,526)	(11,676)	(4,532)
Process Cost		\$000s	(973,608)	-	-	(40,510)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)
G&A Cost		\$000s	(91,735)	-	-	(3,817)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)
Refining and Freight Cost		\$000s	(8,378)	-	-	(406)	(628)	(765)	(397)	(398)	(471)	(554)	(409)	(361)	(472)	
Royalties		\$000s	(124,152)	-	-	(8,381)	(11,983)	(11,089)	(5,250)	(5,375)	(6,851)	(7,169)	(7,176)	(6,443)	(5,543)	(7,012)
Subtotal Cash Costs Before By-Product Credits		\$000s	(2,418,365)	-	-	(78,901)	(105,560)	(104,156)	(144,904)	(136,853)	(141,278)	(139,593)	(189,248)	(168,679)	(172,740)	(155,666)
By-Product Credits		\$000s	164,273	-	-	11,825	17,545	15,917	11,360	9,363	10,920	16,835	14,773	5,398	7,780	8,762
Total Cash Costs After By-Product Credits		\$000s	(2,254,093)	-	-	(65,075)	(88,015)	(88,240)	(133,544)	(127,520)	(130,358)	(122,758)	(154,476)	(163,281)	(164,960)	(146,904)
Operating Margin	42%	\$000s	1,728,412	-	-	135,537	294,025	266,571	30,499	42,654	80,900	99,936	70,475	46,507	12,402	78,546
Other Admin Expenses		\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-
EBITDA		\$000s	1,728,412	-	-	135,537	294,025	266,571	30,499	42,654	80,900	99,936	70,475	46,507	12,402	78,546
Depreciation Allowance		\$000s	(543,029)	(120,651)	(80,434)	(715)	(13,948)	(87,238)	(31,927)	(36,781)	(60,255)	(715)	(2,691)	(41,132)	(715)	(2,175)
Depletion Allowance		\$000s	(485,279)	-	-	(30,911)	(58,143)	(53,944)	-	(2,936)	(34,854)	(33,892)	(2,898)	(5,944)	(34,080)	(34,080)
Earnings Before Taxes		\$000s	719,503	(120,651)	(80,434)	103,911	221,933	125,389	(1,428)	2,936	10,323	64,367	33,892	2,688	5,844	42,291
Federal Income Tax & State Tax		\$000s	(214,344)	-	-	(9,782)	(33,541)	(33,973)	(1,254)	(1,359)	(3,733)	(17,808)	(10,000)	(1,944)	(2,534)	(12,054)
Net Income		\$000s	505,159	(120,651)	(80,434)	94,129	188,393	91,416	(2,882)	1,578	6,590	46,759	23,886	744	3,310	30,238
Non-Cash Add Back - Depreciation		\$000s	543,029	120,651	80,434	715	13,948	87,238	31,927	36,781	60,255	715	2,691	41,132	715	2,175
Non-Cash Add Back - Depletion		\$000s	465,279	-	-	30,911	58,143	53,944	-	2,936	10,323	34,854	33,892	2,898	5,944	34,080
Working Capital		\$000s	0	(3,620)	(2,413)	150	(8,328)	(1,436)	8,722	(1,804)	(3,469)	(989)	1,259	(236)	1,166	(2,515)
Operating Cash Flow		\$000s	1,514,067	(3,620)	(2,413)	121,605	254,156	231,162	37,965	35,851	73,898	81,335	61,758	44,327	11,035	63,978
Initial Capital		\$000s	(201,985)	(120,651)	(80,434)	-	-	-	-	-	-	-	-	-	-	-
Sustaining Capital		\$000s	(342,544)	-	-	(715)	(13,948)	(87,238)	(31,927)	(36,781)	(60,255)	(715)	(2,691)	(41,132)	(715)	(2,175)
Closure/Reclamation/Monitoring Costs		\$000s	(52,432)	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Capital		\$000s	(596,962)	(120,651)	(80,434)	(715)	(13,948)	(87,238)	(31,927)	(36,781)	(60,255)	(715)	(2,691)	(41,132)	(715)	(2,175)
Cash Flow Adj./Reimbursements		\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-



Economic Model Annual Summary																	
		Company: Paramount Gold Nevada Corp Project Name: Sleeper Gold & Silver OP Project Scenario Name: Base Case - Measured, Indicated, and Inferred Resources Analysis Type: IA & SK-1300															
		Calendar Year	Project Stage	Time Until Closure in Years	US\$ & Metric Units	LoM Avg / Total	Year -2 Pre-Prod. 22	Year -1 Pre-Prod. 21	Year 1 Ops 20	Year 2 Ops 19	Year 3 Ops 18	Year 4 Ops 17	Year 5 Ops 16	Year 6 Ops 15	Year 7 Ops 14	Year 8 Ops 13	Year 9 Ops 12
LoM Metrics																	
Economic Metrics																	
Discount Rate	BOP	8%			0.9259	0.8573	0.7938	0.7350	0.6806	0.6302	0.5835	0.5403	0.5002	0.4632	0.4289	0.3971	0.3677
a) Pre-Tax																	
Free Cash Flow	\$000s		1,132,350	(124,270)	(82,847)	130,672	273,749	177,897	7,294	4,269	17,177	98,232	69,073	5,139	12,854	73,856	
Cumulative Free Cash Flow	\$000s			(124,270)	(207,117)	(75,445)	197,303	375,200	382,494	386,762	403,939	502,172	571,245	576,384	589,238	683,094	
NPV @ 8%	\$000s		505,047	(115,065)	(71,028)	103,732	201,213	121,074	4,396	2,491	9,280	49,141	31,994	2,204	5,104	27,157	
Cumulative NPV @ 8%	\$000s			(115,065)	(186,093)	(62,361)	118,852	238,926	244,522	247,013	256,293	305,433	337,427	338,632	344,736	371,893	
IRR	%		51.3%														
Payback Period	years		1.3			1.0	0.3	-									
b) After-Tax																	
Free Cash Flow	\$000s		918,006	(124,270)	(82,847)	120,891	240,208	143,924	6,039	2,910	13,444	80,625	59,067	3,196	10,320	61,803	
Cumulative Free Cash Flow	\$000s			(124,270)	(207,117)	(86,227)	153,981	297,905	303,944	306,854	320,298	400,922	459,990	463,185	473,508	536,308	
NPV @ 8%	\$000s		402,353	(115,065)	(71,028)	95,967	176,560	97,952	3,806	1,698	7,263	40,332	27,359	1,371	4,098	22,725	
Cumulative NPV @ 8%	\$000s			(115,065)	(186,093)	(90,126)	98,434	184,386	188,192	189,890	197,153	237,485	264,845	266,215	270,314	293,038	
IRR	%		44.5%														
Payback Period	years		1.4			1.0	0.4	-									
Operating Metrics																	
Mine Life	Years		17														
Average Daily Mining Rate	td mined		74,000	-	-	30,417	30,417	30,417	85,724	66,657	65,990	58,698	97,222	97,222	95,079	83,666	
Average Daily Processing Rate	td placed		29,000	-	-	20,276	30,000	30,000	30,000	30,000	30,000	30,000	30,000	30,000	30,000	30,000	
Mining Cost	\$ / t mined		\$2.53	-	-	2.20	2.20	2.20	2.20	2.47	2.59	2.59	2.59	2.59	2.59	2.59	
Mining Cost	\$/t process		\$6.37	-	-	3.30	2.23	2.23	6.30	5.50	5.70	5.07	8.40	8.40	8.29	7.23	
Dewatering Cost	\$/t process		\$0.59	-	-	0.23	0.28	0.24	0.53	0.57	0.65	1.07	0.48	0.51	1.08	0.42	
Processing Cost	\$/t process		\$5.55	-	-	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	
G&A Cost	\$/t process		\$0.52	-	-	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	
Subtotal Direct Operating Costs	\$/t process		\$13.03	-	-	9.61	8.39	8.55	12.89	12.14	12.42	12.21	14.96	14.98	15.45	13.72	
Refining and Freight Cost	\$/t process		\$0.05	-	-	0.06	0.08	0.07	0.04	0.04	0.04	0.05	0.05	0.04	0.04	0.04	
NSR Royalty	\$/t process		\$0.71	-	-	0.87	1.11	1.03	0.49	0.50	0.62	0.66	0.66	0.60	0.51	0.65	
Total Operating Cost	\$/t process		\$13.78	-	-	10.53	9.77	9.64	13.42	12.67	13.08	12.93	15.67	15.62	15.99	14.41	
Sales Metrics																	
Au Sales	koz		1,101	-	-	50	106	99	46	47	59	62	62	58	49	63	
Ag Sales	koz		3,376	-	-	200	366	332	237	195	228	351	308	112	162	183	
Total Cash Cost (LOM)	\$ / oz Au		2,048														
Total AISC (LOM)	\$ / oz Au		2,407			1,312	961	1,780	3,631	3,476	3,248	1,996	2,515	3,508	3,363	2,380	
Avg. LOM Annual Au Sales (excl. rinsing phase)	koz/yr		65														
Avg. LOM Annual Ag Sales (excl. rinsing phase)	koz/yr		199														





Economic Model Annual Summary																
		Company: Paramount Gold Nevada Sleeper Gold & Silver OP Project Name: Sleeper Gold & Silver OP Scenario Name: Base Case - Measured, In IA & SK-1300 Analysis Type:														
		Year 12	Year 13	Year 14	Year 15	Year 16	Year 17	Year 18	Year 19	Year 20	Year 21	Year 22	Year 23	Year 24	Year 25	
Calendar Year	Project Stage	Time Until Closure In Years	US\$ & Metric Units	Op 9	Op 8	Op 7	Op 6	Op 5	Op 4	Op 3	Op 2	Op 1	Closure	Closure	Closure	Closure
Market Prices																
Gold, Forecast		US\$/oz	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600
Silver, Forecast		US\$/oz	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00
Physicals																
Measured & Indicated Material Mined	46%	kt	7,548	7,873	8,156	8,367	8,499	8,552	-	-	-	-	-	-	-	-
Inferred Material Mined	55%	kt	3,252	2,927	2,644	2,443	2,249	2,092	-	-	-	-	-	-	-	-
Total Mineralized Material Mined	100%	kt	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800
Total Waste Mined		kt	24,200	24,200	16,219	24,200	15,903	9,409	-	-	-	-	-	-	-	-
Total Material Mined		kt	35,000	35,000	27,019	35,000	26,703	15,553	-	-	-	-	-	-	-	-
Stripping Ratio		W:O	2.24	2.24	1.50	2.24	1.47	1.53	-	-	-	-	-	-	-	-
Total Mineralized Material Processed		kt	10,800	10,800	10,800	10,800	10,800	6,145	-	-	-	-	-	-	-	-
Gold Grade, Processed		g/t	0.27	0.27	0.27	0.26	0.29	0.31	-	-	-	-	-	-	-	-
Silver Grade, Processed		g/t	2.36	2.35	3.07	1.29	1.21	2.62	-	-	-	-	-	-	-	-
Contained Gold, Processed		koz	95	95	91	100	62	-	-	-	-	-	-	-	-	-
Contained Silver, Processed		koz	818	815	1,065	443	421	518	-	-	-	-	-	-	-	-
Average Recovery, Gold		%	75.0%	72.6%	71.9%	78.0%	77.4%	71.9%	0.0%	0.0%	0.0%	-	-	-	-	-
Average Recovery, Silver		%	18.1%	20.6%	20.7%	14.3%	12.4%	14.3%	0.0%	0.0%	0.0%	-	-	-	-	-
Recovered Gold, Processed		koz	72	69	69	71	77	45	-	-	-	-	-	-	-	-
Recovered Silver, Processed		koz	148	168	220	83	52	74	-	-	-	-	-	-	-	-
Payable Gold, Total		koz	71	68	68	71	77	44	-	-	-	-	-	-	-	-
Payable Silver, Total		koz	144	163	213	81	51	72	-	-	-	-	-	-	-	-
Cash Flow																
Gold Gross Revenue	95.0%	\$000s	256,117	246,368	245,877	254,131	277,158	159,671	-	-	-	-	-	-	-	-
Silver Gross Revenue	4.0%	\$000s	6,902	7,815	10,243	2,949	2,429	3,457	-	-	-	-	-	-	-	-
Gross Revenue Before By-Product Credits	100.0%	\$000s	263,019	254,183	256,120	257,080	279,587	163,128	-	-	-	-	-	-	-	-
Gold Gross Revenue		\$000s	256,117	246,368	245,877	254,131	277,158	159,671	-	-	-	-	-	-	-	-
Silver Gross Revenue		\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Gross Revenue After By-Product Credit		\$000s	256,117	246,368	245,877	254,131	277,158	159,671	-	-	-	-	-	-	-	-
Mining Cost		\$000s	(90,720)	(90,720)	(70,033)	(90,720)	(89,215)	(40,315)	-	-	-	-	-	-	-	-
Dewatering Costs		\$000s	(5,234)	(5,240)	(12,884)	(8,430)	(6,090)	(3,057)	-	-	-	-	-	-	-	-
Process Cost		\$000s	(59,933)	(59,933)	(59,933)	(59,933)	(59,933)	(34,099)	-	-	-	-	-	-	-	-
G&A Cost		\$000s	(5,947)	(5,947)	(5,947)	(5,947)	(5,947)	(3,213)	-	-	-	-	-	-	-	-
Refining and Freight Cost		\$000s	(503)	(497)	(522)	(457)	(400)	(305)	-	-	-	-	-	-	-	-
Royalties		\$000s	(7,875)	(7,611)	(7,668)	(7,699)	(8,373)	(4,885)	-	-	-	-	-	-	-	-
Subtotal Cash Costs Before By-Product Credits		\$000s	(169,913)	(169,645)	(156,888)	(170,887)	(149,748)	(85,873)	-	-	-	-	-	-	-	-
By-Product Credits		\$000s	6,902	7,815	10,243	2,949	2,429	3,457	-	-	-	-	-	-	-	-
Total Cash Costs After By-Product Credits		\$000s	(163,012)	(161,832)	(146,645)	(167,938)	(147,320)	(82,416)	-	-	-	-	-	-	-	-
Operating Margin	42%	\$000s	93,105	84,535	99,432	86,193	129,839	77,255	-	-	-	-	-	-	-	-
Other Admin Expenses		\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-
EBITDA		\$000s	93,105	84,535	99,432	86,193	129,839	77,255	-	-	-	-	-	-	-	-
Depreciation Allowance		\$000s	(49,938)	(516)	(1,460)	(11,351)	-	(990)	-	-	-	-	-	-	-	-
Depletion Allowance		\$000s	(21,584)	(36,986)	(37,268)	(37,407)	(40,682)	(23,737)	-	-	-	-	-	-	-	-
Earnings Before Taxes		\$000s	21,584	47,034	60,704	37,435	89,156	52,529	-	-	-	-	-	-	-	-
Federal Income Tax & State Tax		\$000s	(7,137)	(13,411)	(16,838)	(11,041)	(24,141)	(13,990)	-	-	-	-	-	-	-	-
Net Income		\$000s	14,448	33,623	43,866	26,394	65,016	38,539	-	-	-	-	-	-	-	-
Non-Cash Add Back - Depreciation		\$000s	49,938	516	1,460	11,351	990	-	-	-	-	-	-	-	-	-
Non-Cash Add Back - Depletion		\$000s	21,584	36,986	37,268	37,407	40,682	23,737	-	-	-	-	-	-	-	-
Working Capital		\$000s	(2,194)	347	(915)	408	(1,747)	1,309	-	-	-	-	-	-	-	-
Operating Cash Flow		\$000s	83,774	71,472	81,679	75,560	103,951	64,574	18,375	-	-	-	-	-	-	-
Initial Capital		\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Sustaining Capital		\$000s	(49,938)	(516)	(1,460)	(11,351)	-	(990)	-	-	-	-	-	-	-	-
Closure/Reclamation/Monitoring Costs		\$000s	-	-	-	-	-	-	(22,533)	(7,845)	(6,932)	(7,044)	(2,915)	(2,105)	(1,418)	(1,640)
Total Capital		\$000s	(49,938)	(516)	(1,460)	(11,351)	-	(990)	(22,533)	(7,845)	(6,932)	(7,044)	(2,915)	(2,105)	(1,418)	(1,640)
Cash Flow Adj./Reimbursements		\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-



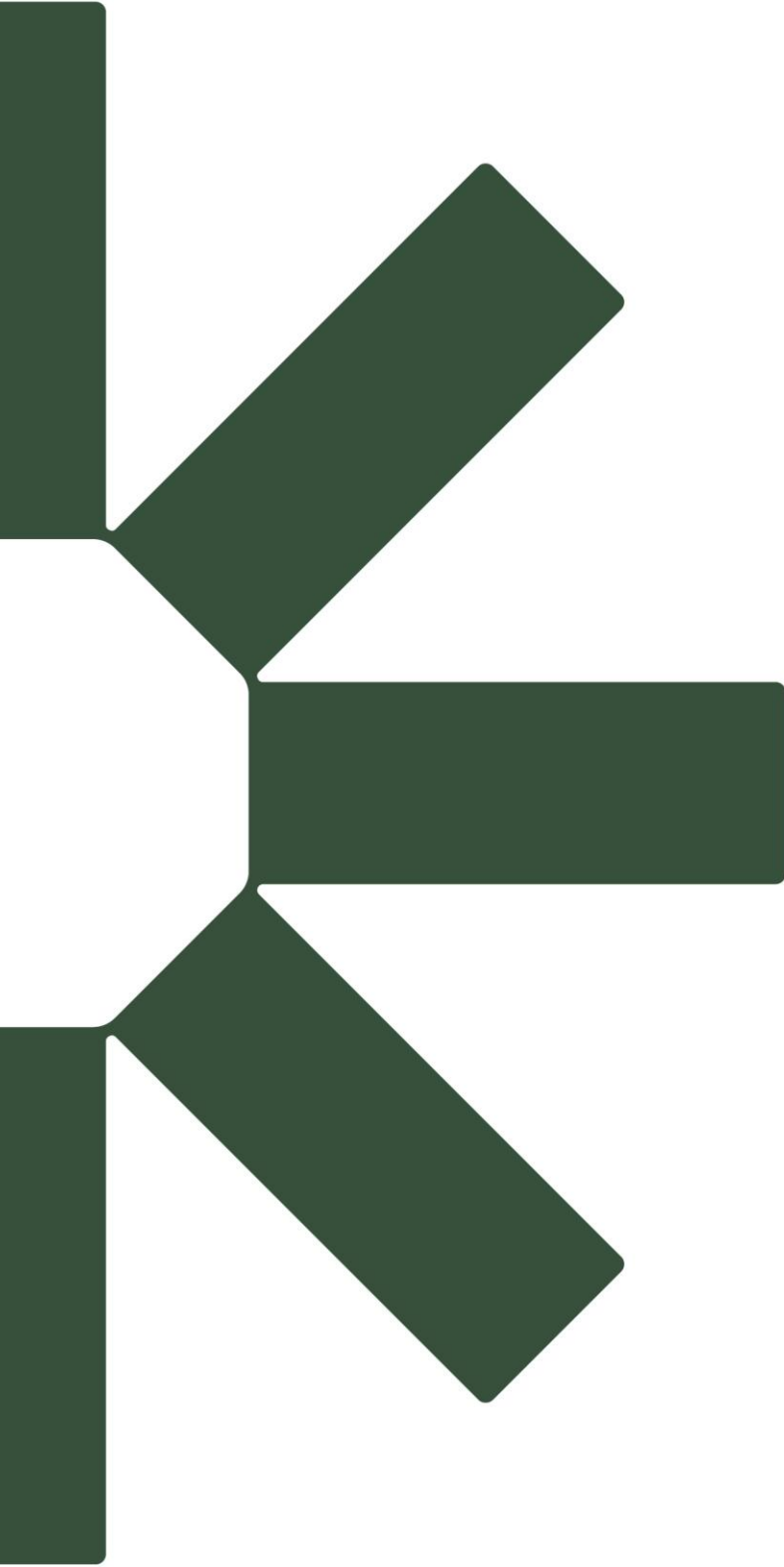
Table 28-2: Alternative Case Cash Flow Summary

Economic Model Annual Summary			New Sleeper Gold LLC																
SLR			Sleeper Gold & Silver OP Project																
Company			Alternative Case - M-I Resources																
Project Name			IA & SK-1300																
Scenario Name																			
Analysis Type																			
Calendar Year	Year 2	Year 1	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Year 11	Year 12	Year 13	Year 14	Year 15	Year 16	
Project Stage	Pre-Prod.	Pre-Prod.	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	Ops	
Time Until Closures In Years	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	
Min/Mt Prices	US\$/oz		LOM Avg / Total																
Gold Forecast	41,622	4,370	4,000	3,500	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600	3,600
Silver Forecast	448.40	66.00	59.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00	48.00
Physicals																			
Total Mineralized Material Mined (M-I Resources)	kt	62,447	-	3,359	9,234	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800
Total Waste Mined	kt	65,708	-	11,641	11,766	9,200	8,334	8,966	7,940	4,163	-	-	-	-	-	-	-	-	-
Total Material Mined	kt	121,156	-	15,000	20,000	20,000	19,134	16,456	16,740	11,817	-	-	-	-	-	-	-	-	-
Stripping Ratio	W/O	0.94	-	3.47	1.43	0.85	0.77	0.52	0.74	0.54	-	-	-	-	-	-	-	-	-
Total Mineralized Material Processed	kt	62,447	-	3,359	9,234	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800	10,800
Gold Grade, Processed	gt	0.27	-	0.25	0.24	0.27	0.26	0.29	0.29	0.31	-	-	-	-	-	-	-	-	-
Silver Grade, Processed	gt	3.83	-	4.04	5.16	5.54	2.73	3.55	3.20	2.78	-	-	-	-	-	-	-	-	-
Contained Gold, Processed	koz	602	-	27	62	96	89	101	99	77	-	-	-	-	-	-	-	-	-
Contained Silver, Processed	koz	7,697	-	436	1,366	1,925	948	1,233	1,110	678	-	-	-	-	-	-	-	-	-
Average Recovery, Gold	%	74.3%	-	82.0%	75.2%	72.2%	80.2%	72.7%	72.6%	70.9%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Average Recovery, Silver	%	18.1%	-	10.4%	17.8%	21.3%	12.2%	20.6%	20.6%	14.7%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Recovered Gold, Processed	koz	410	-	22	47	69	71	74	72	55	-	-	-	-	-	-	-	-	-
Recovered Silver, Processed	koz	1,396	-	45	243	411	116	254	227	100	-	-	-	-	-	-	-	-	-
Payable Gold, Total	koz	408	-	22	47	68	71	73	72	55	-	-	-	-	-	-	-	-	-
Payable Silver, Total	koz	1,354	-	44	235	398	112	247	220	97	-	-	-	-	-	-	-	-	-
Cash Flow																			
Gold Gross Revenue	\$000s	1,476,625	-	86,459	169,244	245,930	255,358	263,612	258,504	195,918	-	-	-	-	-	-	-	-	-
Silver Gross Revenue	\$000s	65,491	-	2,600	11,300	19,125	5,398	11,846	10,551	4,639	-	-	-	-	-	-	-	-	-
Gross Revenue Before By-Product Credits	\$000s	1,542,117	-	91,059	179,544	265,056	260,757	275,458	269,056	201,156	-	-	-	-	-	-	-	-	-
Gold Gross Revenue	\$000s	1,476,625	-	86,459	169,244	245,930	255,358	263,612	258,504	195,918	-	-	-	-	-	-	-	-	-
Silver Gross Revenue	\$000s	-	-	2,600	11,300	19,125	5,398	11,846	10,551	4,639	-	-	-	-	-	-	-	-	-
Total Gross Revenue After By-Product Credit	\$000s	1,476,625	-	86,459	169,244	245,930	255,358	263,612	258,504	195,918	-	-	-	-	-	-	-	-	-
Mining Cost	\$000s	(314,037)	-	(30,860)	(91,840)	(51,840)	(49,594)	(42,879)	(48,873)	(30,850)	-	-	-	-	-	-	-	-	-
Development Costs	\$000s	(45,374)	-	(3,229)	(6,875)	(8,396)	(6,937)	(6,926)	(11,579)	(4,532)	-	-	-	-	-	-	-	-	-
Process Cost	\$000s	(348,544)	-	(18,640)	(45,693)	(59,933)	(59,933)	(59,933)	(59,933)	(42,477)	-	-	-	-	-	-	-	-	-
G&A Cost	\$000s	(35,041)	-	(2,824)	(5,647)	(5,647)	(5,647)	(5,647)	(5,647)	(4,002)	-	-	-	-	-	-	-	-	-
Refining and Freight Cost	\$000s	(3,157)	-	(156)	(403)	(617)	(486)	(569)	(547)	(379)	-	-	-	-	-	-	-	-	-
Royalties	\$000s	(48,169)	-	(2,727)	(7,374)	(7,933)	(7,808)	(8,247)	(8,056)	(6,023)	-	-	-	-	-	-	-	-	-
Subtotal Cash Costs Before By-Product Credits	\$000s	(760,341)	-	(60,455)	(115,833)	(134,367)	(129,305)	(122,001)	(134,335)	(89,044)	-	-	-	-	-	-	-	-	-
By-Product Credits	\$000s	65,491	-	2,600	11,300	19,125	5,398	11,846	10,551	4,639	-	-	-	-	-	-	-	-	-
Total Cash Costs After By-Product Credits	\$000s	(724,850)	-	(63,855)	(104,533)	(115,241)	(123,907)	(110,155)	(123,784)	(84,405)	-	-	-	-	-	-	-	-	-
Operating Margin	\$000s	751,776	-	24,603	63,711	130,689	131,451	153,459	134,750	113,113	-	-	-	-	-	-	-	-	-
Other Admin Expenses	\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
EBITDA	\$000s	751,776	-	24,603	63,711	130,689	131,451	153,459	134,750	113,113	-	-	-	-	-	-	-	-	-
Depreciation Allowance	\$000s	(454,148)	(219,718)	(114,691)	(32,027)	(27,102)	(6,287)	(34,562)	(14,165)	(3,353)	(2,042)	-	-	-	-	-	-	-	-
Depletion Allowance	\$000s	(203,321)	-	-	(16,304)	(38,568)	(37,942)	(40,052)	(39,154)	(29,270)	-	-	-	-	-	-	-	-	-
Earnings Before Taxes	\$000s	94,307	(219,718)	(114,691)	(7,424)	16,304	85,834	88,947	99,212	92,243	81,800	-	-	-	-	-	-	-	-
Federal & State Income Tax	\$000s	(45,604)	-	(33)	(33)	(2,519)	(6,165)	(5,377)	(9,349)	(9,323)	(8,591)	-	-	-	-	-	-	-	-
Net Income	\$000s	47,702	(219,718)	(114,691)	(7,957)	15,786	77,669	82,410	89,264	82,220	72,819	-	-	-	-	-	-	-	-
Non-Cash Add Back - Depreciation	\$000s	454,148	219,718	114,691	32,027	27,102	6,287	34,562	14,165	3,353	2,042	-	-	-	-	-	-	-	-
Non-Cash Add Back - Depletion	\$000s	203,321	-	-	16,304	38,568	37,942	40,052	39,154	29,270	-	-	-	-	-	-	-	-	-
Working Capital	\$000s	-	(6,592)	(3,447)	(1,435)	(1,476)	(2,515)	(957)	(1,288)	356	458	16,865	-	-	-	-	-	-	-
Operating Cash Flow	\$000s	705,172	(6,592)	(3,447)	22,636	59,716	113,403	123,957	142,225	125,813	104,590	16,865	-	-	-	-	-	-	-
Initial Capital	\$000s	(334,609)	(219,718)	(114,691)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Sustaining Capital	\$000s	(119,539)	-	-	(32,027)	(27,102)	(6,287)	(34,562)	(14,165)	(3,353)	(2,042)	-	-	-	-	-	-	-	-
Closure/Reclamation/Monitoring Costs	\$000s	(19,703)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Capital	\$000s	(472,851)	(219,718)	(114,691)	(32,027)	(27,102)	(6,287)	(34,562)	(14,165)	(3,353)	(2,042)	(8,038)	(2,798)	(2,473)	(2,513)	(1,040)	(751)	(506)	(585)
Cash Flow Adj./Reimbursements	\$000s	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-



Economic Model Annual Summary																						
 Company: New Sleeper Gold LLC. Project Name: Sleeper Gold & Silver OP Project Scenario Name: Alternative Case - M-I Resources Analysis Type: IA & S-K-1300																						
		Year -2	Year -1	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Year 11	Year 12	Year 13	Year 14	Year 15	Year 16			
Calendar Year	Project Stage	US\$ & Metric Units	LoM Avg/Total	Pre-Prod. 22	Pre-Prod. 21	Ops 20	Ops 19	Ops 18	Ops 17	Ops 16	Ops 15	Ops 14	Ops 13	Ops 12	Ops 11	Ops 10	Ops 9	Ops 8	Ops 7	Ops 6	Ops 5	
LoM Metrics																						
Economic Metrics																						
Discount Rate	BOP	%		0.929	0.873	0.798	0.730	0.686	0.632	0.593	0.540	0.502	0.463	0.429	0.397	0.367	0.340	0.312	0.291	0.273	0.262	
a) Pre-Tax	Free Cash Flow	\$000s	278,325	(226,310)	(118,338)	(8,859)	35,132	121,887	95,932	138,006	131,783	111,529	8,827	(2,798)	(2,473)	(2,519)	(1,040)	(751)	(506)	(585)	-	
	Cumulative Free Cash Flow	\$000s		(226,310)	(344,648)	(353,508)	(319,374)	(196,497)	(100,565)	37,452	169,234	300,763	399,590	286,792	284,319	281,807	280,767	280,016	279,510	278,925	278,925	
	NPV @ 8%	\$000s	58,799	(209,546)	(101,456)	(7,032)	25,823	82,954	60,454	89,525	71,198	55,792	4,069	(1,200)	(982)	(924)	(354)	(237)	(148)	(158)	(158)	275,925
	Cumulative NPV @ 8%	\$000s		(209,546)	(311,002)	(318,034)	(292,211)	(209,256)	(148,803)	(68,277)	2,921	58,713	62,802	61,601	60,619	59,696	59,342	59,105	58,957	58,799	58,799	
	IRR	%	11.5%																			
	Payback Period	years	4.7			1.0	1.0	1.0	1.0	0.7	-	-	-	-	-	-	-	-	-	-	-	
b) After-Tax	Free Cash Flow	\$000s	232,321	(226,310)	(118,338)	(9,332)	32,613	113,122	89,395	128,000	122,460	102,548	8,827	(2,798)	(2,473)	(2,519)	(1,040)	(751)	(506)	(585)	-	
	Cumulative Free Cash Flow	\$000s		(226,310)	(344,648)	(354,039)	(321,425)	(208,304)	(119,909)	9,151	131,611	234,159	242,986	240,188	237,715	235,202	234,163	233,412	232,906	232,321	232,321	
	NPV @ 8%	\$000s	31,106	(209,546)	(101,456)	(7,456)	23,372	76,989	56,334	74,722	64,161	51,299	4,069	(1,200)	(982)	(924)	(354)	(237)	(148)	(148)	(148)	-
	Cumulative NPV @ 8%	\$000s		(209,546)	(311,002)	(318,457)	(294,455)	(217,496)	(161,162)	(86,440)	(20,279)	31,020	35,109	33,909	33,927	32,003	31,649	31,412	31,265	31,106	31,106	31,106
	IRR	%	9.5%			1.0	1.0	1.0	1.0	0.9	-	-	-	-	-	-	-	-	-	-	-	
	Payback Period	years	4.9																			
Operating Metrics																						
Mine Life	Years		7																			
Average Daily Mining Rate	td mined		50,000	-	-	41,667	55,556	55,556	53,149	45,738	52,055	46,315	-	-	-	-	-	-	-	-	-	
Average Daily Processing Rate	td placed		29,000	-	-	9,330	22,872	30,000	30,000	30,000	30,000	30,000	-	-	-	-	-	-	-	-	-	
Mining Cost	\$ / t mined		\$2.59	-	-	2.59	2.59	2.59	2.59	2.59	2.59	2.59	-	-	-	-	-	-	-	-	-	
Mining Cost	\$/t process		\$5.03	-	-	11.69	6.30	4.80	4.59	3.95	4.50	4.00	-	-	-	-	-	-	-	-	-	
Dewatering Cost	\$/t process		\$0.73	-	-	0.96	0.83	0.78	0.54	0.46	1.07	0.59	-	-	-	-	-	-	-	-	-	
Processing Cost	\$/t process		\$5.55	-	-	5.55	5.55	5.55	5.55	5.55	5.55	5.55	-	-	-	-	-	-	-	-	-	
G&A Cost	\$/t process		\$0.56	-	-	0.64	0.69	0.52	0.52	0.52	0.52	0.52	-	-	-	-	-	-	-	-	-	
Subtotal Direct Operating Costs	\$/t process		\$11.87	-	-	18.33	13.37	11.65	11.20	10.48	11.64	10.67	-	-	-	-	-	-	-	-	-	
Retrofitting and Freight Cost	\$/t process		\$0.05	-	-	0.05	0.05	0.06	0.04	0.05	0.05	0.05	-	-	-	-	-	-	-	-	-	
Nett Royalty	\$/t process		\$0.74	-	-	0.81	0.65	0.73	0.72	0.76	0.76	0.79	-	-	-	-	-	-	-	-	-	
Total Operating Cost	\$/t process		\$12.66	-	-	19.78	14.07	12.44	11.97	11.30	12.44	11.50	-	-	-	-	-	-	-	-	-	
Sales Metrics																						
Au Sales	koz		408	-	-	22	47	68	71	73	72	65	-	-	-	-	-	-	-	-	-	
Ag Sales	koz		1,354	-	-	44	235	398	112	247	220	97	-	-	-	-	-	-	-	-	-	
Total Cash Cost (LOM)	\$ / oz Au		1,778	-	-								-	-	-	-	-	-	-	-	-	
Total AOC (LOM)	\$ / oz Au		2,117	-	-								-	-	-	-	-	-	-	-	-	
Avg. LOM Annual Au Sales (excl. mining phase)	koz/yr		64	-	-	4,336	2,817	1,779	2,234	1,698	1,770	1,565	-	-	-	-	-	-	-	-	-	
Avg. LOM Annual Ag Sales (excl. mining phase)	koz/yr		218	-	-								-	-	-	-	-	-	-	-	-	





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